

US Army Corps of Engineers<sub>®</sub>

Engineer Research and Development Center

# Assessment of Training Noise Impacts on the Red-cockaded Woodpecker: 1999 Results

by David K. Delaney, Larry L. Pater, Timothy J. Hayden, Linton Swindell, Tim Beaty, Larry Carlile, and Eric Spadgenske May 2000



20000710 126



Engineer Research and Development Center

# Assessment of Training Noise Impacts on the Red-cockaded Woodpecker: 1999 Results

by David K. Delaney, Larry L. Pater, Timothy J. Hayden, Linton Swindell, Tim Beaty, Larry Carlile, and Eric Spadgenske

May 2000



# **Executive Summary**

This report is submitted as partial fulfillment of the terms of the Strategic Environmental Research and Development Program (SERDP)-funded project CS-1083. The purpose of this research is to assess the effects of military training noise on the endangered Red-cockaded Woodpecker (RCW) and to develop assessment methodology. The results of this research will provide a scientific basis for RCW management protocols, and will partially satisfy requirements of a 1996 U.S. Fish and Wildlife Service (USFWS) biological opinion that requires the Army to assess effects of implementing the 1996 "Management Guidelines for the RCW on Army Installations." These new guidelines significantly reduce restrictions on training for military installations on which RCWs are present. These installations include Fort Stewart, GA; Fort Bragg, NC; Fort Benning, GA; Fort Polk, LA; Fort Gordon, GA; Fort Jackson, SC; Camp Lajeune, NC; Eglin Air Force Base (AFB), FL; and Camp Blanding, FL. This research is being conducted jointly by the U.S. Army Construction Engineering Research Laboratory (CERL), an element of the U.S. Army Engineer Research and Development Center (ERDC); Fort Stewart, and the U.S. Army Forces Command (FORSCOM). The project was developed by CERL in coordination with FORSCOM, the USFWS RCW Recovery Coordinator and Region 4 office, the Fort Stewart Director of Training, the Fort Stewart Department of Public Works (DPW) Fish and Wildlife Branch, and the Army Threatened and Endangered Species (TES) User Group.

During this second year of the study, we experimentally tested RCW response to controlled military training noise events under realistic conditions, namely .50-caliber blank fire and artillery simulators. We measured both proximate response behavior and nesting success, while continuing to measure baseline behavioral data from undisturbed sites. Measured levels of experimental noise did not affect RCW nesting success or productivity. RCW flush response was shown to increase as stimulus distance decreased, regardless of stimulus type. Woodpeckers returned to their nests relatively quickly after being flushed. Noise levels within RCW nest cavities were substantially louder than levels recorded at the base of the tree. It is important to note that the data collected to this point are sufficient to confirm statistical power to make strong conclusions or to establish reliable noise dose-response relationships or thresholds. The data collected to this point are sufficient to confirm that the project technical approach is appropriate and that the research objectives will be achieved.

# **Foreword**

This study was conducted for the Strategic Environmental Research and Development Program (SERDP) under an FY98 Conservation Project, No. CS-1083, "Assessment of Training Noise Impacts on the Red-cockaded Woodpecker." The technical monitor was Dr. Robert Holst.

The work was performed by the Ecological Processes Branch (CN-N) of the Installations Division (CN), Construction Engineering Research Laboratory (CERL) in cooperation with Jones Technologies, Inc. The CERL Principal Investigator was Dr. Larry L. Pater. The technical editor was Gloria J. Wienke. Steve Hodapp is Chief, CEERD-CN-N, and Dr. John T. Bandy is Chief, CEERD-CN. The Acting Director of CERL is Dr. Alan W. Moore.

CERL is an element of the U.S. Army Engineer Research and Development Center (ERDC), U.S. Army Corps of Engineers. The Acting Director of ERDC is Dr. Lewis E. Link and the Commander is COL Robin R. Cababa, EN.

This work could not have been accomplished without the very able field assistance of (alphabetical) Tim Brewton, Michelle Huffman, Margaret Klich, Ronald Knopik, Brian Platt, Aaron Rinker, and Andrew Walde. We particularly appreciate the skill, support, and cooperation of the 10<sup>th</sup> Engineer Battalion; the 3<sup>rd</sup> Battalion, 7<sup>th</sup> Infantry; and the 3<sup>rd</sup> Squadron, 7<sup>th</sup> Cavalry for providing personnel, equipment, and supplies to assist us in conducting our experimental trials. We thank the Director of Training Office on Fort Stewart, particularly Howard Bullard, Tony Tellames, and Joe Caligiure for logistical support and close cooperation in the day-to-day operation of this study. We would also like to thank Linton Swindell and his staff at the Department of Public Works Fish and Wildlife Office for all their assistance during this project.

#### DISCLAIMER

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products. All product names and trademarks cited are the property of their respective owners.

The findings of this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

DESTROY THIS REPORT WHEN IT IS NO LONGER NEEDED. DO NOT RETURN IT TO THE ORIGINATOR.

# **Contents**

Executive Summary3				
Fo	reword	4		
List of Figures and Tables				
1	Introduction	9		
	Background	9		
	Objectives			
	Approach	11		
	Scope	11		
	Mode of Technology Transfer	12		
2	Literature Review	13		
3	Technical Approach	16		
	Null Hypotheses	16		
	Study Area	16		
	Sample Cluster Selection	17		
	Impact Measures	19		
	Behavior and Proximate Response Measurement Protocols	21		
	Demographic and Nesting Success Data	21		
	Video Surveillance	23		
	Sound Instrumentation and Recording	24		
	Sound Metrics	24		
	Statistical Data Analysis	26		
4	Results	27		
	Initiation Dates for each Nesting Phase	27		
	Overall Population Dynamics	27		
	Sample Cluster Population Dynamics	28		
	Noise and Response Monitoring Summary			
	Passive Monitoring			
	Experimental Testing			
	Noise Measurement Testing			
	Distance and Noise Level Thresholds for Response	30		

	Experime	ntal Tests	30
	Passive E	Events	32
5	Discussion	n	38
	Nesting Su	ıccess	38
		oonse and Related Behaviors	
		sponse	
		ehaviors	
	Distance a	nd Sound Thresholds	39
	Noise Mea	surement Test	40
6	Plans and	Conclusions	41
	Plans		41
		ns	
Re	ferences		43
Αp	pendix A:	Significant Legal Requirements	50
Αp	pendix B:	Summary Data Tables	51
Αp	pendix C:	Source Spectra Examples	54
Αp	pendix D:	Detailed Noise Event and RCW Response Data	59
CE	RL Distribu	tion	143
D.	nort Docum	nentation Page	144

**Figures** 

# **List of Figures and Tables**

	1	Adult Red-cockaded Woodpecker delivering prey to the nest10		
	2	Location of Fort Stewart within the state of Georgia17		
	3	Locations of training areas and RCW clusters on Fort Stewart18		
	4	Artillery simulator blast		
	5	.50-caliber machine gun		
	6	Assessment hierarchy for training impact on threatened and endangered species20		
	7	Examples of audiograms and frequency weighting26		
	8 .	RCW flush frequency by stimulus type and distance31		
	9	Mean return time for RCWs in response to experimental testing31		
	10	Noise levels from M-16 live fire events at cluster 103 on May 12, 199933		
	11	Noise levels from M-16 live fire events at cluster 103 on May 13, 199933		
	12	Noise levels from M-16 live fire events at cluster 103 on May 13, 199935		
	13	SEL weighting comparison for M-16 live fire on May 17, 1999, from range and tree impact noise near a RCW nest site35		
	C-1	SEL weighting comparison for experimental artillery simulator blast at cluster 172 on June 4, 1999		
	C-2	SEL weighting comparison for experimental .50-caliber blank fire at cluster 151 on June 24, 1999		
	C-3	SEL weighting comparison for a passive grenade simulator blast at cluster 41 on June 2, 199956		
	C-4	SEL weighting comparison for a passive helicopter flight at cluster 6 on April 29, 199957		
	C-5	SEL comparison of passive large-caliber live fire at cluster 172 on April 27, 199958		
Tables				
	B1	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of experimental artillery simulator testing on Fort Stewart, GA, 1999		
	B2	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of experimental .50-caliber blank fire testing on Fort Stewart, GA, 1999.		

B3	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive M-16 live fire on Fort Stewart, GA, 1999.	53
B4	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive grenade simulator blasts on Fort Stewart, GA, 1999.	53
B5	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive helicopter flights on Fort Stewart, GA, 1999. Stimulus distances represent the closest estimated approach distance by a helicopter	53
B6	Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise level of passive large-caliber live fire on Fort Stewart, GA, 1999	53
D1	Summary data for experimental artillery simulator blast noise on Fort Stewart, GA, 1999.	60
D2	Representative unweighted noise spectra for experimental artillery simulators on Fort Stewart, GA	67
D3	Summary data for experimental .50 caliber blank fire on Fort Stewart, GA	74
D4	Representative unweighted spectra for experimental .50-caliber blank fire on Fort Stewart, GA.	94
D5	Summary data for passive M-16 live fire noise on Fort Stewart, GA	. 111
D6	Representative unweighted noise spectra for passive M-16 live fire on Fort Stewart, GA	.120
D7	Summary data for passive helicopter flights on Fort Stewart, GA	.131
D8	Representative unweighted noise spectra for passive helicopter flights on Fort Stewart, GA.	.132
D9	Summary data for passive large-caliber live fire noise on Fort Stewart, GA	.133
D10	Representative unweighted noise spectra for passive large-caliber live fire events on Fort Stewart, GA.	.134
D11	Summary data for ambient sound levels on Fort Stewart, GA	.135
D12	Representative unweighted noise spectra for ambient sound levels on Fort	139

# 1 Introduction

#### **Background**

The Endangered Species Act requires that all Federal agencies carry out programs to conserve threatened and endangered species (TES) and to evaluate the impacts of Federal activities on listed species (Scott et al. 1994). TES management on military installations, particularly that involving the Red-cockaded Woodpecker (RCW), has raised questions about the interaction between Army training and the conservation of Red-cockaded Woodpeckers on military lands. The goal of RCW management on Fort Stewart is to recover the population while eliminating conflicts with the training mission by eliminating the need for training restrictions (Fort Stewart Endangered Species Management Planning [ESMP] Team 1998). A brief summary of legal requirements is presented in Appendix A. Because noise management has traditionally focused on minimizing human annoyance, loud activities have often been relocated to sparsely populated areas where wildlife resides. This has led to increased interactions between military activity and wildlife (Holland 1991). Increasing importance has been placed on determining the extent of noise impacts on wildlife (Bowles 1995), especially threatened and endangered species (Delaney et al. 1999; Pater et al. 1999).

The Red-cockaded Woodpecker (*Picoides borealis*) is an endangered species that inhabits mature, open pine forests of the southeastern United States (Figure 1; Jackson 1994). Historically, RCW populations were distributed throughout the South from eastern Texas to the Atlantic coast, and north to New Jersey (Jackson 1987). The distribution has been reduced with the extirpation of RCWs from New Jersey (Lawrence 1867), Missouri (Cunningham 1946 as cited in Jackson 1987), and most recently Maryland (Devlin et al. 1980). The majority of RCWs are currently restricted to public lands, namely National Forests, military installations, and National Wildlife Refuges (Jackson 1978, Lennartz et al. 1983). Military installations, in particular, are gaining recognition as a valuable resource in the recovery of TES (Jordan et al. 1995). It has been estimated that nearly a quarter of the remaining RCWs are located on nine military installations in the southeast (Costa 1992), which includes the Fort Stewart population. Such a close association has led to increased conflicts between TES conservation

requirements and the military's mission of maintaining a high degree of combat readiness (Jordan et al. 1995).



Figure 1. Adult Red-cockaded Woodpecker delivering prey to the nest.

In 1984 the Army initially established a 200-ft (61-m) buffer zone around all RCW cavity trees to protect nesting habitat and identify RCW management units. In 1996, the Department of the Army (DA) issued revised guidelines for the management of RCWs on military lands, to reduce training restrictions, and increase adaptive management of the RCW and its habitat. These guidelines are scheduled to go in to effect by early 2000. Under the revised guidelines, certain transient military activities are permitted within 50 ft (15 m) of RCW cavity trees. These include: (1) military vehicle and personnel travel, including armor; (2) .50-caliber machine gun blank fire and 7.62-mm blank fire and below; (3) artillery/hand grenade simulators and Hoffman type devices; (4) hand digging of hasty individual fighting positions; (5) use of smoke grenades and star cluster/parachute flares; and (6) smoke and haze operation (see Hayden 1997 for a more detailed description of past and current Army guidelines for RCWs). A 1996 USFWS biological opinion requires the Army to assess effects due to implementing the 1996 guidelines (Jordan et al. 1997). The current project will provide an important aspect of this required assessment.

The Fort Stewart Fish and Wildlife Directorate prepared an Endangered Species Management Plan (Fort Stewart ESMP Team 1998) for the installation that detailed changes under these revised guidelines: (1) consideration will be given jointly to training mission requirements and RCW biological requirements when implementing ESMP; (2) reduction in off-limit area for thru-cluster maneuver traffic around cluster trees from 200 ft (61 m) to 50 ft (15 m); and (3) the types of training activities allowed within RCW clusters will be expanded.

#### **Objectives**

The primary research objective of this multiyear study is to determine the impact of certain types of training noise on the endangered Red-cockaded Woodpecker. This will require that we develop dose-response threshold relationships for quantifying RCW responses to noise levels and stimulus distances, and relate these to nesting success. A second objective is to develop and disseminate costeffective techniques for documenting the effects of training noise on TES populations. These techniques include the capability to characterize noise stimuli, to document behavioral responses, and to determine resulting population effects due to military noise. Achieving these objectives will provide a means to manage impact on both military training capability and TES, and will provide a factual basis for mitigation and management protocols and guidelines. This research directly addresses the #1 Army Conservation Pillar User Requirement, which is concerned with impacts of military operations on threatened and endangered species. The results of this research will partially satisfy requirements of the 1996 USFWS biological opinion (Jordan et al. 1997) that requires the Army to assess effects due to implementing the 1996 "Management Guidelines for the RCW on Army Installations."

## **Approach**

Chapter 3 presents details of the technical approach used in this research. The chapter includes discussions of the study area, cluster selection, impact measures, response protocols, nesting success, video surveillance, sound instrumentation and recording, sound metrics, and statistical analysis.

## Scope

All aspects of the research plan were reviewed and approved by the USFWS and Fort Stewart before monitoring activity began. Results from this research apply

directly to Fort Stewart, but may also be applicable to other installations in the southeastern United States where RCWs are exposed to similar noise. This study will use population data collected at Fort Stewart and other installations under a Forces Command (FORSCOM) program. Specific evaluation of impact of maneuver training activities is being conducted under a separate coordinated research effort. Training noise sources examined during this study include artillery simulators, .50-caliber blank fire, large-caliber live fire, small-arms live fire, grenade simulators, and helicopter flights. RCW response to other military activity, such as vehicle noise associated with maneuver training, aircraft overflights, and Multiple Launch Rocket System (MLRS) fire, will be documented opportunistically, but is not of high priority in this study.

#### Mode of Technology Transfer

Products of this research will be provided directly to the Military Services for use during consultation with the USFWS and for development of management protocols. This aspect of the transition plan will directly help to alleviate impacts on military training capability and will provide information to the military that will guide effective management of impacts on endangered species populations. Other technology transfer methods will include technical papers and journal articles and TES and noise workshops. The information will also be disseminated through the Environmental Noise Program Office of the U.S. Army Center for Health Promotion and Preventive Medicine, the Army TES User Group, and the U.S. Air Force (USAF) International Bibliography on Noise (IBON). Other forums for dissemination include the North Atlantic Treaty Organization (NATO) Committee for Challenges to Modern Society (CCMS) subcommittees for noise effects, the International Committee on the Biological Effects of Noise (ICBEN), the Acoustical Society of America Animal Bioacoustics technical committee, and the Department of Defense (DoD) Committee on Environmental Noise.

# 2 Literature Review

Noise disturbance studies have often been anecdotal and fail to quantitatively measure either the stimulus or the behavioral response related to the animal's fitness. Predictive models for the relationship between disturbance dosage and quantifiable effects are even more scarce (Awbrey and Bowles 1990; Grubb and King 1991; Grubb and Bowerman 1997). Although many types of human disturbance have been reported as affecting birds (Fyfe and Olendorff 1976), very little research has addressed the effects of human activity on woodpeckers, especially the endangered Red-cockaded Woodpecker (Charbonneau et al. 1983; Jackson 1983; Beaty 1986; Jackson and Parris 1995; The Nature Conservancy [TNC] 1996; Pater et al. 1999).

Few researchers have directly compared differences in bird responsiveness between aerial and ground-based disturbances (Bowles et al. 1990). Studies that have examined the effects of aircraft activity on nesting birds (e.g., Platt 1977; Windsor 1977; Ellis 1981; Anderson et al. 1989) have often noted a slight but nonsignificant decrease in nesting success and productivity for disturbed versus undisturbed nests. Anderson et al. (1989) noted a slight decline in the nesting success of experimental Red-tailed Hawk (*Buteo jamaicensis*) nests versus control nests (80 percent experimental versus 86 percent control success) after helicopter disturbances.

In contrast, ground-based disturbances appear to have a greater effect than aerial disturbances on the nesting success of some bird species. In their classification tree model of Bald Eagle (*Haliaeetus leucocephalus*) responses to various anthropogenic disturbances, Grubb and King (1991) determined that Bald Eagles in Arizona showed the highest response frequency and severity of response toward ground-based disturbances, followed by aquatic, and lastly by aerial disturbances. Delaney et al. (1999) reported similar findings for Mexican Spotted Owl (*Strix occidentalis lucida*) response to military helicopter activity and chain saws, observing that chain saws elicited a greater flush response rate than helicopters at comparable distances and noise levels.

A bird's behavior during the nesting season is an important determinant of its ultimate nesting success or failure (Hohman 1986). Various bird species have been reported to abandon their nests after being exposed to ground-based and

aerial disturbances. White and Thurow (1985) reported that approximately 30 percent of Ferruginous Hawks (*Buteo regalis*) abandoned their nests after being exposed to various ground-based disturbances, but there were no controls for comparison. Anderson et al. (1989) reported that 2 of 29 Red-tailed Hawk nests were abandoned after being flushed by helicopter flights, compared with 0 of 12 control nests. Ellis et al. (1991) found only 1 of 19 Prairie Falcon (*Falco mexicanus*) nests were abandoned when exposed to frequent low-altitude jet flights during the nesting season (no control sites used). Platt (1977) reported similar rates with only 1 of 11 Gyrfalcon (*F. rusticolus*) nests failing (reportedly due to snow damage), compared with 0 of 12 control nests. Of the 6 Peregrine Falcon (*F. Peregrinus*) nests exposed to helicopter flights, only 1 was abandoned (also apparently due to inclement weather) compared with 0 of 3 control sites (Windsor 1977).

Birds may be more susceptible to disturbance-caused nest abandonment early in the nesting season, possibly because parents have less energy invested in the nesting process (Knight and Temple 1986). Some animals appear reluctant to leave the nest later in the nesting season (Anderson et al. 1989; Ellis et al. 1991; Delaney et al. 1999). Steenhof and Kochert (1982) reported that Golden Eagles (Aquila chrysaetos) and Red-tailed Hawks exposed to human intrusions during early incubation had significantly lower nesting success than individuals exposed later in the season (45 percent success for Golden Eagles and 57 percent for Red-tailed Hawks within experimental groups versus 71 percent and 74 percent success with control groups, respectively). Although reactions of adult birds at the nest can influence hatching rates and fledgling success (Windsor 1977), flush behavior of adult birds from the nest is poorly quantified (Fraser et al. 1985; Holthuijzen et al. 1990; Delaney et al. 1999). In the few studies that have examined bird responses to specific disturbance types (e.g., aircraft approach distance), flush rates were higher if birds were naive (i.e., not previously exposed; Platt 1977). Some birds are more reluctant to flush off the nest during incubation and early nestling phases than later in the season (Grubb and Bowerman 1997; Delaney et al. 1999). Animal responsiveness has been shown to increase as the nesting season progresses (Grubb and Bowerman 1997). Delaney et al. (1999) found that Mexican Spotted Owls were more responsive to helicopters later in the reproductive cycle, which suggests that adult defensive behavior may decrease as the young mature. In contrast, Holthuijzen et al. (1990) found Prairie Falcon responsiveness to nearby blasting activity decreased as the nesting season progressed.

Few studies have documented the threshold distance that causes birds to flush in response to noise disturbance events. In those studies that reported stimulus distance, it was rare for birds to flush when the stimulus distance was greater than 60 m (Carrier and Melquist 1976; Edwards et al. 1979; Craig and Craig 1984; Delaney et al. 1999). Similar findings were reported by Carrier and Melquist (1976) for Osprey (*Pandion haliaetus*), and Ellis (1981) for Peregrine Falcons. Many disturbance study reports imply that animal response increases with decreasing stimulus distance (Platt 1977; Grubb and King 1991; McGarigal et al. 1991; Stalmaster and Kaiser 1997), though only a few studies have experimentally tested this relationship (Delaney et al. 1999; Pater et al. 1999). Delaney et al. (1999) found that the proportion of owls flushing in response to a disturbance was strongly and negatively related to stimulus distance and positively related to noise level. Pater et al. (1999) found similar results when they experimentally exposed Red-cockaded Woodpeckers to military training noise.

Even fewer examples are available for noise response thresholds. Snyder et al. (1978) reported that Snail Kites (Rostrhamus sociabilis) did not flush even when noise levels were up to 105 decibels, A-weighted (dBA) from commercial jet traffic. This result was qualified by the fact that test birds were living near airports and may have habituated to the noise. Edwards et al. (1979) found a doseresponse relationship for flush responses of several species of gallinaceous birds when approach distances were between 30 and 60 m and noise levels approximated 95 dBA. Delaney et al. (1999) reported that Mexican Spotted Owls did not flush during the nesting season when the sound exposure level (SEL) for helicopters was  $\leq$  92 dBA and the Equivalent Average Sound Level (LEQ) for chain saws was  $\leq$  46 dBA. Noise response thresholds were fairly comparable with data from the nonnesting season (SEL of 92 dBA for helicopters and LEQ of 51 dBA for chain saws).

Distance has been described as the most commonly used surrogate for noise disturbance in the literature on animal response to noise, and has been proposed to be the best representative for quantifying the relationship between stimulus and response measures (Awbrey and Bowles 1990). The reason appears to be that distance is more conveniently implemented into management practices (i.e., establishing buffer zones) than other variables. However, use of a properly measured noise level as the stimulus measure facilitates broader application of response results, in particular to sources of similar aural character but different acoustic power emission.

# 3 Technical Approach

#### **Null Hypotheses**

Data collection, summary, and statistical analyses to assess and characterize military training noise in RCW clusters, and to evaluate the relationship between noise levels and RCW demographic data, are based on the following formal null hypotheses:

- Ho: There is no difference in the nesting success, productivity, or nesting behavior between disturbed and undisturbed RCW nest sites.
- Ho: There is no relationship between stimulus distance or noise level and RCW response behavior.
- Ho: There is no difference in RCW response between types of training activities.

#### Study Area

Fort Stewart is located in southeast Georgia (Figure 2), within Liberty, Long, Bryon, Tattnall, and Evans counties, and is the largest Army Installation east of the Mississippi River. Physiographically, this area lies within the Atlantic Coastal Flatwoods Province, within a humid, semi-tropical latitude, and averages 50 in. (127 cm) of rain per year. The average temperature in January is 62 °F (44 °C) with a relative humidity of 70 percent, while July averages 91 °F (32 °C) with a relative humidity of 76 percent. Approximately 66 percent of the 112,745 ha of the installation are terrestrial and cover three main forest types: upland pine stands composed primarily of longleaf (*Pinus palustris*), loblolly (*P. taeda*), and slash pine (*P. elliottii*); mixed pine-hardwood sites; and hardwood stands. The remaining habitats include various wetland types and open water (Fort Stewart ESMP Team 1998).

The primary mission of Fort Stewart is training and operational readiness of the 3rd Infantry Division (Mech.) and other nondivision units. The 3rd Infantry Division (previously the 24th) was activated in 1975 and redesignated as a mechanized division in 1979 (Hayden 1997). Training activities are conducted year-round at Fort Stewart to maintain a combat ready fighting force. The installa-

tion also supports training of regional National Guard and Reserve units, as well as joint training exercises with troops from other installations and DoD Branches (Fort Stewart ESMP Team 1998).

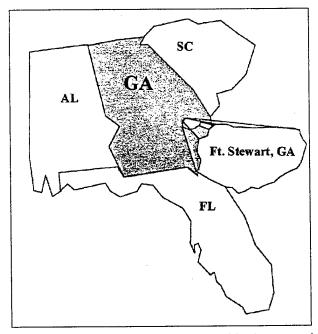


Figure 2. Location of Fort Stewart within the state of Georgia.

Fort Stewart contains a variety of impact and firing areas (Figure 3). The central feature of the installation is the Artillery Impact Area (AIA; about 5,200 ha), which is surrounded by dozens of artillery firing points varying in distance from a few hundred meters to thousands of meters from the impact area. On the western border of the AIA is the Red Cloud Multipurpose Range Complex (MPRC) containing eight separate ranges. Just south of the AIA is the Explosive Ordnance Disposal Area (EOD), the Demolition Area (DEMO), and the Small Arms Impact Area (13 live-fire ranges, about 2,300 ha). To the east and northeast of the AIA are the Calfax and Luzon Ranges, and three smaller Aerial Gunnery Ranges (AGRs). There are also seven drop zones located throughout the installation (Hayden 1997).

#### Sample Cluster Selection

There are 294 known RCW clusters distributed across Fort Stewart (Figure 3). None are known to be in the AIA because this area has not been surveyed due to safety concerns. Of the approximately 165 reproductively active (mated pair present) RCW clusters in 1999, we chose 48 sample clusters for experimentation during the second field season. This was a substantial increase over 1998 for

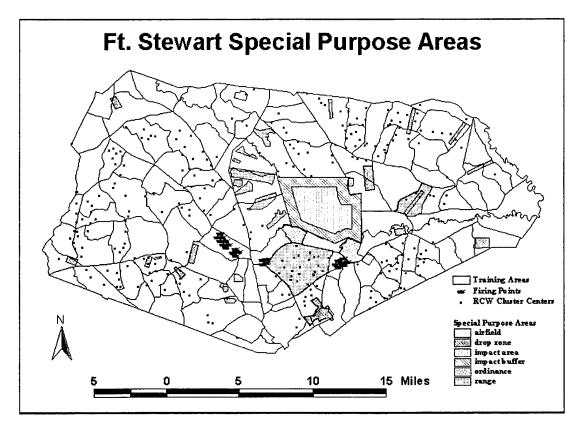


Figure 3. Locations of training areas and RCW clusters on Fort Stewart.

which we were able to collect experimental data at only four sample clusters (Pater et al. 1999). We intend to use these same clusters insofar as practical throughout this multiyear study. We classified clusters according to type and level of training noise, based on the number, distance, and noise levels of stimulus events that each cluster typically receives. Three types of sample sites were chosen: passive disturbed, undisturbed, and experimental. "Passive disturbed" sites were those sites that received potentially significant noise disturbance as part of normal training operations; we had no direct control over time, number, or level of noise events at these sites. Noise types include large-caliber live fire, small arms live fire, grenade and artillery simulators, and helicopter flights. We attempted to choose sites that received predominantly one type of noise, but this was sometimes impossible if we were to also use the highest noise level clusters. "Undisturbed" or "low disturbance" sites (the two terms are equivalent and are used interchangeably in this report) are sites where noise levels were judged likely to be consistently low or absent for all of the noise types. At these sites we observed behavior and measured success as a baseline for judging impact at disturbed sites. It is likely that at least some level of military noise of some type can be perceived at every RCW cluster on Fort Stewart. Our criterion for low disturbance is noise levels at or near ambient noise levels. At "experimental" sites we exposed birds to either artillery simulators (Figure 4) or .50-caliber blank fire (Figure 5) under controlled conditions at distances of 15.2, 30.5, 61,

76.2, 91.5, 122, and 244 m from the nest tree (Appendix B, Tables B1 and B2). Not all distances were tested for each noise source because bird response dictated which distances would be used for developing a distance-response threshold. The experimental sites were chosen from among cluster sites that had low to moderately low disturbance levels. This implies that birds at these sites were not habituated to the noise stimulus. Sample size was limited by the number of clusters that fit each of the foregoing selection protocol criteria and by available field observation resources.



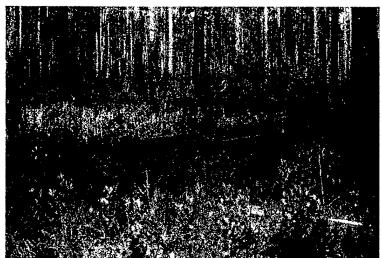


Figure 4. Artillery simulator blast. Figure 5. .50-caliber machine gun.

#### **Impact Measures**

Selection of noise impact criteria is a critical issue. For humans the response criterion is typically annoyance. For domesticated species the issue may be damage to individual animals or impacts on profits. For TES, the ultimate concern is long-term survival of the species. The challenge is to develop a relatively short-term procedure for inferring impact on long-term survival. The conceptual approach used in this study is depicted in Figure 6. First, proximate responses to the noise stimulus are measured. A proximate response is the direct and immediate response of the animal to the stimulus; for example a behavioral (e.g., flight) or a physiological (e.g., change in heart rate) response. This tracks with the first regulatory decision criterion of the Endangered Species Act (ESA), that is, whether the action or activity "may affect" the species. Next, we examine whether the stimulus that elicited the proximate response affects "individual fitness," which is typically evaluated in terms of adult and juvenile mortality or

reduced nesting success. Mortality and nesting success are established by field monitoring of many individuals throughout the nesting season. This level of effect tracks with the next decision criterion of the ESA, namely whether the action or activity is "likely to jeopardize the continued existence" of the species. Population effects will be inferred from measures of individual fitness by application of population viability analysis (PVA) models. Current applications of PVA do not capture the temporal and spatial variability of training events, and thus cannot model the resulting effects on endangered species' demographic parameters. Researchers at the Engineer Research and Development Center, Construction Engineering Research Laboratory (ERDC/CERL) currently are developing PVA modeling approaches capable of capturing training effects in predictive population models. This is a shared effort under this project and a related ERDC/CERL research effort to evaluate effects of maneuver training (vehicles and troops) on RCWs.

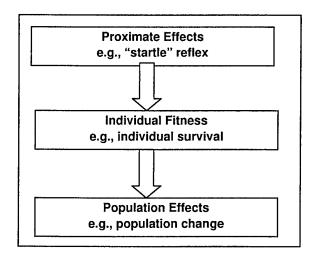


Figure 6. Assessment hierarchy for training impact on threatened and endangered

In summary, the research paradigm is that proximate effects can be linked to individual fitness, which in turn can be linked to population effects. As a specific example, consider that a bird might flush from a nest (a proximate response) in response to a noise event. It is possible that this could lead to failure of the nest, especially if the noise and flush response occurred repeatedly. Monitoring is required to determine nesting success of disturbed and undisturbed nests. A population model is required to determine if such failure of some percentage of nests has an effect on survival of the population.

#### **Behavior and Proximate Response Measurement Protocols**

We documented woodpecker behavior at low and high noise disturbance nest sites by direct observation (camouflaged blinds more than 30 m from the nest) and through video surveillance. We divided the nesting cycle into three stages: incubation (eggs present 0 to 11 days), brooding (small chicks attended by adults: days 12 through 22), and nestling (larger chicks typically unattended in nest: day 23 until fledging). A "data session" consisted of behavioral observations of at least one adult RCW, typically for 1 hour or longer. At disturbed sites we attempted to observe behavior for some period of time before and after each noise event. This was sometimes not possible at passive disturbed sites because noise events were so frequent that we could not document undisturbed behavior for extended periods of time.

To evaluate RCW baseline behavior and responses to military training activities, we measured several parameters:

- 1. Alert RCW moves to the cavity mouth, head movements, orient to noise source;
- 2. Flush from nest RCW departs from the nest in response to the stimulus, and remains away from the nest for a measured period of time;
- Recovery time length of time an adult is away from the nest after being flushed;
- 4. Nest attentiveness proportion of time that the adults spend on the nest through the nesting season (calculated for diurnal, 24-hour periods, and for each nesting phase);
- 5. Prey deliveries number and rate of prey deliveries to the nest;
- 6. Trips number and duration of times the attending adult left the nest.

RCW behavior categories 4 through 6 will be presented in a future report after the data have been fully analyzed.

## **Demographic and Nesting Success Data**

RCW demographic data (population size, growth, density, and distribution) were collected in accordance with established protocols used by the Fish and Wildlife Branch DPW on Fort Stewart. Demographic data included the following parameters for each cluster:

- 1. Cluster occupancy cluster occupied by one or more RCWs. Most individuals are identified by unique leg band combinations (provides a measure of population size, growth, and stability);
- 2. Mated status presence of both an adult male and an adult female RCW;
- 3. Active nest at least one egg was laid;
- 4. Nesting success at least one fledgling was produced (provides a measure of the proportion of RCW clusters that are reproductively successful);
- 5. Nesting productivity number of young fledged per nest (provides a measure of fecundity);
- 6. Number of eggs produced;
- 7. Number of nestlings hatched;
- Group size (provides a possible measure of territory quality and availability).

#### These data enable several trends to be detected:

- 1. Reproductive loss mortality rate of eggs, nestlings, and fledglings during nesting;
- 2. Annual nest reoccupancy rates provides a potential measure of RCW response to disturbance. Sites with heavy disturbance levels may be abandoned in subsequent years in favor of other sites further from specific disturbances;
- 3. Site tenacity turnover rate of adult and helper RCWs within a cluster site across years;
- 4. Nesting success rates at disturbed and undisturbed sites;
- 5. Mean number of young fledged at disturbed and undisturbed sites;
- 6. Mean clutch and brood size at disturbed and undisturbed sites;
- 7. Reproductive potential total number of young that could be produced if all eggs and nestlings survived to fledge successfully.

Most of the demographic data for Red-cockaded Woodpecker clusters was collected by DPW Fish and Wildlife personnel from Fort Stewart. Each active (at least one RCW present) cluster was initially visited to determine the cluster occupancy. Adult RCWs were banded to determine group size and affiliation using methods similar to Walters et al. (1988). A 25 percent random sample of all RCW clusters were then monitored approximately every 7 to 9 days to record clutch and brood size. Nestlings were uniquely color banded approximately 5 to 10 days after hatching. Clusters were visited 20 to 25 days after nestlings were banded to determine the number and sex of fledglings (Walters et al. 1988). The 25 percent sample included many of our sample clusters. We augmented the DPW Fish and Wildlife sample by monitoring demographic data (particularly the number of young fledged) for additional cluster sites to provide more complete coverage of our sample clusters.

#### Video Surveillance

Video cameras are being used as a means to record RCW behavior over prolonged periods, to reduce costs, and to avoid potentially disruptive effects of human presence. The camera systems can also be used to document response in areas that cannot be safely monitored (e.g., downrange from firing positions). Cameras were attached to tree trunks with adjustable, jointed angle-brackets and screws. Cameras were mounted at the same level or slightly above nest height in the nearest practical tree and at least 5 m from the nest tree so as not to disturb incubating woodpeckers. Power and coaxial cables were covered with camouflaged cloth and were attached to a 10.5-cm, DC (direct current) monitor and battery so camera placement could be directed from the base of the camera tree. At least two people are required for camera placement: a climber to position the camera and a person on the ground to check the video signal and placement. Then, a trunk line is attached at the base of the tree (covered by a camouflaged 1.2-cm diameter hose for protection against rodents), allowing the power/recording station to be placed 60 m from the tree to minimize potential disturbance to the woodpeckers. We put the recorder, twin batteries, and all connectors inside a weatherproof bin concealed under a camouflaged tarpaulin. Freshly recharged batteries are used for each set of recordings. We used chargecoupled device (CCD) video-board cameras (both black and white and color) to document RCW behavior at 8 nest sites during the 1999 nesting season. The solid state, 12-volt, flexible circuit-board black and white cameras were equipped with 12.0-mm lenses, while the color cameras had 75-mm lenses. The cameras provide a minimum of 380 lines of resolution and have a minimum sensitivity of 0.45 Lux. Black and white cameras are mounted in waterproof heavy-gauge plastic switch boxes with transparent covers (12.9 x 6.7 x 4.1 cm) which, except for the lens and LED (light-emitting diode) area, are painted black. Color cameras were housed in metal weatherproof containers. Two ports are threaded into the protective housing: one for the power supply and the second for the video signal (Delaney, Grubb, and Garcelon 1998). Panasonic Model AG-1070DC Professional/Industrial VHS video recorders, connected to cameras via coaxial cable (RG-59), provided approximately 24 hours of coverage per tape. These 12-volt, DC-powered recorders were designed for surveillance applications. Cameras and video recorders are powered by two 12-volt, 33.0-amp-hour, Power-Sonic Model PS-12330 sealed rechargeable batteries connected in parallel (a 24-hour taping would draw a single battery below operational limits). These "gel-cell" type batteries (weighing 11.3 kg each) reduce the risk of battery damage, and eliminate the potential for spillage during backpack transport.

#### Sound Instrumentation and Recording

Sony TCD-D7, Digital Audio Tape (DAT) recorders were used to continuously record all noise events, along with the exact time and date. We attached Bruel & Kjaer (B&K) Type 4149 1.3-cm Condenser Microphones with 7.5-cm wind screens to B&K Model 2639 Preamplifiers, mounting the microphone on a 1-m stick, and placing the unit directly under a woodpecker's nest about 1-m from the tree trunk. The power supply and DAT recorder were also placed at the base of the nest tree in a small camouflaged container. A 1.0-kHz, 94-dB calibration signal (20 micropascals reference) from a B&K Type 4250 Sound Level Calibrating System was recorded before and after each noise event recording. This signal provides a reference for sound levels and spectra when data are later analyzed using a B&K Type 2144 Frequency Analyzer. All noise data were analyzed at ERDC/ CERL. In addition to recording noise levels at the base of the nest tree, we also recorded noise levels within nest cavities during the postnesting season and at nonnesting sites.

#### **Sound Metrics**

Noise is defined as sound that is undesirable or constitutes an unwarranted disturbance, and can alter behavior or normal functioning (ANSI S1.1-1994). The types of military noise that are within the scope of this study vary widely in instantaneous transient amplitude, duration, spectral energy content, and suddenness of onset. Appropriate noise metrics and frequency weighting are essential to adequately quantify noise impact for each type of noise. Noise metrics are chosen to measure the noise dose in a way that meaningfully correlates with subject response. Frequency weighting is an algorithm of frequency-dependent attenuation that simulates the hearing sensitivity and range of the study subjects. Frequency weighting discriminates against sound that, while easily measured, is not heard by the study subjects. The current project requires specialized metrics and techniques to meaningfully measure noise impacts on animals. Our paradigm is to measure noise events in terms of unweighted one-third-octave-band levels, apply frequency weighting to the resultant spectra, and calculated appropriate overall metrics.

Only noise that is audible to the study species should be accounted for in the metric used to quantify noise level. Frequency weighting designed for humans may not be appropriate for animal species. The commonly used "A" frequency weighting (ANSI S1.4-1983) attenuates noise energy according to human hearing range and sensitivity. For human response to blast noise, "C" frequency weighting is often applied to received blast noise signals, rather than "A" weighting

which is more representative of human hearing response (ANSI S1.4-1983). This is done to retain low frequency energy that, while not heard by humans, causes a secondary rattle in buildings which does evoke response (ANSI S12.4-1986). This is not appropriate for wildlife. An audiogram, which describes hearing range and sensitivity, provides guidance regarding appropriate frequency weighting for the species of interest and also aids in interpretation of noise response data. Figure 7 shows a composite average audiogram of seven orders of birds, with an approximate representation of a human audiogram and the "A" weighting curve included for comparison. The differences are substantial. The "owl" audiogram further illustrates how audiograms can vary among species. We searched the literature and consulted several leading experts on bird hearing without finding an audiogram for the RCW or for any species in RCW's order, Piciformes. Thus, as part of this project we will obtain an audiogram that will be used to develop a frequency weighting function that is appropriate for woodpeckers. Information on the current RCW audiogram work can be found in Pater et al. (1999). It is well-established (ANSI S12.40-1990; S12.9-1996; S12.17-1996; Homans 1974; NAS 1977, 1981; Rice 1983; Rice et al. 1986; Schomer et al. 1994) that the appropriate metric for blast noise is SEL, which is essentially the time integral of the square of the acoustic pressure. We measured blast noise as unweighted 1/3-octave band SEL, to which frequency weighting appropriate for the RCW will be applied (when available from the audiogram portion of this study, described in Appendix B) to obtain appropriately weighted overall levels. The same metric and procedure was also used with small arms noise (Buchta 1990; Hede and Bullen 1982; Hoffman et al. 1985; Luz 1982; Sorenson and Magnusson 1979; Vos 1995). Two metrics, the SEL and the maximum 1-second equivalent average (LEQ) level, were used for helicopter noise, airplane noise, and vehicle pass-by noise, since both are meaningful in terms of correlation with response (Environmental Protection Agency [EPA] 1974, 1982; Federal Interagency Committee on Urban Noise [FICUN] 1980; Fidell et al. 1991; Schomer 1994; Schultz 1978; U.S. Code of Federal Regulations 1980). Ambient noise was measured as LEQ for various appropriate time periods (EPA 1982). In all cases, the noise signals were recorded on digital audio tapes and preserved for possible further analysis.

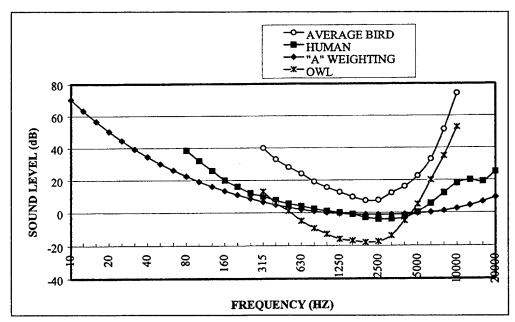


Figure 7. Examples of audiograms and frequency weighting.

#### **Statistical Data Analysis**

We used SPSS 8.0 for Windows (SPSS Inc. 1998) to perform all descriptive statistics; for example, one-way ANOVA for comparing the mean number of eggs, nestlings, and young fledged between the first through third nesting attempts. Independent sample *t*-tests were used to compare nest productivity data between experimental and control sites. Whenever appropriate, multiple observations at single nests were averaged before inferential tests were performed so that the sample sizes are the number of nests examined. We used a one-tailed Fisher Exact Test to assess 2x2 contingency tables for variability in nesting success between disturbed and undisturbed nest sites (Zar 1984). Alpha levels of 0.05 will be required to reject a null hypothesis for all tests. Means ± standard error (SE) are presented throughout this document.

# 4 Results

#### **Initiation Dates for each Nesting Phase**

The first woodpecker clutches were initiated on approximately 13 April through 16 May, while secondary clutches (clusters that renested after initial nest failure) were initiated on 3 May through 14 June. Third clutches were initiated on 16 May through 23. Eggs from initial nesting attempts hatched on approximately 23 April through 26 May, while nests from second nesting attempts hatched on 13 May through 24 June. Third nesting attempts hatched on approximately 5 June through 3 July. We observed young fledging from initial nesting attempts on 22 May through 21 June, and from 8 June through 20 July for fledglings from secondary nesting attempts. Third nesting attempts fledged on approximately 21 June through 9 July.

#### **Overall Population Dynamics**

Of the 198 potential breeding pairs on Fort Stewart, 165 nested during the 1999 nesting season (83.3 percent). This was a 20 percent increase over the number of potential breeding pairs (165) and a 17 percent increase in the number of clusters that nested (141) on Fort Stewart in 1998. Of the clusters that nested, 86.1 percent fledged young successfully. Thirty-three of the 47 clusters that initially failed to nest were found renesting within the following 2 weeks, with 72.7 percent of these sites successfully fledging young. Clusters that renested were found to be as successful (Fisher Exact Test, P = 0.15; 72.7 percent for sites that renested versus 70.2 percent for initial nesting attempts) and productive as sites that nested only once. We observed no statistically significant difference in number of eggs ( $F_{2200} = 0.98$ , P = 0.38), nestlings ( $F_{2202} = 0.64$ , P = 0.53), or the number of young fledged ( $F_{2,199} = 1.20$ , P = 0.30) between sites that renested and those that nested only once. We then pooled these data to determine mean rates for the overall population. Mean clutch size for RCW nests was  $2.75 \pm 0.07$ eggs/nest; mean brood size was 2.22 ± 0.07 nestlings/nest; and the number of young fledged was  $1.76 \pm 0.08$  young/occupied nest  $(2.04 \pm 0.07$  young/successful nest). Occupied nests include sites that are successful as well as sites that are not. Successful nests include only those sites that are successful in fledging young. Approximately 290 young fledged from RCW nest sites during 1999, with

53.0 percent of those young being male. There was a 35.9 percent decline in the reproductive potential of RCW nests from the incubation phase to the nestling phase (P < 0.001). The decline was not as dramatic from the nestling phase to the fledgling phase (16.9 percent), but was still significant (P = 0.04). Overall, we observed a significant decline of 53.2 percent in the reproductive potential from incubation through the fledgling phase  $(F_{2.492} = 61.8, P < 0.001)$ . Of the 23 clusters that failed to produce young during 1999, it appears as if at least one site failed due to nest predation by a rat snake (*Elaphe obsoleta*), while a second nest may have been lost to southern flying squirrels (*Glaucomys volans*). In another case, a rat snake was taken by Fort Stewart Fish and Wildlife personnel from a cluster that had produced a second clutch. The snake later passed identification bands for the young of that cluster confirming that it had consumed the nestlings. Two other sites had partial brood loss due to flooding of the nest cavity.

#### **Sample Cluster Population Dynamics**

As was the case for the population as a whole, the project sample clusters that renested after initial nest failure were as successful and productive as sites that nested only once. Therefore, data were pooled before determining overall sample group fitness rates. Disturbed and undisturbed nest sites did not differ significantly in the number of eggs ( $F_{1,72}$  = 1.65, P = 0.20), number of nestlings ( $F_{1,72}$  = 3.52, P = 0.07), or number of young fledged ( $F_{1.72} = 3.09$ , P = 0.08). Forty-two of the 48 disturbed RCW nest sites were successful in producing an average of 3.47  $\pm$  0.16 eggs/nest, 2.27  $\pm$  0.16 nestlings/nest, and 1.84  $\pm$  0.16 young/occupied nest  $(2.14 \pm 0.14 \text{ young/successful nest})$ , while 23 of 25 undisturbed sites were successful in producing an average of 3.56 ± 0.31 eggs/nest, 2.28 ± 0.17 nestling/nest, and 1.80 ± 0.17 young/occupied nest (1.96 ± 0.15 young/successful nest). The number of disturbed sites that successfully nested was not significantly different from undisturbed sites (Fisher Exact Test, P > 0.05). For disturbed sites, 8 of the 48 nesting attempts were second attempts. One disturbed site produced and successfully fledged a second clutch, though experimental testing was only done during the first clutch. For undisturbed sites, 8 of 25 nesting attempts were second attempts. The number of disturbed cluster sites that renested was not significantly different from undisturbed sites (Fisher Exact Test, P > 0.05). One undisturbed site attempted to nest for a third time, but did not successfully fledge young. We found no difference in the reproductive success (Fisher Exact Test, P > 0.05) or productivity ( $F_{1.47} = 2.49$ , P = 0.12) for RCW cluster sites exposed with artillery simulator blast noise versus sites that received .50-caliber blank fire.

#### **Noise and Response Monitoring Summary**

During the 1999 field season we documented RCW response to experimental noise from controlled artillery simulators and .50-caliber blank fire. Passive noise from large-caliber live fire (25-mm M2A2 Bradley Fighting Vehicles, 120-mm M1A1-Tanks, and 155-mm M109 Howitzers), grenade simulators, small-arms live fire (5.56 mm M-16 and Saw, 7.62-mm, and .50-caliber machine guns), and military helicopters was recorded as it occurred. Passive noise was monitored during all nesting phases, while experimental tests were performed only during the incubation and early portions of the brooding phase when adults were present at the nest for extended periods of time.

We made noise measurements and behavioral response observations at a total of 48 experimental and 14 passive sample clusters (9 of the 14 passive sample clusters were also used in experimental testing). Detailed results are described below and are presented in the data tables and figures in Appendices B, C, and D. The tables of Appendix B present summaries of the noise level measurements and RCW responses. A typical spectrum for the most prevalent noise sources is presented in Appendix C. Appendix D presents noise level summaries for each noise stimulus type and detailed noise measurements in terms of one-third-octave-band SEL levels. These are the data to which future adjustments for cavity resonance and woodpecker frequency weighting will be applied to obtain single-number overall noise levels. We also made behavioral observations at a total of 25 undisturbed sample clusters for the purpose of obtaining a baseline against which to judge proximate response at the disturbed clusters.

#### Passive Monitoring

We recorded 691 passive noise events in 34 data sessions at 14 RCW clusters during the 1999 nesting season. Small-arms live fire events (M-16 rifles) were recorded most frequently, followed by large-caliber live fire events (greater than 20 mm in diameter), helicopters, and grenade simulators. Multiple noise events and stimulus types were usually recorded during each data session. Stimulus type, frequency, and noise level varied for each cluster and are shown in the tables of Appendix B.

#### **Experimental Testing**

We conducted 105 experimental tests at 48 cluster sites (24 for each noise type) during the 1999 nesting season (Tables B1 and B2, Appendix B).

#### Noise Measurement Testing

In addition to recording noise levels at the base of active RCW nest sites, we also measured noise levels in nest cavities before or after the nesting season. Both natural and artificial cavities were tested in 1999. Nest cavities were found to act as sound resonators, emphasizing the 125 to 250-Hz portion of the frequency band, and varying by individual tree. In the examples presented in Figures C1 and C2 (Appendix C), artillery simulators and .50-caliber blank fire events had maximum spectral noise levels 13 and 13.1 dB louder, respectively, inside the nest cavity compared with recordings for the same events measured at the base of the nest tree.

#### **Distance and Noise Level Thresholds for Response**

#### Experimental Tests

#### **Artillery Simulators**

As stimulus distance decreased, RCWs flush frequency increased (Figure 8), regardless of stimulus type (Tables B1 and B2). RCWs did not flush when artillery simulator blasts were ≥ 244 m away from nest sites and SEL noise levels < 84 dBA (89 dB, unweighted). Only one flush response was documented at a distance of 122 m. RCWs returned to their nests on average within 4.6 minutes after being flushed, while returning no later than 10 minutes overall (Figure 9). Data collection during the 2000 field season will emphasize the distance between 122 and 244 m to better develop the distance and noise thresholds for RCW response, as well as replicate those distances tested during the 1999 season.

#### .50-Caliber Blank Fire

Similarly, we only recorded one flush response due to .50-caliber blank fire at 122 m. We attempted to test RCW response to .50-caliber blank fire at distances > 122 m, but due to weather and other logistical constraints we were not able to develop a distance-response threshold for the cluster that flushed at 122 m. Data collection during the 2000 field season will emphasize this distance. Blank fire testing consistently elicited higher response rates than artillery simulators at similar distances (Figure 8). At distances  $\leq 122$  m, .50-caliber blank fire elicited a significantly greater flush response (49.1 percent) than comparably distance artillery simulators (31.3 percent; Fisher's Exact Test: P < 0.05, Appendix B: Tables B1 and B2).

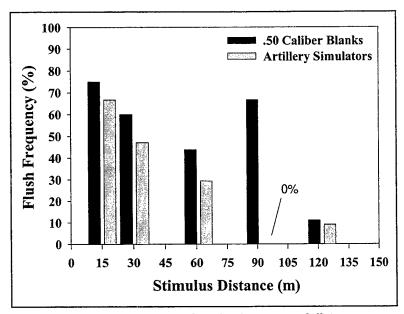


Figure 8. RCW flush frequency by stimulus type and distance.

RCWs flushed only once when .50-caliber blanks were fired at distances of 122 m from nest sites and did not flush when SEL noise levels were < 72 dBA (82 dB, unweighted). Ambient sound levels were substantially lower than experimental noise events during all tests. On average, RCWs returned to their nests within 6.3 minutes after being flushed (within 12 minutes overall; Figure 9). Data collection during the 2000 field season will emphasize areas greater than 122 m to develop the distance and noise thresholds for RCW response, as well as replicate those distances tested during the 1999 season.

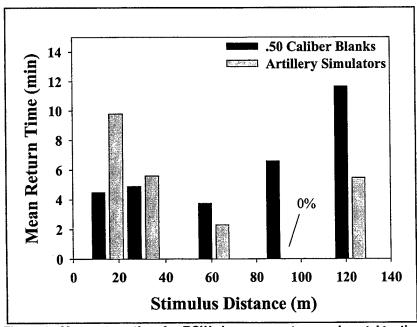


Figure 9. Mean return time for RCWs in response to experimental testing.

#### Passive Events

#### **Small-Caliber Live Fire**

There was only one RCW nest site, cluster 103, that received small-caliber live fire noise at distances less than 400 m. Noise levels at cluster 103 were louder than other clusters due to supersonic bullet noise ("sonic boom") and ricocheting bullets from an M-16 range (Small Arms — Golf) hitting trees in close proximity to the nest tree. The two other clusters monitored for passive noise in the Small Arms Impact Area (clusters 3 and 25) were between ranges and much further downrange than cluster 103 and therefore received lower noise levels. These sites were monitored remotely during firing periods via video camera and audio recording equipment.

RCWs did not appear to flush in response to small-caliber noise at cluster 103, but their flight activities may have been influenced. On 3 separate days, over a 6-day period, RCWs were only observed arriving and departing from the nest during inactive periods at the range (Figures 10 through 12). Data points for Figures 10 through 12 represent individual bullet noise events or groups of muzzle blast events that were separated in time from other shots. Red lines represent times when RCWs returned to the nest and blue lines represent times that birds departed the nest. Noise levels from bullet "sonic booms" and ricocheting bullets were substantially louder than rifle muzzle noise coming from the range (Figure 13). Further analysis will reveal whether the "bullet noise" is due to sonic booms and/or bullets impacting trees. When we compared the frequency spectra for muzzle blast noise versus bullet noise we found that most of the noise energy for muzzle blast noise occurred at 630 Hz, while the bullet noise occurred at higher frequency levels, around 1600 to 2000 Hz. Bullet noise is identified on Figures 10 through 12 by the similarities between the unweighted and "A" weighted noise levels, and account for all data points above 78 dB. "A" weighted noise levels were very close to their corresponding unweighted noise levels. Bullet noise reached levels 30 dB louder than muzzle blast noise within the 1600 to 2000 Hz range and around 15 dB louder when peak levels for both noise events were compared (Figure 13). Bullet noise represented 15.6 percent (102 noise events, Table B3) of the noise events that were documented at cluster 103. Cluster 103 successfully fledged two young in 1999.

Overall, RCWs did not flush when small-arms live fire was more than 400 m from active nest sites and SEL noise levels were < 77 dBA (79 dB, unweighted; Appendix B, Table B3). Small-arms live fire events < 100 m did not represent shots from rifles themselves, but were from bullet noise. We were not able to determine the exact distances that bullets were hitting surrounding trees, but due

termine the exact distances that bullets were hitting surrounding trees, but due to the received noise levels and the fact that we have seen bullets lodged in nearby trees, distances appear to be relatively close. Rifle noise from Small Arms — Golf M-16 range was approximately 430 m from the nest. We did not locate any other active RCW nest sites < 400 m from any small arms ranges to which we had access for testing purposes.

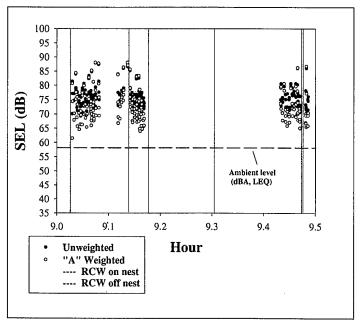


Figure 10. Noise levels from M-16 live fire events at cluster 103 on May 12, 1999.

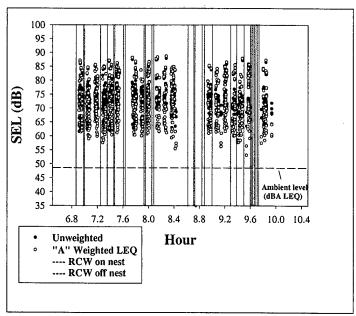


Figure 11. Noise levels from M-16 live fire events at cluster 103 on May 13, 1999.

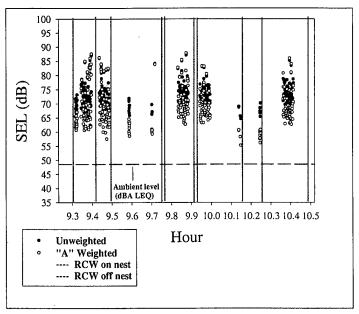


Figure 12. Noise levels from M-16 live fire events at cluster 103 on May 13, 1999.

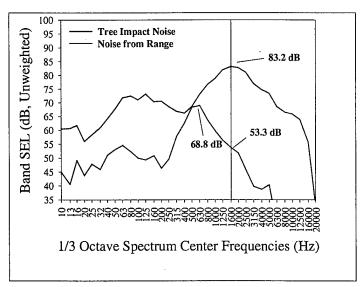


Figure 13. SEL weighting comparison for M-16 live fire on May 17, 1999, from range and tree impact noise near a RCW nest site.

#### **Grenade Simulators**

RCWs flushed once during eight grenade simulator blasts recorded during passive noise events. This flush event occurred during a realistic training maneuver when a grenade simulator was detonated approximately 100 m from the nest (Figure C3, Appendix C). A bird was observed returning to the nest within 8 minutes after the flush had occurred (this site was successful in fledging one young). Overall, RCWs did not flush when grenade simulators were detonated ≥ 200 m from nest sites and SEL noise levels were < 84 dBA (91 dB, unweighted;

Appendix B, Table B4). We did not record any grenade simulators < 100 m or between 100 and 200 m and therefore could not test for response within those ranges.

#### Helicopters

RCWs did not flush when military helicopters were  $\geq$  100 m from nest sites and SEL noise levels were < 88 dBA (104 dB, unweighted; Appendix B, Table B5). Due to the low probability of encountering helicopters, we were unable to test for RCW response at distances < 100 m.

#### Large-Caliber Live Fire

Large-caliber live fire events on Fort Stewart were dramatically reduced from numbers documented in 1998, therefore our ability to record RCW responses to such passive noise events was also limited. The 1999 field season data show that RCWs did not flush when large-caliber guns were fired at distances  $\geq 700$  m from nest sites and SEL noise levels were < 85 dBA (103 dB, unweighted; Appendix B, Table B6). We did not record any large-caliber gun fire < 700 m from any active RCW nest site, therefore, we could not test for response within that range.

# 5 Discussion

#### **Nesting Success**

The preliminary findings, based on 1999 experimental testing data, suggest that measured levels of training noise did not affect RCW nesting success or productivity. We believe the small but nonsignificant decrease in reproductive success between disturbed (N=48) and undisturbed (N=25) sites was attributable to natural attrition inherent in the larger disturbed sample. Through further investigation over the next year we will be able to make more definitive conclusions regarding RCW fitness as a function of training noise.

#### Flush Response and Related Behaviors

#### Flush Response

The proportion of Red-cockaded Woodpeckers that flushed in response to experimental training noise was negatively related to stimulus distance. The dose-response relationship for RCWs based on flush frequency with distance and noise level indicated that .50-caliber blank fire elicited a greater response than artillery stimulators. RCWs apparently perceive artillery simulators as less threatening than .50-caliber blank fire because of their shorter duration (total event duration), minimal visibility, and lessened association with human activity. It is possible that disturbances in closer proximity to an RCW's location may also be more visible and therefore elicit a greater response than a disturbance farther away, regardless of noise level. It is important to consider all aspects of a stimuli when examining an animal's response to a disturbance. Although season and nesting phase influence avian response to disturbance (Thiessen 1957; Knight and Temple 1986; Delaney et al. 1999), habituation, prior experience, and animal temperament are important factors that should be taken into account (Hart 1985; Manci et al. 1988).

RCWs flushed infrequently in response to passive military training noise during the 1999 nesting season. Most of the passive noise events that we recorded were distant and had relatively low noise levels. Woodpeckers returned to their nests relatively quickly after being flushed. Return times by RCWs were comparable with times reported for bird species in other noise disturbance studies (Awbrey and Bowles 1990; Holthuijzen et al. 1990), and were comparable with 1998 RCW response data (Pater et al. 1999). The amount of time that an attending adult is away from the nest has important consequences when we consider the role that nest predation and nest competition has on this species. There are a number of species that are capable of usurping nesting cavities from the RCW. Both redbellied woodpeckers (Melanerpes carlinus) and red-headed woodpeckers (Melanerpes erythrocephalus) have been shown to remove and eat eggs, usually in the process of usurping the cavity from the RCW. Southern flying squirrels (Glaucomys volans) have also been documented to eat eggs or young when competing with RCWs for nest cavities (Jackson 1994).

#### **Nesting Behaviors**

Through audio and video surveillance it appears that noise from Small Arms — Golf may have influenced RCW behavior at cluster 103 during the 1999 nesting season. RCWs were not observed arriving or departing from the nest during the nestling phase when the range was firing, only during inactive periods. It is possible that small arms fire from the range is influencing the timing, frequency, and duration of RCW flights from the nest. Noise levels for that range were louder than other comparably distant ranges due to the orientation of the rifles and because of bullet noise from sonic booms and ricocheting bullets. We are currently analyzing the remainder of the video data to determine if nest attentiveness, trip frequency, timing, and duration, or the number of prey deliveries are influenced by experimental or passive training activities on Fort Stewart.

We did not observe any nest abandonment relative to camera use. Birds were observed using camera trees for foraging and perch sites when coming and going from the nest tree.

#### **Distance and Sound Thresholds**

Despite the aggressive nature of our testing regime (i.e., close proximity and repeated exposure), RCW behavioral responses were minimal when experimental stimuli were  $\geq 122$  m away. We did not observe RCWs flushing from the nest when noise stimuli were  $\geq 244$  m away. Stimulus distances > 122 m will be tested in more detail during the 2000 field season for the development of more definitive distance and sound thresholds based on RCW response parameters. A similar pattern was present during passive disturbances. We observed no flush responses by RCWs when passive stimuli were  $\geq 200$  m away. Due to the varied nature and location of maneuver training activities on Fort Stewart, it is highly

unlikely that woodpeckers would receive as much disturbance activity during the nesting season within any year as the experimentally disturbed RCW sites received during this year's study.

An examination of the data presented in Appendices B and D reveals a wide range of received noise levels at a given distance. One reason is that different types of noise sources of course have different acoustic emissive power. For a given noise source, received noise level also depends on differences in propagation conditions, a result of differences in atmospheric wind and temperature structure. It is well known that at distances of several kilometers, received noise level can vary by as much as 20 dB above and below the mean due to changes in meteorological conditions (Embleton 1982; Li et al. 1994; Larsson and Israelsson 1991; Pater 1981; Piercy et al. 1977; White and Gilbert 1989; White et al. 1993). Differences in received noise level can also be due to orientation of the weapon relative to the receiver. Many weapons exhibit substantial directivity; some as much as 15 dB louder downrange (Pater 1981; Pater et al. (DRAFT); Schomer et al. 1976a and 1976b [Vol I and II]; Schomer et al. 1979; Schomer et al. 1981; Schomer 1982; Schomer 1984; Schomer and Goebel 1985; Schomer 1986a, 1986b; Walther 1972). Some other important factors that should be taken into account are the orientation of the nest cavity relative to the noise source and any barriers between the noise source and the birds position.

#### **Noise Measurement Test**

Noise levels within RCW nest cavities were substantially louder than noise levels recorded at the base of the nest tree. Due to differences in cavity and weapon orientation, presence or absence of barriers, and weapon directivity, we were not able to extrapolate noise levels recorded at the base of the tree to received levels within RCW nest cavities. Noise measurements will therefore have to be taken inside each nest cavity before or after the nesting season for each noise source to determine the noise levels that birds may actually be experiencing. We will investigate this in more detail in 2000. We will also continue testing for differences between artificial and natural cavities during the 2000 field season. Data comparing natural and artificial cavities are currently being analyzed to determine if there is a variation in the resonant frequency of the nest trees and if there are any differences in the noise level or duration of the noise event from comparably distant stimulus events.

## 6 Plans and Conclusions

#### **Plans**

The results of the second year of this project have shown that the basic technical approach is appropriate and effective. The primary need is for more data, which we will collect during the 2000 field season by replicating the research protocol from 1999. In particular, we will obtain more data for experimental manipulations and passive disturbance events, such as small arms blanks, artillery, and helicopters. We will search for reproductively active clusters that are located in areas that will fill in the blanks in the data in terms of stimulus distance and noise level.

The matter of cavity resonance effect on the noise level perceived by the RCWs will continue to be investigated. We cannot measure noise levels in the cavity being used by an endangered species during the nesting season; therefore, we will make cavity measurements during pre- and post-nesting periods. The investigation of woodpecker hearing is beginning to return useful results; the current effort will be continued. An expanded effort may be appropriate.

One aspect of the technical approach that has not yet been executed is to use available noise models and training activity data to calculate noise dose for each cluster, and to examine these data for correlation with nesting success data. Fort Stewart installed the updated version of the Range Facility Management Support System (RFMSS) early in 1998. This system includes detailed data regarding training activity. These data will be used in 2000 to examine said correlation.

#### **Conclusions**

During the second year of this study of the impacts of training noise on the RCW, we observed and documented experimental training noise events and the resulting RCW responses under realistic conditions. We measured both proximate response behavior and nesting success. We also observed RCW behavior and nesting success at clusters where noise stimuli were absent or minimal (near or below ambient sound levels), to provide an undisturbed behavior baseline

against which to judge response and impact. No significant difference in nesting success was found between experimentally disturbed and relatively undisturbed nest sites. The second year data are limited in number and statistical power and are not sufficient to make strong conclusions or to establish reliable noise doseresponse relations or thresholds. The results are however sufficient to confirm that the project technical approach is appropriate and needs only minor revision, and that the project objectives will be achieved.

### References

- Anderson, D.E., O.J. Rongstad, and W.R. Mytton. 1989. "Response of nesting red-tailed hawks to helicopter flights." *Condor* 91:296-299.
- ANSI, American National Standards Institute S1.1-1994, "American National Standard: Acoustical Terminology," 1994.
- ANSI, American National Standards Institute S1.4-1983, "American National Standard Specification for Sound Level Meters," 1983.
- ANSI, American National Standards Institute S12.17-1996, "Impulse Sound Propagation for Environmental Noise Assessment," August 1996.
- ANSI, American National Standards Institute S12.40-1990, "Sound Level Descriptors for Determination of Compatible Land Use," 1990.
- ANSI, American National Standards Institute S12.4-1986, "American National Standard Method for Assessment of High-Energy Impulsive Sounds with Respect to Residential Communities," 1986.
- ANSI, American National Standards Institute S12.9-1996, "Quantities and Procedures for Description and Measurement of Environmental Sound Part 4: Noise Assessment and Prediction of Long-term Community Response," September 1996.
- Awbrey, F.T., and A.E. Bowles. 1990. The effects of aircraft noise and sonic booms on raptors: a preliminary model and a synthesis of the literature on disturbance. Noise and Sonic Boom Impact Technology, Technical Operating Report 12. Wright-Patterson Air Force Base (AFB), OH.
- Beaty, T.A. 1986. Response of Red-cockaded Woodpeckers to habitat alteration. Directorate of Engineering and Housing, Fish and Wildlife Section, Fort Stewart, GA.
- Bowles, A.E. 1995. "Responses of wildlife to noise." Pages 109-156 in R.L. Knight and K.J. Gutzwiller, editors. Wildlife Recreationists, Island Press, Washington, DC.
- Bowles, A.E., F.T. Awbrey, and R. Kull. 1990. "A model for the effects of aircraft overflight noise on the reproductive success of raptorial birds." Noise and Sonic Boom Impact Technology, Inter-Noise 90. Wright-Patterson AFB, OH.
- Buchta, E. 1990. "A field survey of annoyance caused by sounds from small firearms," J. Acoust. Soc. Am., 88, 1459-1467.
- Carrier, W.D., and W.E. Melquist. 1976. "The use of a rotor-winged aircraft in conducting nesting surveys of ospreys in northern Idaho." J. Raptor Res. 10:77-83.

Charbonneau, D., L. Swindell, E.J. Moore, T.A. Beaty, and A. Eaton. 1983. "Preliminary report of the effects of forage habitat reduction on Red-cockaded Woodpecker reproduction in the CALFAX Range Facility at Ft. Stewart, Georgia." Directorate of Engineering and Housing, Fish and Wildlife Section, Fort Stewart, GA.

- Costa, R. 1992. "Challenges for recovery," pp 37-44 in *Proceedings from Sandhills Red-cockaded Woodpecker conference*. D.J. Case and Assoc., Mishawaka, Inc.
- Craig, T.H., and E.H. Craig. 1984. "Results of a helicopter survey of cliff nesting raptors in a deep canyon in southern Idaho." *Journal of Raptor Research* 18:20-25.
- Delaney, D.K., T.G. Grubb, and D.K. Garcelon. 1998. "An infrared video camera system for monitoring diurnal and nocturnal raptors." J. Raptor. Res. 33:290-296
- Delaney, D.K., T.G. Grubb, P. Beier, L.L. Pater, and M.H. Reiser. 1999. "Effects of helicopter noise on Mexican Spotted Owls." *Journal of Wildlife Management* 63:60-76.
- Devlin, W.J., J.A. Mosher, and G.J. Taylor. 1980. "History and present status of the Red-cockaded Woodpecker in Maryland." Am. Birds 34:314-316.
- Edwards, R.G., A.B. Broderson, R.W. Barbour, D.F. McCoy, and C.W. Johnson. 1979. Assessment of the environmental compatibility of differing helicopter noise certification standards. Final Report for the Department of Transportation, WA. Report #FAA-AEE-19-13. Contract #78419000000000.
- Ellis, D.H. 1981. Responses of raptorial birds to low level military jets and sonic booms: Results of the 1980-81 Joint U.S. Air Force-U.S. Fish and Wildlife Service Study. Institute for Raptor Studies Report NTIS ADA108-778.
- Ellis, D.H., C.H. Ellis, and DP. Mindell. 1991. "Raptor responses to low-level jet aircraft and sonic booms." Environmental Pollution 74:53-83.
- Embleton, T. 1982. "Sound Propagation Outdoors Improved Prediction Schemes for the 80's," Noise Control Engineering Journal, 18/1, 30-39.
- EPA. 1974. Information on Levels of Environmental Noise Requisite to Protect Health and Welfare with an Adequate Margin of Safety, U.S. Environmental Protection Agency, Report No. 550/9-74-004, March 1974.
- EPA. 1982. Guidelines for Noise Impact Analysis, U.S. Environmental Protection Agency, Report No. 550/9-891-105, April 1982.
- FICUN. 1980. Federal Interagency Committee on Urban Noise, Guidelines for Considering Noise in Land Use Planning and Control.
- Fidell, S. et al. 1991 "Revision of a Dosage Effect Relationship for the Prevalence of Annoyance Due to General Transportation Noise," J. Acoust. Soc. Am., 89, 221-233.
- Fort Stewart Endangered Species Management Planning Team. 1998. Endangered Species Management Plan. 116 pages.

- Fraser, J.D., L.D. Frenzel, and J.E. Mathisen. 1985. "The impact of human activities on breeding bald eagles in north-central Minnesota." *Journal of Wildlife Management* 49:585-592.
- Fyfe, R.W., and R.R. Olendorff. 1976. "Minimizing the dangers of studies to raptors and other sensitive species." Canadian Wildlife Service Occasional Paper 23.
- Grubb, T.G. and R.M. King. 1991. "Assessing human disturbance of breeding bald eagles with classification tree models." *Journal of Wildlife Management* 55:501-512.
- Grubb, T.G., and W.W. Bowerman. 1997. "Variations in breeding bald eagle response to jets, light planes, and helicopters." *Journal of Raptor Research* 31:213-222.
- Hart, B.L. 1985. The behavior of domestic animals. W.H. Freeman, New York, New York, USA.
- Hayden, T.J. 1997. Biological assessment of the effects of the proposed revision of the 1994 management guidelines for the Red-cockaded Woodpecker on Army installations. Special Report (SR) 97/48, ADA322086 (U.S. Army Construction Engineering Research Laboratory [CERL] January 1997).
- Hede and Bullen. 1982. "Community reaction to noise from a suburban rifle range," Journal of Sound and Vibration, 82, 39-49.
- Hoffman, R., A. Rosenheck, and U. Guggenbuehl. 1985. Assessment Procedure for Rifle Firing Noise from 300 Meter Facilities, EMPA Department for Acoustics and Noise Abatement, Swiss Federal Office for Environmental Protection, February 1985.
- Hohman, W.L. 1986. "Incubation rhythms of Ring-necked Ducks." Condor 88:290-296.
- Holland, E.D. 1991. "The environment can ground training." Naval Proceedings, October 1991: 71-75.
- Holthuijzen, A.M.A., W.G. Eastland, A.R. Ansell, M.N. Kochert, R.D. Williams, and L.S. Young. 1990. "Effects of blasting on behavior and productivity of nesting prairie falcons." Wildlife Society Bulletin 18:270-281.
- Homans, B. 1974. User Manual for the Acquisition and Evaluation of Operational Blast Noise Data, CERL TR E-42, AD782911, June 1974.
- Jackson, J.A. 1978. "Analysis of the distribution and population status of the Red-cockaded Woodpecker," pp 101-111 in R.R. Odum and L. Landers, eds. Proceedings of the rare and endangered wildlife symposium. Georgia Dep. Nat. Res., Game Fish Div., Tech Bull., WL 4.
- Jackson, J.A. 1983. "Possible effects of excessive noise on post-fledging Red-cockaded Woodpeckers," pp 38-40 in D.A. Wood, ed. Red-cockaded Woodpecker symposium II proceedings, Florida Game Fresh Water Fish Commission, Tallahassee, FL.
- Jackson, J.A. 1987. "The Red-cockaded Woodpecker," pp 479-493 in R.L. DiSilvestro, ed. Audubon wildlife report 1987, Academic Press, New York.

Jackson, J.A. 1994. "Red-cockaded woodpecker (*Picoides borealis*)," pp 1-19 in A. Poole and F. Gill, eds. *The Birds of North America*, No. 85. The Academy of Natural Sciences, Washington, DC, The American Ornithologists Union.

- Jackson, J.A., and S.D. Parris. 1995. "The ecology of Red-cockaded Woodpeckers associated with construction and use of a multi-purpose range complex at Ft. Polk, Louisiana," pp 277-282 in D.L. Kulhavy, R.G. Hooper, and R. Costa, eds. Red cockaded Woodpecker: recovery, ecology, and management. Center for Applied Studies in Forestry, College of Forestry, Stephen F. Austin State University, Nacogdoches, TX.
- Jordan, R.A., K.S. Wheaton, and W.M. Weiher. 1995. Integrated endangered species management recommendations for Army Installations in the Southeastern United States: Assessment of the potential effects of Army-wide management guidelines for the Red-cockaded Woodpecker on associated endangered, threatened, and candidate species. Final Report, The Nature Conservancy Southeast Regional Office, North Carolina.
- Jordan, R.A., K.S. Wheaton, W.M. Weiher, and T.J. Hayden. 1997. Integrated endangered species management recommendations for Army Installations in the Southeastern United States. CERL SR 97/94, ADA286931 (CERL, June 1997).
- Knight, R.L., and S.A. Temple. 1986. "Why does intensity of avian nest defense increase during the nesting cycle?" Auk 103:318-327.
- Larsson, C., and S. Israelsson. 1991. "Effects of Meteorological Conditions and Source Height on Sound Propagation near the Ground," Applied Acoustics 33 (1991), 109-121.
- Lawrence, G.N. 1867. "Catalogue of birds observed in New York, Long and Staten Islands and the adjacent parts of New Jersey," Annual Lyceum of the Natural History of New York 8:279-300.
- Lennartz, M.R., P.H. Geissler, R.F. Harlow, R.C. Long, K.M. Chitwood, and J.A. Jackson. 1983. "Status of the Red-cockaded Woodpecker on federal lands in the south," pp 7-12 in D.A. Wood, ed. *Red-cockaded Woodpecker symposium II Proceedings*. Florida Game Fresh Water Fish Commission, Tallahassee, FL.
- Li, Y.L., M.J. White, and S.J. Franke. 1994. "New fast field programs for anisotropic sound propagation through a wind velocity profile," J. Acoust. Soc. Am. 95, 718-726, February 1994.
- Luz, G. 1982. "An improved procedure for evaluating the annoyance of small arms ranges," J. Acoust. Soc. Am., 72, Suppl. 1, S26.
- Manci, K.M., D.N. Gladwin, R. Villella, and M.G. Cavendish. 1988. Effects of aircraft noise and sonic booms on domestic animals and wildlife: a literature synthesis. U.S. Fish and Wildlife Service Technical Report NERC 88.
- McGarigal, K., R.G. Anthony, and F.B. Isaacs. 1991. "Interactions of humans and bald eagles on the Columbia River estuary." Wildlife Monograph 115:1-47.
- NAS, National Academy of Sciences. 1977. Committee on Hearing, Bioacoustics, and Biomechanics, Working Group 69 Report, Guidelines for Preparing Environmental Impact Statements on Noise.

- NAS, National Academy of Sciences. 1981. Committee on Hearing, Bioacoustics, and Biomechanics, Working Group 84 Report, Assessment of Community Response to High-Energy Impulsive Sounds.
- Pater, L. 1981. Gun Blast Far Field Overpressure Contours, Naval Surface Weapons Center, TR-79-442, March 1981.
- Pater, L., Walter Alvendia, Raman Yousefi, and James Wilcoski. DRAFT. "Acoustic Spectral Emission Data for Several Small Weapons," Draft CERL Technical Report.
- Pater, L.L., D.K. Delaney, and T.J. Hayden. 1999. Assessment of training noise impacts on the Red-cockaded Woodpecker: Preliminary results. CERL Technical Report (TR) 99/51(CERL, June 1999).
- Piercy, J.E., T. Embleton, and L. Sutherland. 1977. "Review of Noise Propagation in the Atmosphere," J. Acoust. Soc. Am., 61, 1403-1418, June 1977.
- Platt, J.B. 1977. "The breeding behavior of wild and captive gyrfalcons in relation to their environment and human disturbance." Ph.D. dissertation. Cornell University, Ithaca, NY.
- Rice, C. 1983. "CEC Joint Research on Annoyance due to Impulse Noise: Laboratory Studies," Noise as a Public Health Problem: Proceedings of the Fourth International Congress, Volume 2, G. Rossi, Editor, Cetnro Ricerche E Studi Amplifon, Milan, Italy, pp 1073-1084.
- Rice, C., I. Flindell, and J. John. 1986. "Annoyance due to Impulse Noise: Laboratory Studies, Final Report, CEC Third Programme, Phase 2, 1984-85," Contract Report 86/13, Institute of Sound and Vibration Research, University of Southampton, July 1986.
- Schomer, P. 1994. "New Descriptor for High-Energy Impulsive Sounds," *Noise Control Eng. J.* 42(5), 179-191.
- Schomer, P.D. 1982. Acoustic Directivity Patterns for Army Weapons: Supplement 1, CERL TR N-60, ADA121665, September 1982.
- Schomer, P.D. 1984. Acoustic Directivity Patterns for Army Weapons: Supplement 2, CERL TR N-60, ADA145643, August 1984.
- Schomer, P.D. 1986a. Acoustic Directivity Patterns for Army Weapons: Supplement 4: The Multiple Launch Rocket System, CERL TR N-60, ADA166490, February 1986.
- Schomer, P.D. 1986b. "High-energy Impulsive Noise Assessment," J. Acoust. Soc. Am., 79(1), 182-186, January 1986b.
- Schomer, P.D., and S.S. Goebel. 1985. Acoustic Directivity Patterns for Army Weapons: Supplement 3: The Bradley Fighting Vehicle, CERL TR N-60, ADA155219, April 1985.
- Schomer, P.D., D. Effland, V. Pawlowska, and S. Roubik. 1981. Blast Noise Prediction Volume 1: Data Bases and Computational Procedures, CERL TR N-98, ADA099440, March 1981.

- Schomer, P.D., L. Wagner, L. Benson, E. Buchta, K.-W. Hirsch, and D. Krahe. 1994. "Human and community response to military sounds: Results from field-laboratory tests of small-arms, tracked-vehicle, and blast sounds," *Noise Control Engineering Journal*, Vol 42, 71-84.
- Schomer, P.D., L.M. Little, and A.B. Hunt. 1979. Acoustic Directivity Patterns for Army Weapons, CERL TR N-60, ADA066223, January 1979.
- Schomer, P.D., R.J. Goff, and L.M. Little. 1976a. The Statistics of Amplitude and Spectrum of Blasts Propagated in the Atmosphere Vol. I, CERL TR N-13, ADA033475, November 1976.
- Schomer, P.D., R.J. Goff, and L.M. Little. 1976b. The Statistics of Amplitude and Spectrum of Blasts Propagated in the Atmosphere Vol. II: Appendices C through E, CERL TR N-13, ADA033361, November 1976.
- Schultz, T.J. 1978. "Synthesis of Social Surveys on Noise Annoyance," J. Acoust. Soc. Am., 64, 377-405.
- Scott, J.M., S.A. Temple, D.L. Harlow, and M.L. Shaffer. 1994. "Restoration and management of endangered species," pp 531-539 in T.A. Bookhout, ed. Research and management techniques for wildlife and habitats. Fifth ed. The Wildlife Society, Bethesda, MD.
- Snyder, N.F.R., H.W. Kale II, and P.W. Sykes, Jr. 1978. An evaluation of some potential impacts of the proposed Dade County training jetport on the endangered Everglade Kite. FWS, Patuxent Wildl. Res. Cent., MD.
- Sorenson and Magnusson. 1979. "Annoyance caused by noise from shooting range," Journal of Sound and Vibration, 62, 437-442.
- SPSS, Inc. 1998. SPSS 8.0 for Windows: base, professional statistics, and advanced statistics. SPSS, Inc., Chicago, IL.
- Stalmaster, M.V., and J.L. Kaiser. 1997. "Flushing responses of wintering bald eagles to military activity." Journal of Wildlife Management 61:1307-1313.
- Steenhof, K., and M.N. Kochert. 1982. "An evaluation of methods used to estimate raptor nesting success." Journal of Wildlife Management 46:885-893.
- The Nature Conservancy (TNC). 1996. Effects of military training on the Red-cockaded Woodpecker. Final Report for Fort Benning Army Installation.
- Thiessen, G. 1957. "Acoustic irritation threshold of ring-billed gulls." Journal of Acoustical Society of America 29:1307-1309.
- U.S. Code of Federal Regulations. 1980. Title 14, Part 150. "Airport Noise Compatibility Planning."
- Vos, J. 1995. "A review of research on the annoyance caused by impulse sounds produced by small firearms," *Proceedings of INTER-NOISE 95: Vol 2, Noise Control Foundation*: New York, 875-878.

- Walters, J.R., P.D. Doerr, and J.H. Carter, III. 1988. "The cooperative breeding system of the red-cockaded woodpecker." *Ethology* 78:275-305.
- Walther, M.F. 1972. Gun Blast from Naval Guns, NWL Technical Report TR-2733, Naval Weapons Laboratory, August 1972.
- White, C.M., and T.L. Thurow. 1985. "Reproduction of ferruginous hawks exposed to controlled disturbance. *Condor* 87:14-22.
- White, M.J., and K.E. Gilbert. 1989. "Application of the parabolic equation to the outdoor propagation of sound," *Applied Acoustics* 27(3), 227-238.
- White, M.J., C.R. Shaffer, and R. Raspet. 1993. Measurements of Blast Noise Propagation over Water at Aberdeen Proving Ground, MD, CERL TR EAC-93/02, ADA280383, September 1993.
- Windsor, J. 1977. The response of Peregrine Falcons (Falco peregrinus) to aircraft and human disturbance. Mackenzie Valley Pipeline Investigations, Report for Environmental Social Programs. Canadian Wildl. Serv.
- Zar, J.H. 1984. Biostatistical Analysis. Prentice-Hall, Englewood Cliffs, New Jersey.

# Appendix A: Significant Legal Requirements

The Endangered Species Act (ESA) requires Federal agencies to carry out programs for the conservation of threatened and endangered species. Agencies are further required to ensure that their actions do not jeopardize the continued existence of listed species or result in the destruction or adverse modification of the critical habitat of these species. These requirements fall under provisions of Section 7 of the Act, which also requires agencies to conduct biological assessments to evaluate the impacts of their activities on listed species. This assessment serves as the primary basis for coordination with the U.S. Fish and Wildlife Service which, in turn, issues a biological opinion and specific endangered species management recommendations. Implementation of these recommendations can place constraints on execution of the military mission. To avoid possible penalties resulting from findings of "take" due to harassment or harm resulting from exposure to military-related noise, a capability is needed to evaluate and monitor the impact of noise on both behavior and breeding success of affected species. Under the ESA it is the responsibility of the land owner, not of the U.S. Fish and Wildlife Service, to evaluate effects of land use activities on threatened and endangered species.

The ESA prohibits take of endangered species, where "take" means to harass, harm, pursue, hunt, shoot, wound, kill, trap, capture, or collect, or attempt to engage in any such conduct. Within the definition of take, the term "harm" has been subject to significant judicial scrutiny. "Harm" is clearly an act that actually kills or injures wildlife, but it may also include actions that significantly impair essential behavioral patterns, including breeding, feeding, or sheltering.

The National Environmental Policy Act (NEPA) requires Federal agencies to assess the impact of planned activities on the environment and to make the assessment available to the general public. The decision making procedures are documented by either an Environmental Assessment (EA) or an Environmental Impact Statement (EIS). Noise and threatened and endangered species are often important issues in these documents, particularly as reviewers place a stronger emphasis on cumulative effects of activities.

# **Appendix B: Summary Data Tables**

Table B 1. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of experimental artillery simulator testing on Fort Stewart, GA, 1999.

Stimulus Distance (m)	Cluster Tested	Number of	Number of	Number of	Noi	Noise Levels, SEL (dB)	(dB)	Typical Ambient LEQ
		Noise Events	Data Sessions	Flushes	Cavity level	Cavity level unweighted	"A" weighted	(dB) "A" weighted
15.2	79, 137, 183	3	3	2	109.0-114.9	109.0-114.9 100.8-107.4	95.9-100.8	40.5-40.7
30.5	1,41,47,79,80,81,86, 87,107,126,137,159, 172,177,183,197,198	17	17	8	106.0-111.3	106.0-111.3 101.9-104.9	90.6-98.9	38.0-43.0
61.0	2,41,47,48,75,80,86,87,107,126,159,172, 177,179,197,198,218	17	17	5	103.9-108.9	103.9-108.9 94.4-103.8	89.5-94.5	38.1-56.5
91.5	2,75,218	3	3	0	105.3	99.1-100.9	85.9-89.0	38.9-41.1
122.0	2,47,48,71,75,87,172,179,184,198,218	11	11		98.0-104.1	93.7-99.1	75.4-83.9	41.0-44.2
244.0	184	-	1	0		97.7	77.9	41.3
Totals	24	52	52	16				

Table B 2. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of experimental .50-caliber blank fire testing on Fort Stewart, GA, 1999.

Stimulus Distance (m)	Clusters Tested	Number of	Number of	Number of	S.	Noise Levels, SEL (dB)	(dB)	Typical Ambient LEQ
•		Noise Events	Data Sessions	Flushes	Cavity level	unweighted	unweighted "A" weighted	(dB) "A" weighted
15.2	23, 53, 61, 151	39	4	3	115.1-118.9	115.2-108.3	101.6-103.1	41.5-53.7
30.5	23,32,36,51,53,61, 88,120,129,148, 151, 163,194,206	86	15	6	108.7-113.7	94.4-105.1	90.7-99.9	40.8-41.2
61.0	6,10,36,51,57,120, 129,133,139,148, 163,176,194,205, 206,227,	114	16	7	99.6-108.9	85.7-98.8	78.9-88.9	37.0-42.7
91.5	6,36,57,129,133,139, 176,205,228	99	6	9	93.6-102.5	84.3-95.0	78.3-87.4	39.2-42.7
122.0	12,23,51,57,133,148, 176,205,228	63	6	-	93.4-96.4	86.4-89.4	79.5-82.7	38.2-41.5
Totals	24	380	53	56				

Table B 3. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive M-16 live fire on Fort Stewart, GA, 1999.

Stimulus Distance (m)	Cluster Tested	Number of Noise Events	Number of Data Sessions	Number of Flushes	Noise Leve Unweighted	els, SEL (dB) "A" weighted	Typical Ambient LEQ (dB) "A" weighted
N/A	103	102	3	0	78.2-87.9	77.7-88.1	49.4-58.3
400-450	3, 103	484	4	0	63.5-79.4	55.5-77.4	49.2-59.5
1200	25	68	1	0	66.3-76.0	50.2-69.8	46.9
Totals	3	654	8	0			

Table B 4. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive grenade simulator blasts on Fort Stewart, GA, 1999.

Stimulus Distance (m)	Cluster Tested	Number of Noise Events	Number of Data Sessions	Number of Flushes	Noise Leve Unweighted	els, SEL (dB) "A" weighted	Typical Ambient LEQ (dB) "A" weighted
100	41	1	1	1	95.0	89.5	42.3
200	41	1	1	0	91.6	84.8	42.5
300	103	1	1	0	80.4-83.3	58.5-61.8	49.4
400	103	5	5	0	78.2-78.7	60.0-68.2	49.4
Totals	2	8	8	1			

Table B 5. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise levels of passive helicopter flights on Fort Stewart, GA, 1999. Stimulus distances represent the closest estimated approach distance by a helicopter.

Stimulus Distance (m)	Cluster Tested	Number of Noise Events	Number of Data Sessions	Number of Flushes	Noise Leve Unweighted	els, SEL (dB) "A" weighted	Typical Ambient LEQ (dB) "A" weighted
100-150	6	2	2	0	104.4	88.0	
200-250	23, 44, 83	4	3	0	95.3-99.2	78.7-84.9	38.14-53.7
300	6, 10, 143, 151, 218	5	5	0	90.3-93.8	75.0-84.1	37.0-56.5
400	25, 218	2	2	0	84.8-85.1	71.6-74.5	46.9-56.5
Totals	9	13	12	0			

Table B 6. Flush response of nesting Red-cockaded Woodpeckers versus the number, distance and noise level of passive large-caliber live fire on Fort Stewart, GA, 1999.

Stimulus Distance (m)	Cluster Tested	Number of Noise Events	Number of Data Sessions	Number of Flushes	Noise Leve unweighted	els, SEL (dB) "A" weighted	Typical Ambient LEQ (dB) "A" weighted
700-800	172	2	1	0	101.8-103.0	83.5-85.6	41.4
3000-3500	25,83	10	2	0	68.0-91.3	53.3-65.1	39.8-46.9
5000-6000	10,143,159	4	3	0	79.6-86.4	50.1-71.3	38.1-46.2
Totals	6	16	6	0			

# **Appendix C: Source Spectra Examples**

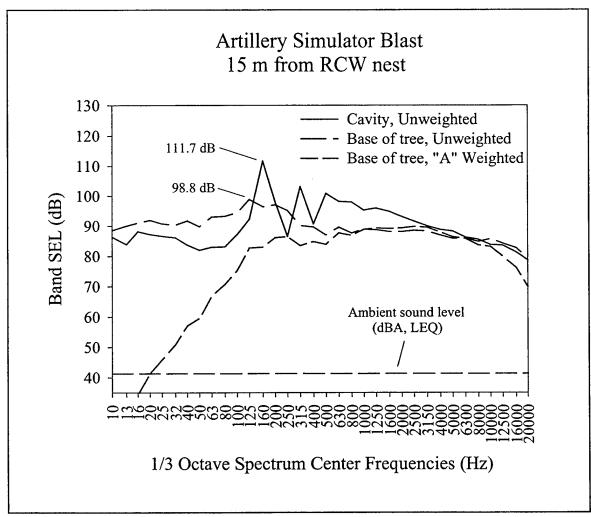


Figure C-1. SEL weighting comparison for experimental artillery simulator blast at cluster 172 on June 4, 1999.

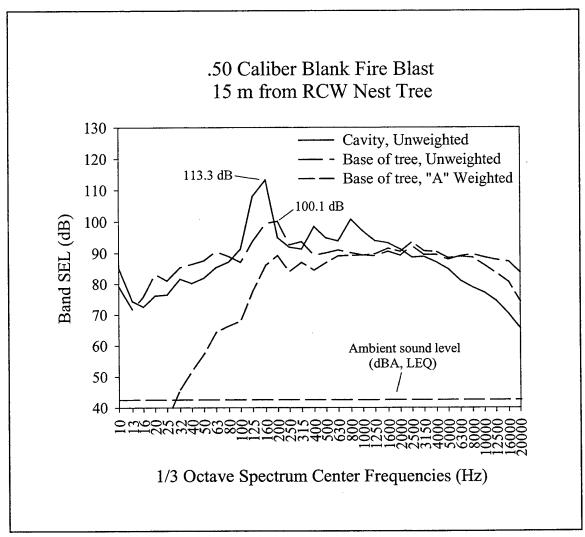


Figure C-2. SEL weighting comparison for experimental .50-caliber blank fire at cluster 151 on June 24, 1999.

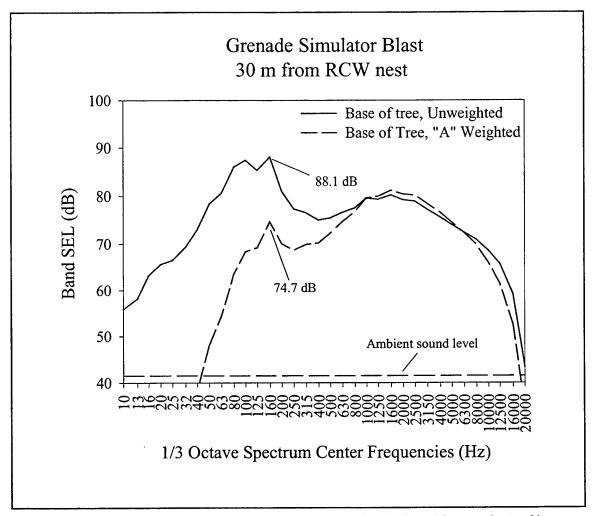


Figure C-3. SEL weighting comparison for a passive grenade simulator blast at cluster 41 on June 2, 1999.

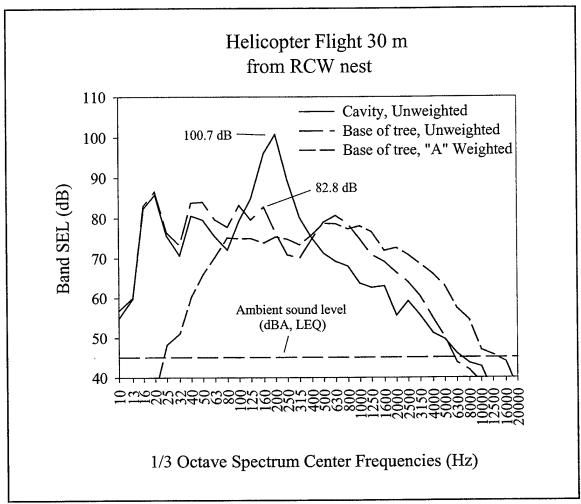


Figure C-4. SEL weighting comparison for a passive helicopter flight at cluster 6 on April 29, 1999.

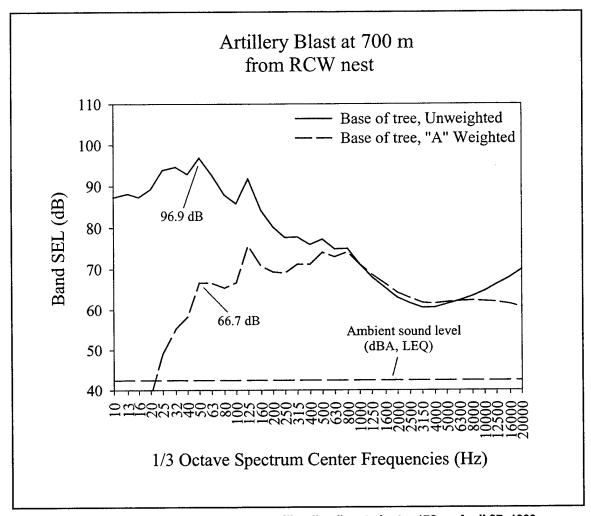


Figure C-5. SEL comparison of passive large-caliber live fire at cluster 172 on April 27, 1999.

Appendix D: Detailed Noise Event and RCW Response Data

Table D 1. Summary data for experimental artillery simulator blast noise on Fort Stewart, GA, 1999.

1999. Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	mic
Ciusiei	Date	Phase	Type	Dist.	Re-	time (min)	l tomano	Pos.		
		& Day	Type	(m)	sponse			. 00.	Flat	Α
1	05-May-99	1-4	Art. Sim.	<del>\</del>	0	0		Base	104.5	96.8
1	08-Jun-99	i-7	Art. Sim.	30.5	0	0		Base	102.8	96.7
2	28-Apr-99	1-3	Art. Sim.	122	0	0		Base	89.4	84.5
2	03-May-99	I-8	Art. Sim.	61	0	1.5		Base	102.1	92.7
2	06-May-99	1-9	Art. Sim.	91.5	0	0		Base	100.9	89.0
2	21-May-99	I-1	Art. Sim.	61	0	0		Base	102.1	92.2
2	27-May-99		<b>-</b>	61	0	0		Base	100.5	91.0
2	<del> </del>	N-9	<u></u>	30.5	0	0		Base	107.0	99.7
6	27-May-99	Post-fled.		30.5	0	0		Base	105.0	98.1
6	27-May-99	<del></del>		30.5	0	0	İ	Cavity	110.6	101.3
6	27-May-99		Art. Sim.	61	0	0		Base	100.9	93.3
6	27-May-99		Art. Sim.	61	0	0		Cavity	105.7	96.7
6	27-May-99		Art. Sim.	122	0	0		Base	88.7	79.3
6	27-May-99		Art. Sim.	122	0	0		Cavity	102.6	92.2
41	26-May-99	I-1	Art. Sim.	30.5	0	0		Base	104.0	96.6
41	02-Jun-99	I-8	Clay.	0	0	7.95		Base	95.0	89.5
41	02-Jun-99	1-8	Clay.	0	0	7.95		Base	91.6	84.8
41	02-Jun-99	I-8	Art. Sim.	61	0	1.48		Base	101.0	91.2
44	27-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	112.2	103.4
44	27-May-99	Post-fled.	Art. Sim.	61	0	0		Base	103.9	94.9
44	27-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	113.9	105.9
44	27-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	105.0	99.2
44	27-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	112.8	105.1
44	27-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	106.8	100.1
47	26-Apr-99	Egg laying	Art. Sim.	30.5	0	0		Base	100.3	85.2
47	30-Apr-99	I-3	Art. Sim.	61	0	0		Base	102.9	92.6
47	03-May-99	I-6	Art. Sim.	30.5	0	0		Base	104.9	97.7
47	04-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Base	106.3	100.7
47	04-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	112.7	107.0
47	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	104.8	96.5
47	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	112.3	104.3
47	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	111.6	103.4
47	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	102.1	92.1
47	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	112.7	103.8
47	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	103.9	96.0
47	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	103.3	93.1
47	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	112.8	104.0

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	t mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
47	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	110.5	104.4
47	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	102.5	94.3
47	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	100.1	89.1
47	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	108.1	99.9
48	23-Apr-99	I-3	Art. Sim.	122	0	0		Base	101.5	86.7
48	23-Apr-99	1-3	Art. Sim.	244	0	0		Base	97.9	83.2
48	27-Apr-99	1-7	Art. Sim.	61	0	0		Base	103.6	92.8
48	02-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	104.0	95.5
48	02-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	112.1	104.0
48	02-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	111.4	102.5
48	02-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	102.8	93.1
51	26-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	109.0	103.8
51	26-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	113.0	107.5
51	26-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	113.3	106.3
51	26-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	106.4	100.1
52	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	107.8	101.4
52	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	108.2	100.9
52	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	104.1	97.1
52	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	105.6	98.0
52	13-May-99	Post-fled.	Art. Sim.	61	0	0		Base	99.8	90.1
52	13-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	104.7	93.4
52	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	101.8	96.0
52	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	95.9	91.6
52	13-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	96.8	92.2
52	13-May-99	Post-fled.	Art. Sim.	61	0	0		Base	91.6	90.0
71	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	98.0	84.2
71	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	100.8	86.8
71	07-Jun-99	Post-fled.	Art. Sim.	122	0	0		Cavity	99.1	83.2
71	07-Jun-99	Post-fled.	Art. Sim.	122	0	0		Base	94.3	78.5
75	28-Apr-99	I-3	Art. Sim.	122	0	0		Base	99.8	86.1
75	03-May-99	I-8	Art. Sim.	61	0	0		Base	101.7	90.6
75	06-May-99	N-0	Art. Sim.	91.5	0	0		Base	100.4	86.3
75	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	101.2	90.0
75	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	109.8	99.3
75	07-Jun-99	Post-fled.	Art. Sim.	91.5	0	0		Cavity	105.3	93.7
75	07-Jun-99	Post-fled.	Art. Sim.	91.5	0	0		Base	106.0	94.3
79	06-May-99	1-3	Art. Sim.	30.5	0	0		Base	103.3	96.7
79	13-May-99	I-10	Art. Sim.	30.5	0	0		Base	104.1	97.5
79	14-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	107.4	100.8

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	t mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
79	14-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	114.6	107.9
79	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	95.3	85.3
80	17-May-99	I-1	Art. Sim.	61	0	0		Base	94.4	89.5
80	21-May-99	I-5	Art. Sim.	30.5	0	0		Base	103.6	95.1
81	06-May-99	l-1	Art. Sim.	30.5	0	0		Base	103.5	94.4
86	04-May-99	1-6	Art. Sim.	30.5	0	2.917		Base	103.6	96.9
86	04-May-99	I-6	Art. Sim.	30.5	0	0.1208333 3		Base	104.0	97.2
86	09-May-99	N-0	Art. Sim.	61	0	3.717		Base	96.7	89.5
86	12-May-99	N-3	Art. Sim.	30.5	0	13.667		Base	102.5	93.3
87	23-Apr-99	I-1	Art. Sim.	122	0	5.467		Base	96.8	83.1
87	27-Apr-99	I-5	Art. Sim.	61	0	0		Base	104.1	95.1
87	30-Apr-99	I-8	Art. Sim.	30.5	0	1.567		Base	106.3	98.9
87	03-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	105.5	94.2
87	03-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	109.2	103.0
87	03-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	102.7	94.1
87	03-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	106.8	101.1
103	13-May-99	N-3	Clay.	0	0	0		Base	80.4	61.8
103	13-May-99	N-3	Clay.	0	0	0		Base	81.4	58.5
103	13-May-99	N-3	Clay.	0	0	0		Base	82.7	59.7
103	13-May-99	N-3	Clay.	0	0	0		Base	78.8	60.0
103	13-May-99	N-3	Clay.	0	0	0		Base	83.3	60.3
103	13-May-99	N-3	Clay.	0	0	0		Base	78.7	68.2
103	13-May-99	N-3	Clay.	0	0	0		Base	84.8	85.6
103	13-May-99	N-3	Clay.	0	0	0		Base	78.4	55.5
107	05-May-99	1-9	Art. Sim.	30.5	2	5.067		Base	104.5	98.9
107	10-May-99	N-0	Art. Sim.	61	0	0		Base	101.9	92.5
107	12-May-99	I-7	Art. Sim.	30.5	2	5.15		Base	105.1	98.6
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	103.8	97.8
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	112.3	106.3
107	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	99.3	90.1
107	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	111.3	103.5
107	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	101.9	94.6
107	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	94.9	88.2
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	108.6	99.4
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	117.8	108.9
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	103.8	97.8
107	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	112.3	106.3
125	13-May-99	Post-fled.	Art. Sim.	15.2	0	О		Base	103.0	97.6
125	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	107.1	99.7

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) at	mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
125	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	97.9	93.0
125	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	100.3	93.7
125	13-May-99	Post-fled.	Art. Sim.	61	0	0		Base	91.3	87.8
125	13-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	94.7	89.1
125	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	103.3	96.6
125	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	106.1	99.4
125	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	101.9	96.1
125	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	104.3	96.7
125	13-May-99	Post-fled.	Art. Sim.	61	0	0		Base	89.8	83.9
125	13-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	95.7	89.2
126	04-May-99	1-3	Art. Sim.	30.5	0	0		Base	105.4	98.2
126	09-May-99	I-8	Art. Sim.	61	0	0		Base	102.1	90.5
126	13-May-99	N-1	Art. Sim.	30.5	0	0		Base	104.2	97.6
137	04-May-99	I-7	Art. Sim.	30.5	0	0		Base	103.4	93.7
137	26-May-99	I-7	Art. Sim.	30.5	2	3.483		Base	103.6	94.3
137	01-Jun-99	N-1	Art. Sim.	15.2	0	0		Base	100.8	95.9
137	01-Jun-99	0	Art. Sim.	15.2	0	0		Base	100.8	95.9
143	27-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	102.7	95.4
143	27-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	110.9	103.7
143	27-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	105.6	98.7
143	27-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	109.8	102.7
159	03-May-99	I-3	Art. Sim.	61	0	0		Base	102.5	94.2
159	06-May-99	l-5	Art. Sim.	30.5	2	2.7		Base	111.6	104.7
159	17-Jun-99	Post-fled.	Art. Sim.	30.5	0	0	<u> </u>	Base	106.8	99.7
159	17-Jun-99	Post-fled.	Art. Sim.	30.5	Ó	0		Cavity	114.5	106.8
159	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	115.2	105.5
159	17-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	103.0	94.4
172	23-Apr-99	I-7	Art. Sim.	122	0	0		Base	100.5	86.8
172	27-Apr-99	N-0	Art. Sim.	61	0	0		Base	101.4	91.9
172	03-May-99	N-6	Art. Sim.	61	О	0		Base	103.9	96.6
172	04-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Base	106.7	100.1
172	04-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	113.5	106.8
172	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	104.6	99.1
172	04-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	113.0	106.4
172	04-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	102.9	93.3
172	04-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	112.4	104.6
177	09-May-99	1-3	Art. Sim.	61	0	0		Base	96.4	90.6
177	11-May-99	I-8	Art. Sim.	30.5	2	3.367		Base	104.8	97.5
177	17-May-99	N-0	Art. Sim.	30.5	0	0		Base	104.4	96.2

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	t mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
177	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	110.4	102.8
177	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	103.5	95.1
177	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	101.3	90.8
177	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	109.5	99.1
177	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	109.3	102.8
177	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	105.8	100.1
177	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	98.8	86.5
177	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	104.1	93.7
179	23-Apr-99	I-4	Art. Sim.	122	0	0		Base	100.0	86.3
179	28-Apr-99	1-9	Art. Sim.	61	0	0		Base	99.8	92.0
179	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	113.7	103.5
179	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	103.0	91.4
179	07-Jun-99	Post-fled.	Art. Sim.	122	0	0		Cavity	108.4	97.2
179	07-Jun-99	Post-fled.	Art. Sim.	122	0	0		Base	99.6	81.5
183	04-May-99	I-6	Art. Sim.	30.5	0	0		Base	101.9	90.6
183	10-May-99	N-1	Art. Sim.	15.2	0	0		Base	103.6	98.0
183	07-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Base	105.8	97.5
183	07-Jun-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	109.0	103.7
183	07-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	108.6	102.1
183	07-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	104.0	97.1
183	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	101.2	90.8
183	07-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	108.8	100.1
184	23-Apr-99	l-1	Art. Sim.	244	0	0		Base	97.7	77.9
184	27-Apr-99	I-5	Art. Sim.	122	0	0		Base	99.1	83.9
194	26-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	107.3	99.6
194	26-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	113.8	106.0
194	26-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	114.5	105.2
194	26-May-99	Post-fled.	Art. Sim.	30.5	0	0	<u> </u>	Base	106.4	99.0
197	06-May-99	I-7	Art. Sim.	30.5	2	5.983		Base	103.2	95.1
197	10-May-99	N-0	Art. Sim.	61	0	0		Base	97.7	86.3
197	12-May-99	N-2	Art. Sim.	30.5	0	0		Base	101.0	93.5
197	18-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	103.6	94.0
197	18-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	104.1	94.5
197	18-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	107.8	100.3
197	18-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	101.6	92.6
197	18-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	105.0	98.3
197	18-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	107.8	101.0
198	23-Apr-99	I-5	Art. Sim.	122	0	0		Base	100.3	88.2
198	27-Apr-99	I-9	Art. Sim.	61	0	0		Base	103.3	93.8

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	t mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
198	30-Apr-99	N-1	Art. Sim.	30.5	0	0		Base	104.6	97.6
198	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	102.7	95.7
198	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	108.7	100.3
198	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	107.6	95.4
198	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	98.3	87.9
198	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Base	105.6	95.5
198	11-Jun-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	110.7	103.4
198	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Base	102.1	91.2
198	11-Jun-99	Post-fled.	Art. Sim.	61	0	0		Cavity	109.2	99.1
199	11-May-99	Inactive	Art. Sim.	15.2	0	0		Base	113.5	105.8
199	11-May-99	Inactive	Art. Sim.	15.2	0	0		Cavity	117.5	110.7
199	11-May-99	Inactive	Art. Sim.	30.5	0	0		Base	103.6	97.0
199	11-May-99	Inactive	Art. Sim.	30.5	0	0		Cavity	109.7	104.0
199	11-May-99	Inactive	Art. Sim.	61	0 .	0		Base	94.9	85.0
199	11-May-99	Inactive	Art. Sim.	61	0	0		Cavity	101.5	95.0
199	11-May-99	Inactive	Art. Sim.	61	0	0		Base	103.1	95.7
199	11-May-99	Inactive	Art. Sim.	61	0	0		Cavity	104.3	97.1
199	11-May-99	Inactive	Art. Sim.	30.5	0	0		Base	104.0	99.3
199	11-May-99	Inactive	Art. Sim.	30.5	0	0		Cavity	102.5	96.4
206	12-May-99	1-10	Art. Sim.	30.5	0	0		Base	103.6	97.3
208	11-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	102.4	97.2
208	11-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	104.6	97.4
208	11-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	107.5	98.9
208	11-May-99	Post-fled.	Art. Sim.	30.5	0	0		Base	103.3	96.5
208	11-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	106.5	96.0
208	11-May-99	Post-fled.	Art. Sim.	61	0	0		Base	101.0	90.2
211	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	102.3	96.6
211	13-May-99	Post-fled.	Art. Sim.	15.2	0	0		Cavity	106.7	99.0
211	13-May-99	Post-fled.	Art. Sim.	30.5	0	0	,	Base	96.0	90.3
211	13-May-99	Post-fled.	Art. Sim.	30.5	0	0		Cavity	102.6	95.4
211	13-May-99	Post-fled.	Art. Sim.	61	0	0		Base	92.7	89.0
211	13-May-99	Post-fled.	Art. Sim.	61	0	0		Cavity	97.3	91.4
218	23-Apr-99	1-4	Art. Sim.	244	0	0		Base	93.7	75.4
218	27-Apr-99	1-8	Art. Sim.	61	2	1.7		Base	103.8	94.2
218	30-Apr-99	N-0	Art. Sim.	91.5	0	0		Base	99.1	85.9
218	26-May-99	Post-fled.	Art. Sim.	15.2	0	0		Base	107.0	100.8
218	26-May-99		Art. Sim.	15.2	0	0		Cavity	110.1	102.2
218	26-May-99		Art. Sim.		0	0		Base	106.1	98.3
218	26-May-99		Art. Sim.	30.5	0	0		Cavity	110.4	101.9

Cluster	Date	Nesting	Event	Event	RCW	Recovery	Remarks	Mic	SEL (dB) a	ıt mic
		Phase	Туре	Dist.	Re-	time (min)		Pos.		
		& Day		(m)	sponse				Flat	Α
231	11-May-99	Inactive	Art. Sim.	15.2	0	0		Base	104.5	97.0
231	11-May-99	Inactive	Art. Sim.	15.2	0	0		Cavity	109.9	104.5
231	11-May-99	Inactive	Art. Sim.	30.5	0	0		Cavity	107.3	100.6
231	11-May-99	Inactive	Art. Sim.	30.5	0	0		Base	105.4	97.8
231	11-May-99	Inactive	Art. Sim.	61	0	0		Base	101.7	91.4
231	11-May-99	Inactive	Art. Sim.	61	0	0		Cavity	105.4	98.6
236	11-May-99	Inactive	Art. Sim.	15.2	0	0		Base	101.4	93.9
236	11-May-99	Inactive	Art. Sim.	15.2	0	0		Cavity	105.8	98.0
236	11-May-99	Inactive	Art. Sim.	30.5	0	0		Cavity	104.8	97.1
236	11-May-99	Inactive	Art. Sim.	30.5	0	0		Base	102.0	94.5
236	11-May-99	Inactive	Art. Sim.	61	0	0		Base	102.1	90.1
236	11-May-99	Inactive	Art. Sim.	61	0	0		Cavity	105.4	97.7

Ä
Ę
×
š
Fort Stewar
Ξ
ors o
a
핕
ś
l artillery s
Έ
直
en
틒
ğ
or e
ra f
동
g
ise
5
₹
eigh
Ž
ē
ati⊳
ent
res
. Represe
2.
Table D 2.
aple
۳

-1	3																																				
Sec	Overall	SEL	104.5	102.8	89.4	102.1	100.9	102.1	100 5	00.0	0.701	105.0	110.6	100.9	105.7	88.7	102.6	104.0	05.0	2.5	0.	101.0	112.2	103.9	113.9	105.0	112.8	106.8	100.3	102.9	104.9	106.3	112.7	104.8	112.3	111.6	102.1
	20000	T			51	35	53	58	2 6	3 6	5	74	89	64	64	32	39	74	43	3 8	R7	22	73	92	9/	77	76	78	51	22	73	79	79	73	74	72	19
	16000	202	69	8	20	62	57	35	3 8	8 8	2	92	2	171	29	34	43	7/8	50	3 9	<del>3</del>	96	75	7.1	78	85	79	8	53	99	9/	83	81	78	26	74	67
	19500	_	72	72	52	89	19	Ę.	2 5	2	<u> </u>	8	72	7.5	89		46	62	ű	8	2	69	92	75	79	84	80	84	26	89	62	88	82	80	77	9/	5
	10000		75	74	2	73	55	5	5 5	7/8	8	<u></u>	74	22	69	41	51	62	8	8 8	3	72	77	77	80	82	81	88	29	7.	8	82	88	85	78	76	73
	טטטאן טטנט	_	T	7	69 02	Т	Т	T	Т	Т		$\neg$					Γ	Π	Т		66				П				Γ				86 85				1
	5000	1	T	T	77		T		T									Γ	Ī														88				
	900	2004	$\top$	Т	73	1	Т	Т	Т	T	П								Τ			22	83	8	98	98	87	87	89	78	82	87	88	84	85	82	78
	0500 0450	000	Т	Т	72 74	Т	Т	Т	Т	Т	Ţ						Т	Г	Т		73 72		T	Т	Ţ		Γ			Γ	i	ı	91 91		1	1	08 08
	9000	3	T	T	75	Т	Τ	Т	Т	T				Г	Г	Γ	Г	Т	Т		75	79	88	88	6	87	91	88	73	18	98	88	8	82	88	87	1 1
	_	000	T	Т	23 22	Т	Т	T	T	П	П				Г	Г	П	Т	Т		55 57		T	Т	Т	Г	Г	Г	Т	Г	Т	П	97 94	1	i	T	1 1
-	90,	3	g	3 8	3 15	2 2	3 8	2 8	2 8	8	68	87	6	82	83	71	9/	150	3   3	<b>3</b>	9/	T-	1	Т	1		Т	Г	Т	Т	Т	Г	8	Г	Т		
	-	930	_	$\top$	3 82	1'''	Т	Т	7	7				Г	T	Г	T	Т	Т		73	88	26	8	88	88	26	68	22	<u>=</u>	88	8	86	88	35	94	81
		200	_	T	20 20	_	T	T	$\neg$	$\neg$			Г		T	T	Т	Т	T		72	Г	100	Т	1	Г	Т	П	T	Т	Т	Т	95 102	1	1	1	1 1
		<u></u>	63	3 8	8 8	3 8	3 8	5 8	3	88	88	98	8	8	82	65	84	1	5	16	72	62	ജ	82	₽	16	88	6	82	48	<u>.</u>	S	\$ 5	87	8	Ŝ	88
•		500 520	7		2 G	┰	T	Т	$\neg$				Г	Т	Т	Т	_	Т	Т		97 79	8	8	8	6	8	6	g	8	S	3 5	3	101	16	T		T
	- [	125 160	Т	8 8	2 4	20	Т	T	$\neg$	$\neg$			Т	1	92 102	188		18	Т		84 79												91		$\overline{}$	9	T-1
		8	Т	8 8	Т	2 6	Т	Т	$\neg$			Г	Т	Т	8	Т	Т	Т	Т		83	Г	8 8	Т	6	86	8	ક	8 8	8	3 8	3 8	3 8	95	8 6	88	92
	r Frequenc	88	П	3 8	8 8	8 8	Ŧ	Т	П	90 92	16	96 06	88	Г	Т	$\top$	Т	3 8	7	81	81	8	1	┰	7		Т	Т	8 8	Т	8 8	Т	8 8	T	Т	88	95 36
	rum Cente	22	T	3 8	T	Т	Т	3 3					16	Т	Т	Т	2 2	Т	٦	73 78	70 74	ã g	T	3 8	Т	Т	Т	Т	3 8	Т	Т	Т	8 8	Т		T	06
	tave Spect	32 49	T	T	1 8	Т		£ 6	$\neg$		87 87	88	Т	Т	79	Т	1 8	, 6	╗		69	Т	2 %	Т	Т	Τ	Т	Т	Т	Т	┰	Т	\$ 2	; ¥	3 8	3 8	8 8
	<b>≚</b> [	20 22	T		/8 F	T	╗			81 82	Г	ī	Т	Ţ	8 8	Т	T	T		99 99	57 62	77	$\top$	Т		8 æ	Т	T	Т	8 8	0 8	Т	П	3 8	Т	Т	8 8
8	Band SEL (dB	9	$\neg$		$\neg$	Т		╗			Г	Г	Т	Т	Т	3 2	Т	2 9			9 49	T	2 6	Т	3 6	Т	Т	Т	Т	9 9	0 0	Т	0/8	Т	Т	Т	78 79
	Bar	10 13		23	8	2	1	25	74	9 74	77	16	12	2 8	5 15	3 8	G 6	S I	િ	26	9 49	1	$\neg$	3 8	e 8	3 8	3 8	3 2	ē \$	2 į	از	٤١	6 6	à P	e 8	7,	8
וובאובפולפנו	ant Mic	t. Pos.	П			T	$\neg$	$\neg$	Base	Base	Т	Т	Cavit	Т	1	Т	Т		2	Base	Base		Dase	Cavity	$\top$	T	T	T	Т	Т	T	T	Т	T	esegnation of	T	30.5 Base
חבשום		e Dist.		Sim.	. Sim. 30.5	Sim.	Sim.	Sim.	. Sim. 61	Sim.	Sim.	Sim.	Sim 20.5	iii o			. SIM. 122	Art. Sim. 122	. Sim. 30.	0 2 %: e	ص چ و	-	_	_	Art Cim. Dis			21.0	Arr. Sim. 15.2			Art. Sim. 30		Art. 51111. 13.2	Art. Sim. 30.5	Art. Sim. St	Art. Sim. 30
	Date Eve	Type	П	$\neg$		4/28 Art.	$\neg$	5/6 Art	5/21 Art.	П	Т	1	- 1		77/2	- 1	- 1	- 1	5/26 Art	6/2 Live Clay-	6/2 Live Clay-	Т	П.	- 1	5/2/ An	- 1	- 1	ł			٦.	- 1	6/4 Ar	Т	- 1		6/4 Ar
י מומוני	3		П						2		T	T	Τ	T	Ī	Т	اء	9	4	41	41		14	4	4 :	‡ :	‡  :	1 :	4	\$	4	4	4	ş	4	<del>}</del>	4 4

																																					_		
Calc.	Overall	SEL	112.7	103.9	103.3	112.8	110.5	102.5	100.1	108.1	101.5	97.9	103.6	104.0	112.1	111.4	102.8	109.0	113.0	113.3	106.4	107.8	108.2	104.1	105.6	93.8	104.7	101.8	95.9	96.8	91.6	98.0	100.8	99.1	94.3	8.6	101.7	100.4	101.2
	20000								55							73	94	8/																		37	57		59
	16000	T	1																														44	35	41	51	62	49	92
	12500								63																													54	
	10000																																	45	48			09	
	8000																													-	- 1	l						64	
	6300	1	8/	8	75	79	82	77	71	72	69	67	78	81	82	81	79	87	87	85	83	87	82	81	2.2	7.5	99	81	77	14	74	92	25	43	22	29	7.3	99	74
	0009 0	4	8	<u></u>	77	81	84	52	73	74	20	2	2,8	81	83	83	80	91	88	87	98	98	ဆ	85	22	73	69	80	77	11	75	29	28	51	61	69	75	69	92
	3150 4000		$\neg$						5 74																														9/ 2
	2500 31	П	$\exists$	$\neg$													F	-													- 1	- 1			1		1	73 72	1 1
	0 2000	П	П	$\neg$																										1					l		1	74	H
	1250 1600		T	╗													Г		П																			74 74	1 1
	1000												1			1	l	ł							i				ii	l	- 1				l		ŀ	74	1 1
	0 800	$\neg$	_	$\neg$												г	1	_																				74	
	500 630			$\neg$										_		1	Г	П					I	I		i								ĺ		ı	ł	76 73	
	400	П	$\neg$													П			Г						Γ	1								,	ĺ	i i	ı	75 7	1 1
	315 4	П															1	Γ									ı							ı		Į.	ı	8	1 1
	220	П														П	Γ	Г	Г			П	П	_	Ī									1	1	ŀ	1	81	lΙ
	500		102	93	93	101	108	8	82	106	81	9/	88	35	8	ક્ર	8	5	5	<del>1</del> 05	æ	96	66	35	83	8	8	83	82	93	9/	6/	8	73	2	12	8	92	8
	160		티	8	8	Ξ	91	8	8	91	88	84	35	8	<u>5</u>	<u>8</u>	8	5	<u>6</u>	읃	97	8	<u>ē</u>	8	8	듄	ā	84	84	77	81	83	88	8	ę.	78	8	8	8
	125	Ц	ह्य	ક	83	91	98	26	8	<del>1</del> 6	83	98	93	8	5	55	5	88	ક્ષ	ક્ષ	86	8	5	94	ક્ષ	8	83	78	8	72	8/	87	97	8	88	8	8	8	<u></u>
es (Hz	5		8	8	94	87	8	94	8	8	82	88	အ	용	8	83	용	8	8	8	8	88	8	8	क	8	8	8	88	74	11	8	ક્ક	94	8	83	6	&	ន
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	8	Н	8	26	8	88	8	8	8	8	8	8	6	ક્ક	88	8	8	8	ജ	8	8	5	8	ક્ક	ន	8	8	8	8	73	79	8	8	8	88	8	83	8	क्ष
ter Fre	8	Н	8	ಹ	ස	8	8	8	84	8	_		Г	೫		Т	Т	П	П		Г	Г	왕	П		8		8	88	73		8	Г	8	Г	8	Т	П	8
m Cer	20	Н	8		91		Г	88		Г	Г			Г	Γ	Г	Г	П			Г	Γ	9		Γ	Γ-			77	72		Г	8	Т	П	П	8	Т	8
Spectri	<u>용</u>	П	8		87	Γ-	П	П	8	92	Г	8	l	T	Г		Т	Т	8	П	Г	П	Т	Ī	8	Γ	8	1	1	73		8	₩.	Т	T	Т	8		8
ctave	8	П				Г	П	Г	8	75						1	П	Т	Т	Г	Г	Г	8	Г	Т	8	П	П		72	Г	Γ	Г	T	Т	T	88	T	8
11/30	52	П		82	84		T		<u>~</u>	92		8	Г		Ι	Г	8	П	18			Г	6	Г	П	88	П	Г	8	7.	П	П	Г	Τ	Т	Т	Т	8	П
(dB)	8	П	_		82	Г	98	Г	62	1	Г	П			П	П	П	Т	П	Г	Γ	Г	8	П	Т	8	П	Т	П	5 75	П	Г	Т	Т	Т	Т	8	88	П
d SEL	3 16	П			8	П	-	Г	8			3 76	Г	Г	Π	Т	Т	8	Γ	П	П		8	Т	П	<u>@</u>	Т	П	4 75	Г	Г	Г	П	Г	Τ	Т	Т	77	80
Ba	10 13	_	78 85	83 85	78 79	88	89	88	74 76	78 77	_	69	80	8	93	_	_	8	_	_	_	88	75 75			70 78			70 74		_	64 75	59 73	_	_	74 7	_	_	_
Mic	Τ.	П	_	Base	Base	<u>_</u>	Cavity	1	П	Cavity	_	Base	Base	П	Cavity	Т	1	Т	Т	Cavity	Г	T	T	7	Γ	Т	Cavity	Cavity	Base	Cavity	Base	Base	Cavity	Cavity	Base	Base	Base	Base	Base
Event	Dist.		30.5		61	_	30.5	_	_	19	_	244					19		15.2		$\mathbf{r}$	15.2				_	19					19	-		122		_	91.5	_
Event	Type		Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.							
Date	1	-		11/9	6/11	1	11/9	1	<b>†</b>	6/11	4/23	4/23	4/27	П	ī	Т	6/2	1.0	1		$\overline{}$		т	_	_	7	5/13				1		Τ			١	Т	$\top$	1/9
<u>8</u>			47	47	47	47	47	47	47	47	<b>&amp;</b>	<b>&amp;</b>	<del>&amp;</del>	\$	8	48	8	125	5	22	25	25	25	25	S	25	3	25	25	23	25	=	7	7	:   =	75	K	2 12	8

ΗU	<u>-</u>	13																						_	_						
Calc.	Overall	SEL	0.50	000.3	0.00	103.3	104.1	107.4	114.6	95.3	94.4	103.6	103.5	103.6	104.0	96.7	102.5	8.96	104.1	106.3	105.5	109.2	102.7	106.8	80.4	2	t.10	06.7	0.0/	86.3	/:0/
	20000	1,	<u>,</u>	ξ,	<u>ئ</u>	/1	-	7.5	81	51	29	20	9	69	2	29	89	35	8	79	61	74	99	75							
	16000	5	2 2	2 5	3	3	33	4	82	25	88	8	29	7.5	73	28	72	43	78	79	89	9/	72	9/	88	3	g	8	8	/2 6	5
	12500	6	3 5	<sub>ਨ</sub>	ر (	82	23	29	83	26	٤	66	-	75	75	91	75	49	77	78	72	75	75	29							
	10000	- 6	8 8	3	[0]	<u></u>	88	82	94	29	72	23	74	1	1	72	9/	55	11	80	75	11	9/	82	23	3			/7	S S	2
1 1	0 8000	٤	2 8	8	3 3	8	8	83	အ	83	23	9/	14	8	29	72	77	29	22	8	11	62	82	88	34	5 6	e	75 8	9	¥ 8	8
	6300	į	8 3	\$	<u>ا ع</u>	8	8	8	8	93	55	8	2	8	8	73	78	62	78	82	62	₩	62	8	+						**
1 1	2000	8	8 5	g :	8	<u></u>	8	87	93	29	9/	8	2	ਛ	8	74	78	64	79	84	62	83	79	84	85	8 8	<u></u>	÷	8	g !	<del>}</del>
1 1	0 4000		┰	┑	T						11		П							Γ	Γ			Γ			2				5
	3150	П	Т	П	T	П					78	П				_				l	1	į .		1	1	<del>`</del>					8
	00 2500	П	Т	T	П	П					78	$\neg$	П									1	1		1						2/2
	1600 2000		コ								6/						I	1		Г	1	l							46 45		28
	1250 16	П	Т	╗	П						9 79						ł			1	1	ı	1			- 1					28
	1000 12	$\Box$	寸	$\neg$					Г		79   79					П	Г	Ī	Г	П	Γ	П		Г	Т						60
	800	П			$\neg$						79 7							Γ	ı	1	1	I_		1	1	i					22
	630	ГΤ	т-Т	П	$\neg$				1		78	_					1	t	ı		1	1		1	١	- 1				22	32
	200	П	$\neg$						Ι	-	11								ı	1		1	1	i	1		21	21	23	25	28
	<del>\$</del>		83	85	98	86	98	87	83	8	75	84	85	91	9	12	84	72	8	8	88	8	8	8	5 6	25	44	69	23	69	24
	315		8	<u></u>	<u>@</u>	84	83	8	8	88	11	28	82	68	8	11	8	8	83	8	8	ន	2 2	ક		22	21	83	25	54	5
	520	1 1							1	1	11	ł				1	1	ŧ	i	1		1		١.	. 1	1	<u>ස</u>	20	26	29	8
	500	$\overline{}$						-	_		82				ı										- 1				29		8
	9 19	$\mathbf{T}$						П	T		8			l	1	Į.	1	1	1		1	1	1	1	- 1						64
(F	100 125	-					88		1	Г	T	38				8	T	Т	Т	1	Т	8	Т	$\top$	3 6		67	63 58	99	63 58	99 29
ncies (	=	П			2 88		Г	П	Т	т	85 86	5	Г	T		8	Т	Т	Т	Т	T	8	3 8	Т	5 2			9 69	9 99	69	99
Freque	63 80	П	8		83 8	Г	91	Γ	T		88		1	68	Г	Т	88	Т	T	1	98	$\top$	Т	Т	7		99	89	29	88	69
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	35	T		88		П	88	Т	Т	Т	88			Г	Г	Т	88	Т	Т	Т	Т	Т	Т	Т	Т		72	74	71	74	69
mutos	8	П	77	9/	13	84	88	8	8	83	82	98	88	88	88	78	83	88	ક	8	8	8	3 6	, g	B	73	75	8/	E E	82	8
we Spe	8		78	7.5	9/	28	84	87	88	25	92	9	82	8	88	35	æ	2	5	<u> </u>	3 8	1 8	3 2	3 8	8  i	74	7.5	9/	82	92	8
/3 Oct	25		75	74	4	72	8	8	क	8	68	88	83	88	8	72	<u>ڇ</u>	1 2	S	3 2	8	3 8	8 8	3 8	8 1	<u>ب</u>	74	47	8	55	29
1B) at 1	2		75	8	73	22	8	8	18	8	8	8	8	88	8	155	<u>ڇ</u>	2   82	8	3 8	3 2	5 8	3 8	2 8	3	2	72	7	25	47	98
SEL	19		74	72	74	82	8	8	8	8	8	8	88	8	8	8	2	1	: 8	3 2	5   Z	5 8	3 2	5 2	5	99	66	98	49	8	64
Band	10 13		_		22	_	18	_		79	99		78	88				2 62	_	_	3 S	_	<u>د</u> ا و	_	<u> </u>	හි	61 85	49 60	41 38	63 67	24 60
Mic	Τ	T	Cavity 71	Cavity 69	Base 66	Т	Base 87	Т		Base 7	_	т	Base 7	Т	┰┈	1	7	$\top$	Т		$\neg$	ᇽ.	٦,	٦.	Cavity	Base	Base 6	Base 4	Base 4	Base 6	Base 5
Fvent	Т	Ē	61	91.5	91.5	30.5	30.5	30.5	30.5	19	9	30.5	30.5	30.5	30.5	i i	3 6	3 5	1 2	20 6	2000		C.D.	5 3	5	0	0	0	0	0	0
Fvent	Т	Т	Art. Sim.		Art. Sim.		Art Sim.	Art Sim	Art Sim	Art Sim	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art Sim	Art Sim	At Cim	Art Sim	5 6	Art. Olli.	Alt. Olli.	All. Ollif.		- 1	Art. Sim.	Live Clay- more	Live Clay- more	Live Clay-	Live Clay-	Live Clay-	Live Clay- more
Date	_		2/9	139	1	1	۱	•					9,9	ł	- 1	ı	٦		- 1	12/6	ı	1	- 1	- 1	ı	5/13	5/13	5/13	5/13	5/13	5/13
3	Т		35	Т	Г	T	T	Т	Τ	Т	? (€	Т	Т	Т	Т	Т	8 8	3 8	اۃ	3 á	3 á	à	28	à	87	<u>ş</u>	103	103	103	103	103

Calc.	Overall	SEL SEL	34.8	78.4	104.5	101.9	105.1	103.8	112.3	99.3	111.3	101.9	94.9	108.6	117.8	103.0	107.1	97.9	100.3	91.3	94.7	103.3	106.1	101.9	104.3	86.8	95.7	105.4	102.1	104.2	103.4	103.6	100.8	100.8	102.7	110.9
	20000	0,																						1										71		٦
	16000																																	7.5		
	12500																																			
	10000		62																		Ī													6 75		
	8000		69 64			1 67																									ĺ			9/ 9/		
	8300 8		6	2																			83							83				79		
	2000		72	34	82	9/	84	83	84	75	79	72	74	85	84	83	84	79	79	73	73	82	85	85	91	69	73	83	74	84	77	79	81	18	<u>8</u>	8
	2500 3150 4000 5000		75	37	98	79	82	84	98	9/	85	74	74	82	82	84	82	80	80	74	74	84	84	8	8	=	33	8	75	82	78	80	85	85	<u></u>	82
	3150		F		87	80	98	82	88	8	83	75	9/	87	87	82	98	81	85	9/	75	98	82	8	8	2	9	8	77	98	80	181	83	83	8	8
	2500		<u> </u>	40	87	81	88	98	6	29	84	22	77	88	87	98	82	82	6/	77	74	82	84	32	<u></u>	23	74	8	78	98	81	82	84	8	8	88
	2000		<u> </u>	40	68	85	88	98	35	78	87	78	11	88	6	87	98	85	85	78	9/	98	98	82	8	23	92	87	79	87	85	82	82	8	88	8
	0 1600		75	37	88	85	88	87	83	78	8	80	22	88	35	98	8	8	79	78	75	98	82	8	8	7	72	88	79	87	83	85	98	8	쬬	8
	0 1250	Н	23	47	88	85	87	82	8	79	35	84	9/	88	83	98	84	82	80	78	9/	8	88	8	8	7,	92	87	79	87	83	8	8	8	8	8
-	1000		74	48		81												Г														-		82		
	008			45	_	81																			$\neg$									87		
	0 630		98	47	П	85											П								$\neg$					П				8		
	0 200	П		48		81											1								П					-		i	1	8		- 1
	315 400	П	62	43															Γ													1	l	7 87		100
	250  3		53 55	49 49		83 84									Г		Г	Г												0 88		1	П	85 87		$\Box$
	200 2	Н		54 4	_	88											1					_	103			$\neg \neg$	_						ī	98 98		
	90	Н		51	-	7	_							$\overline{}$																				87		
	125	П		g g	26	8	8	26	92		35	85	87	£	8	8	55	8	83	81	87	50				8		95	35	æ	8	П	8	П		83
( <del>Z</del>	100		45	09	Г		Г	ક્ષ		93		-	82		88	8	88	1	Г	Г		ક્ક	89	95	88	85	79	-26	5		æ		8	86	94	æ
encies	8		46	29	94	94	91	91	98		80	62	88		91	83	87	87	82			Г	98			81		8	ક્ક	92	ક્ક	ક્ર	88	98	93	81
Fred	63		49	29	56	95	56	98	98	98	82	79	8	ક્ક	8	88	88	88	83	8	78	83	84	92	85	80	2/	35	8	83	91	91	88	8	94	82
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	22			89	6	8	8	88	8	87	8	12	8	8	87	8	88	8	62	11	9/	8	98	06	82	74	73	8	8	82	85	8	8	98	88	83
ectru	8		40	8	8	6	8	68	84	84	82	62	듄	ន	8	8	8	92	12	82	7	8	98	82	83	71	75	R	8	26	88	8	8	98	98	ਛ
ave Sr	8	L	20	8	88	88	8	8	8	8	8	82	12	ಜ	<u></u>	8	ಹ	78	35	8	22	84	88	81	79	69	8	<u>8</u>	8	8	8	88	8	8	98	8
1300	52	L		22	88	88	ਨ	88	88	82	8	88	75	91	82	8	8	92	<u></u>	8	8	8	8	79	9/	89	22	8	8	87	8	<u></u>	8	84	84	폐
dB) at	ន	L	£ <del>1</del>	F	8	82	8	87		8	8	8	8	8	8	8	П	П	62	29	74	Г	8	8		69		8	8	88	5		88	Т		8
SEL (	192	L	46	8	8	8	8	8	8	92	8	8	9	Γ	Г	8	Т	Т	Т	7		8	8		98	1/		8	8	T	$\vdash$	П	8	T	П	8
Banc	10 13	L		41 61	65	78	87 88	83	82	74 77	82	73 72	61 60	88	88	79				0/ /9	71 68	83	79 84	75 81	77 84	69 71	68 73	81	89		83	_	88		_	81
Mic	Γ.		Base	Base 4	Base	Base 7	Base	Т	Cavity 8	Base	Cavity	_	Base	П		_	Т	7	T	Base	L	-	Г	_		Base (	Cavity	Base	T	Т	Base (	Т	$\top$		_	Cavity
Event	П	Œ	0	0	30.5	19	30.5	30.5	30.5	61	61	19	61	30.5	30.5	15.2		30.5	30.5	61	19	15.2	15.2	30.5	30.5	61	19	30.5	19	30.5	30.5	30.5	15.2	15.2	30.5	30.5
Event	Type		Live Clay- more	Live Clay- more	Art. Sim.	Art. Sim.	Art. Sim.	_	Art. Sim.	Art. Sim.	Art. Sim.		Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Irt. Sim.	Art. Sim.										
Date E	_	$\vdash$	5/13 C	5/13 C C	5/5 A	T_	5/12 A	6/17 A	6/17 A	6/17 A	6/17 A	6/17 A	6/17 A	6/17 A		1						1	$\mathbf{I}$	5/13 A	5/13 A	5/13 A	5/13	5/4 A	П	١	5/4 A	100				5/27 A
Sol.	т.	T	103 12	103	Т	107 5	T	107	107	107	107	107	107	107	Т	1	${}^{-}$	Т	T-	Т	т	T	$\top$	125	125	125	125	Т	T	$\top$	Т	Т	Т	1	143	$\Box$
O		<u></u>	<u> </u>	1-	ΤΞ		١Ē	1-	<u> </u>	三	ت	ĪĒ	بت	±	١Ē	1=	1=	1=	1-	1-	1-	1=	1-	ι=	1=		1=	1=	1=	1=	1=	1=	1	ᄪ	1-	لت

F	3 00	)-1	3_																												_					_			
	Calc.	Overall	105 6	109.8	102.5	111.6	106.8	114.5	115.2	103.0	100.5	101.4	103.9	106.7	113.5	104.6	113.0	102.9	112.4	96.4	104.8	104.4	110.4	103.5	101.3	109.5	109.3	105.8	88.8	100.	2.6	99.8	0 00	0.50	F.00.	0.65	101.9	103.6	103.0
	$\top$	20000	T		T			76	73	99	49	29	29	79	79	76	77	64	74	57	59	20	73	64	69	22	74	72	26	7 %	3 8	PQ 47	<u> </u>	S &	3		ļ	2 2	0)
	Г	10001			Τ	Γ		Γ																					1			2   £				<u>ج</u> :	45 1	۽ ع	10
	90.07	00621	ă	12	8	83	83	8	77	75	58	29	71	84	84	82	81	73	78	65	79	75	22	72	99	09	77	78	29	2 2	5 3	2 2 2	3 2	S 4	<b>⊋</b>   €	ع ا	25	واع	70
	20007	0001	83	8 &	3 5	85	83	<u>a</u>	77	11	62	69	74	98	84	83	85	75	79	74	80	78	7.8	75	69	62	7.8	8	65	70 2	8 1	<u>و</u> و	5 8	8 2	<u>.</u>	\$ 6	3 8	2 2	72
		8 8 8	g	3 8	9	82	84	8	11	62	65	14	9/	82	82	84	84	22	80	74	81	62	62	92	7	99	7.9	85	8	2 2	B	9 2	≟ į		<u> </u>	3 2	29	₹ 3	\$
		300		<u> </u>	, p	8	88	88	8	65	29	74	178	98	98	84	8	78	85	75	81	80	8	82	72	66	81	83	8	3 8	3	2 3	3 5	2 2	1 8	ài	딕	3 3	\$
		2000	ă	£ &	8 8	8	88	8	8	8	69	75	79	98	88	82	87	6/	81	9/	85	18	88	8	74	92	85	82	8	ا و	8	1 2	<u>.</u>	£ 5	2 2	3	7	28	<u>\$</u>
		\$ \$		┰	Т	T	Т	Т	Т	Г									1						1	i i	i	ı		ı	- 1	62 12		- 1				- [	- [
		3120	2	3 8	3 8	8	82	88	88	잃	23	78	8	88	8	98	88	8	8	62	84	8	8	8	82	73	98	88	33	6	2	<u>ال</u>	약	2 2	<u>8</u>  3	2	ج إ	8	<u>&amp;</u>
		82	62	5 8	8 8	8	6	9	8	8	8	79	8	8	8	87	91	82	8	£	8	84	8	83	78	9/	98	88	7	8	2	8 8	2	2 2	<u> </u>	8	2	8	8
		g g	3	à a	3 8	8	8	ន	8	8	74	8	88	88	8	88	8	8	8	8	98	8	8	8	82	62	88	68	75	22	4	8 8	الا	2 2	듸	<u>8</u>	2	84	8
		<u></u>	8	8 8	3 2	8	88	8	8	8	75	<u>8</u>	98	88	8	68	94	82	8	8	98	8	8	8	8	88	8	88	75		2	8 3	5	2	2	8	2	8	8
		<u>22</u>	g	8 8	3 8	8	8	96	8	8	76	<u>8</u>	88	66	8	8	ક્ક	82	5	<u>~</u>	88	8	88	2	8	8	5	68	9/	1	2	<u></u>	g	<u>ا</u> ۾	4	98	ନ	8	8
		8	ç	8 8	3 8	3 8	8	96	8	æ	9/	8	88	68	ક્ષ	88	8	8	6	듄	87	83	ន	88	8	98	83	9	75	၉	2	8 8	2	<u>ور</u> ا	9	67	3	88	8
		8	3	òò	£ 2	1 8	8	88	26	8	15	8	8	88	88	8	26	8	8	8	87	88	98	8	8	5	92	68	9/	8	و	æ 8	8	<u></u>	8	67	8	88	88
		စ္တ		òò	£ &	3 8	8 8	6	8	88	75	듄	82	8	8	87	8	8	8	8	88	88	8	8	<u>~</u>	8	83	8	72	8	2	<u></u>	₃	<u></u>	8	8	8	8	88
		8	Į	6 8	ខ្ល	8	8 8	Ę	₽	8	1	8	88	82	₽	8	ē	88	흗	78	8	8	88	8	8	8	86	8	77	88	9	22	35	8	8	8	8	88	8
		\$	-	8 8	8 8	5 8	8 8	6	8	8	75	8	8	8	6	8	<u></u>	84	क	77	6	8	8	8	8	88	8	83	9/	8	3	ଛ ;	5	8	8	٥	≅	8	84
		315	- 1	8 3	≅ a	5 8	3 8	9	8	8	8	8	8	8	<u>=</u>	88	193	8	102	9	8	8	8	8	8	8	8	8	79	8	<u>8</u>	<u>و</u> ا	ă	8	<u></u>	82	8	84	88
		220	$\overline{}$	_	$\overline{}$	_	_	$\neg$	_	1	$\overline{}$	1	$\overline{}$	1	$\mathbf{T}$	7		-		$\Gamma^-$	Т	1	1				T .	1				\$	- 1				l ì	1	
		200																														82							
		160 5	_	3	2 2	ţ	3 5	=	1 =	8	88	9	용	မ္တ	112	8	Ξ	8	Ε	8	8	ક્ક	<u> </u>	8	16	<u>@</u>	5	8	84	101		87	- 1	8	호	2	8	8	6
		125	- 1	S S	8 8	Т	Т	3 8	8	8	8	88	8	8	8	8	8	8	5	88	ജ	16	8	8	5	8	5	33	88	8	8	8		П	8			35	
	Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	100	H	3 8	8 8	A 호	<u>}</u>  8	3 8	8 8	8	8	8	8	8	8	<u></u> 55	8	Т	T	Т	Т	Т	1	Т	7	Т	Т	Т	T	8		П		94		П	П		П
	ouence	80	$\vdash$	$\neg$	<u>≈</u> ε	_	╅	_	十	$\top$	┰	Т	8	Т	7	8	1	Т	Τ	Т	6	Т	Т	Т	7	8		Т	8	8		क्ष						Г	П
	nter Fr	63	П	Т	8 3	Т	Т	Т	Т	Т	Т.	Т	Т	Т	Т	T		Т	Т	Т	Т		1			1	1		8	84		П		8			Τ	6	П
	S E	20	П	T	S 8	┰	Т	Т	T	T	8	Т	Т	Т	Т	Т	Т	Т	Т	Т	T		T		T	T	T	T	Т			8				Г	8	Π	П
	Spectr	8	Н	_	$\neg$	$\neg$	8 8	_	_	┰	8 8	7	┰	8	T	8	Т	Т	T	₩ ₩	┰	5	Т	Т	2 &	Т	2 6	Т	1			$\Box$		П		П	Т		П
	ctave	器	П	$\neg$	Т	T	Т	Т	Т	Т	T	Т	Т	Т		1	Т			1		1	1	1	- 1	- 1	1	1		1		₩			' ا	1	2 87	9	П
	11/30	52	П	T	3 8	Т	3 8	Т	┰	┱	3 2	Т	7	<u></u>	Т	Т	Т	8	Т	Т	Т	8	Т	Т	3 2	Т	Т	Τ-	2					88		8	79 85	П	82
	(B)	8	П		8 8	$\neg$	7	┰	┰	_	3 8	Т	┰	Т	Т		Т	T	7	Т	Т	. 8	Т	Т	Т	1 2	Т	3 8	Т		08	П	7 74	Т	76 7	88	T	1	8
	d SEL	9 ~	П		8 3 -	Т	1	Т	7				1	T					1	1	1	3 8	2 8	Т	Т	8 8	Т	86 87	Т	T		76 7	22 9	П	74 7	Г		85	П
	g	10 13		_		_	3 2	_	3 8	<del>-</del>	_		Ţ	3 S			-		_	_	2 8	7	00		_	_			_	_	73 7	_	_	_	74 7	_	_	82 8	_
	Mic	Pos.	П	$\neg$		丁	T	_	$\neg$	Dage	Т	Race	Race	Т	Τ.	$\neg$	Т	_	T.		Bace	Baco	Odse	Cavity	Dase	Dase		_	Base	Cavity	Base	Base	Cavity	Base	Cavity	Base	Base	Base	Base
	Event	Dist.	(E)	15.2	15.2		30.5	S 5	G.D.	5 2	2 2	<u> </u>	5 2	5 5					5 4	5 2	2 6	3 6	200			ة ة				19	122	50			_		_		15.2
	Event	Т		Art. Sim.	Sim.	Sim.	E C	E G	E I	Art. Olli.	, i			Art Cim	i din	Art Sim			Art Cim	1 Call.	Art Cim	Art Cim	Aft. Offil.			Art. Sim.	All. Olli.			Sin.	Art Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.
	Date le	_	T		$\overline{}$	T		_		/1/0	$\neg$	┰	┰	Т		5 6	Т	Т	3 3	Т	١.	- 1	. 1.	7		_ [	2 2	Т		1	4/23	1	19	Т	Τ	Τ	T	Т	2/9
	Sel.	Т	T	143 5	$\neg \tau$		_	$\neg$	_	2 5	_	┰	7 5	Т	┰	7	Т	Т	7	$\neg$	Т	_	Т	┪	7	Т	> F	┰	Τ.	1	g	┰	22	_	7	1	T	Т	$\top$
	JO	1	Ε.	-	- 1	-1	- 1	- L	-1	- 1	- 1-		- 17	-1-	-   -	- Ľ	-1:	<u>- 17</u>	-   *	~   *	-17	-17	-1	-1	-1	<u>- 1'</u>	- (	<u>ت</u> ــــ			1	,	تند	1	ᅩ	끅	تب		لنيا

Control   Cont																																						·	Er	RL T
Part	Calc.	Overall	SEL	109.0	108.6	104.0	101.2	108.8	97.7	99.1	107.3	113.8	114.5	106.4	103.2	97.7	101.0	103.6	104.1	107.8	101.6	105.0	107.8	100.3	103.3	104.6	102.7	108.7	9.701	98.3	105.6	110.7	102.1	109.2	113.5	117.5	103.6	109.7	94.9	101.5
Part		20000		92	73	72	61	29	37	37	69	78	75	71	68	25	99	99	28	89	66	92	71	22	63	69	69	71	51	56	29	74	58	89	78	81	69	74	45	63
1,100   1,10		16000		178	75	92	29	20	38	20	74	80	78	74	72	26	0.2	09	09	02	71	62	73	65	65	1/	73	73	51	29	0.2	9/	63	20	82	84	72	9/	53	88
The care   Car		_		79	92	62	1.1	71	32	54	77	81	80	75	75	61	73	62	63	71	74	81	74	62	89	74	74	74	52	62	72	77	99	71	82	82	74	78	57	99
The color   Court				81	22	80	73	72	41	69	80	83	81	79	80	64	26	63	64	73	9/	82	92	99	72	81	92	75	26	65	74	78	69	72	98	82	9/	79	09	89
Type   Clark   Clark   Micro   Read SEL (Clig at 15 Course Special months of the course of the cou		_		85	29	81	74	73	47	83	84	84	83	8	80	29	28	65	65	74	22	85	77	29	74	81	9/	9/	29	89	22	79	72	73	88	87	28	8	64	68
Type   Dieta   Frent   Michael   Band-SEL (48) at 13 Chates Spectrum Center Frequencies (14)   Type   Dieta   Dieta   Sec.   Type   Dieta   Dieta   Sec.   Type   Dieta   Dieta   Sec.   Type   Dieta   Diet				83	79	181	7.5	7.5	51	64	83	82	84	81	81	89	79	29	29	75	11	83	79	20	11	85	79	11	19	2	79	81	73	74	88	88	78	88	67	8
Type   Dist.   Pearl   Mic.   Band SCI, (48) at 13 Octave Special micror Propagations (14)   Type	I							Г																															П	
Type   Fueri   New   Mic   Sear-SER (69) at 13 Octaves Special model of the sear SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13 Octaves Special model of the sea SER (69) at 13																																						1	1	
Type   Cheen   Cheen																																								
Type   Cheff   Cheff   Moc   Shareh Schellun Center Frequencies (H)   Type																																						l	1	1 1
Type   Dist.   Pers.   Mic.   Band SEL (dB) at 1/3 Cotave Spectrum Certae Frequencies (4-)   Type   Dist.   Pers.   Dist.   Pers.   Dist.   Pers.   Dist.   Pers.   Dist.   Pers.   Dist.   Dist.   Pers.   Dist.   Dist.   Pers.   Dist.		1600							Г	П	Г														Г													Π		П
Type   Dail   Event   Mic.   Baard SEL (dB) at 1/3 Cotave Spectrum Center Fraquentice (Hz)   Type   Dail   Type	0 1250		94	91	88	6/	87	જી	R	88	94	35	68	83	74	85	85	85	98	81	88	68	22	8	98	84	87	80	22	82	91	8	88	8	88	8	8	74	-	
Type   Dist   Event   Mic   Band SEL, GB] at 13 Octave Specturn Center Frequencies (Hz)   Type   Dist   Poss   10   10   15   62   12   12   13   13 Octave Specturn Center Frequencies (Hz)   Type   Dist   Poss   10   10   15   62   12   13   13 Octave Specturn Center Frequencies (Hz)   Type   Dist   Type		$\vdash$							i -																F									l	1	ı				П
Type   Dist   Event   Mac   Band SEL, (GB) at 1/3 Octaves Spectrum Center Frequencies (Hz)   Type   Dist   Poss   10   13   15   Octaves Spectrum Center Frequencies (Hz)   Type   Dist   Poss   10   13   15   Octaves   10   13   Octaves Spectrum Center Frequencies (Hz)   Type   Dist   Type   Ty									П	П						$\Box$																						Γ.	i -	
Type   Dist   Post																												ĺ					ı	1		۱.۸		l	ı	
Type   Dist.   Post.   Hold   Ramd SEL (dB) at 1/3 Octave Spectrum Camiler Frequientines (Hz)   Hz   Post.   Hz   Hz   Ramd SEL (dB) at 1/3 Octave Spectrum Camiler Frequientines (Hz)   Hz   Hz   Hz   Hz   Hz   Hz   Hz		-		_					<b></b>			Ι																				_		I	г	_	Г			П
Property   Character   Chemit Mic   Rand SEL (AB) at 13 Octave Spectrum Center Frequencies (Hz)   Property		_			_			_				П															П		П								8	જ	75	83
Propertion of the control of		520		87	68	88	<u>8</u>	88	11	73	85	103	104	35	68	72	85	78	78	66	81	8	8	85	87	8	82	88	82	81	68	휻	æ	8	ස	113	6	ਨੁ	ge.	86
Date Event         Event         Mic         Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (H2)           Type         Dist.         Posc.         10         3         16         20         25         32         40         50         60         100         100           677         Art. Sim.         (152)         Cavity         94         16         20         25         32         40         50         60         100         100           677         Art. Sim.         (152)         Cavity         74         87         91         86         86         86         86         86         86         87         89         97         99         99         90		88		5	104	8	8	55	72	9/	ន	8	91	96	8	85	87	8	<u>6</u>	105	92	8	55	92	8	æ	56	28	<u>8</u>	84	8	8	æ	<u></u>	102	Ξ	ន	5	8	95
Parent         Event         Milko         Band SEL (GB) at 1/3 Octave Spectrum Center Frequencies (Hz)           Type         Dist.         Poss.         10 13 16         20 125         32 40         50 65         60 100           67 Art. Sim.         (Im)         (Im)         13 16         20 125         32 40         50 65         80 100         10 100           67 Art. Sim.         (Im)         (Im)         13 16         80 86         80 86         80 87         80 87         80 87         80 97         90 97           67 Art. Sim.         61 G. Cavity         74 87         80 87         80 86         80 87         80 87         80 97         90 97         90 97           67 Art. Sim.         61 G. Cavity         80 87         81 87         80 88         80 87         80 88         80 97										_	1								1																					
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62		_	L							$\overline{}$	$\overline{}$	Г							1												I		Ĺ	Ł	i .					1 1
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	Sies (F.	<u>\$</u>	L																																					
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	edneuc	8	H																																					
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	anter Fi	63	$\vdash$	ı		l	l .	ı			1					1										ł			1				ı		1		1		1	
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	trum	0	-			_	1		Г		$\overline{}$				_						_	1			I	1			T	T	I			1	1		1	Ł	1	
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	e Spec	32																																						
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	Octav	83		1																																				
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	) at 1/3	8			ı		ı	i .	t						1		ł	ı	1	•		I	ı	ı	1	1			1	ı	ı	1	1	1						
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	EF (48	92		Г			_		1	1		$\overline{}$		$\overline{}$							-	$\overline{}$		_	$\overline{}$	$\overline{}$	$\overline{}$			1	1		$\overline{}$	Г-	$\mathbf{I}$	<u> 2</u> 2	8	ಜ	74	85
Date         Event         Event         Mic           17pe         Dist.         Pos.         10           677         Art. Sim.         15.2         Cavity 74           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         30.5         Base 66           677         Art. Sim.         61         Cavity 63           677         Art. Sim.         16.2         Base 84           677         Art. Sim.         16.2         Base 84           678         Art. Sim.         16.2         Cavity 63           678         Art. Sim.         16.2         Cavity 86           678         Art. Sim.         30.5         Base 85           678         Art. Sim.         30.5         Base 62           576         Art. Sim.         30.5         Base 62           570         Art. Sim.         30.5         Base 62           571         Art. Sim.         61         Base 62	Band S	13		9	8	8	92	ස	33		1			ı				•			ı			1		ı.		1			ı			ı.	1	န	2	28	7	<u></u>
Date         Event         Event           Type         Dist.           677         Art. Sim.         15.5           677         Art. Sim.         30.5           677         Art. Sim.         61           422         Art. Sim.         61           423         Art. Sim.         15.2           576         Art. Sim.         16.2           578         Art. Sim.         16.2           578         Art. Sim.         16.2           578         Art. Sim.         16.2           578         Art. Sim.         16.5           578         Art. Sim.         61           6/18         Art. Sim.         61           6/11         <	F	은	L				1	1																												L	т	Т	T	$\Box$
677 667 677 667 677 667 667 667 667 667	- 1	П	L	Cavit	Cavit	Base	Base	Cavit	Base	П	П	Т	Г			Г	$\Box$	Г	П		T	Т	Г	1	П		Т-	1	1				Г	П	T	Т	Т	Т	П	T
677 667 677 667 677 667 667 667 667 667	Event	Dist.	Œ	15.2	30.5	30.5	61	. 61	244	122	15.2	15.2	30.5	30.5	30.5	- 61	30.5	61	91	5	- 61	30.5	30.5	122	19	30.5	30.5	30.5	19	19	30.5	30.5	19	19	15.2	15.2	30.5	30.5	<u>-</u>	19
677 667 677 667 677 667 667 667 667 667	Event	Type		Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sim	Art. Sirr					
S   S   S   S   S   S   S   S   S   S	Date								•	4/27	5/26	97/5	5/26	5/26	9/9	5/10	5/12	6/18	6/18	8/18	6/18	6/18	6/18	4/23			6/11	6/11	6/11	6/11	6/11	6/11								$\Box$
	8		L	흂	惡	<u>≅</u>	쯆	흂	<del>1</del> 8	184	\$	\$	<u>\$</u>	<u>\$</u>	197	197	197	191	197	197	197	197	191	86	£	8	8	85	8	8	8	88	88	8	8	88	8	8	<u>8</u>	<u>8</u>

-											_												-			_										_		_	
Calc.	Overall	SEL.	103.1	104.3	104.0	102.5	103.6	102.4	104.6	107.5	103.3	106.5	101.0	102.3	106.7	96.0	102.6	92.7	97.3	93.7	103.8	 	107.0	110.1	106.1	110.4	104.5	109.9	107.3	105.4	101.7	105.4	101.4	105.8	104.8	102.0	102.1	105.4	
	20000		58	. 29	73	29	29	65	89	69	99	89	25	72	74	29	68	29	64		22	99	71	72	71	29	89	9/	88	7	54	7.1	69	72	14	69	64	89	
	16000		64	69	9/	69	74	71	11	14	70	2	23	22	72	64	89	25	92	32	69	8	79	76	75	20	71	92	2	74	29	73	7	73	73	11	64	8	
	12500		69	02	80	69	75	74	72	72	73	69	64	8	74	88	29	29	29		65	9	82	69		1/	73	78	71	9/	64	73	73	74	74	7.3	છ	71	
	10000		74	74	81	72	11	11	73	73	75	29	29	<u></u>	84	4	81	7.	9/	34	11	63	8	32	78	72	9/	79	72	78	69	69	7.5	75	75	75	88	72	
	8000		76	71	83	72	80	79	75	74	78	20	20	8	85	74	29	72	75	41	72	99	85	85	79	74	78	79	75	79	72	92	9/	1	75	82	۶	74	
	6300	L	78	11	84	73	88	65	92	9/	£.	74	73	83	85	92	8	73	9/	44	72	69	200	83	200	35	8	81	72	18	74	92	78	12	1	22	73	155	
	2000		8	92	8	74	잃	ぁ	11	1	<u>=</u>	9/	7.5	83	85	92	8	74	2/2	25	62	88	8	82	8	14	20	83	22	8	9/	92	62	92	R	8	74	92	
	0 4000	L	_	П	-	1		Г	1	$\mathbf{r}$	1			1 1					•	1	i	l .	i		Ι.		1				l	ı	ı	ı	1	<u> </u>	1	1	-
	0 3150	-	Т	1	_		Г	Т	Г	П	Т					١ ١		1	1	1	1	ı	1	1		1	l l	l		l	ı	l l	ı		ı	8	1	1	1
	0 2500	$\perp$	1		г	7	П	1	T	Т	Т	Г	i					ı	i	1	1	l	1	1	1		ı	l.		1	ı	1	1	1	1	8	1	Į.	1
	1250 1600 2000	+	_			т	Т	Г	Т	1	T	П	T .					ı	ı	•	1	ŀ	1	1	ı	1	1	ı .	١.	ı		1	1	1	•	8	1	ı	1
	30 160	+	_	1	Т	-	1	Т	т	Т	Т	Т	Γ			I		Г	1	1	ı	ı	1	ı		1	L	1		ı	1	1		1	1	88	1		1
				_	_	т	т	Т	Т	Т	Т	Т		T				1	l	1	i	1	1	1	1	ŀ	1	1	1	1	l		1	1	1	8	1	1	1
H	1000	_		_	_	Ŧ	$\overline{}$	_	$\overline{}$	_	_	т-	1	_	i	1		1	1		1			1		1			1		1	1		- 1		3 6	1		1
	080	┰	$\mathbf{T}$	$\overline{}$	$\overline{}$	Т	T	$\overline{}$	т	1	_	1		1	•	ı		1	1	1		1	1	1	1		1	1	1	1	1	1		1		8 8	1	1	1
	500 630	7	_	$\overline{}$	${}^{-}$	_	Т	$\overline{}$	T	$\neg$	Т.	1	1	1		1	l		1	ı		1	1		1	1	ı	1	1	1	1	1	1	1		68	1	1	1
	400	Т	_	_	_	$\top$	$\overline{}$	_	_	$\overline{}$	_	1	$\mathbf{I}$	T	1	ı		1	1	١.	1		•		1	1		1		1		1				8 8			
	215 14	_																																		3 8			
	250	Т																																		5 8			
	000	Ŧ	_	_	_	_	_	_	_			1																								8			
	180	3	2	83	8	8	8	8	8 8	۽ اِ	3	≅	8	8	202	8	6	22	8	F	8	ă	5 8	3   5	1 3	٤	8	8	8	8	g	8	100	à   à	5 8	<u> 8</u>	1 5	; 8	3
	5 (TZ)	3	8	8	8	<u> </u>	8	3 5	6	<u> </u>	8	Ē	8	8	8	8	æ	=	2	ä	8	8	8 8	3 8	3 8	3 6	<u> </u>	8	ि	8	8	3 2	8	8 8	8 8	8 8	3 8	<u> 8</u>	3
1	(Z) (S)	3	8	8	8	2	8	8	3 2	3 3	5 8	8	5	क्ष	8	8	8	8	R	12	5 S	3 8	8 8	3 3	3 8	3 8	8 8	8	8	8	8 8	4   æ	3 8	3 8	8 8	Т	Т	8 8	7
		8	8	8	8	:  2	8	3   5	8	3 8	3 8	8	8	8	18	8	æ	8 8	2	g	3 6	3 8	8 8	Т	Т	Т	Т	8	Т	Т	Т	Т	Т	Т	Т	_	8 8	Т	7
		3	g	3 2	8	3   2	g	Т	3 8	Т	Т	8 8	Т	Т	Т	Т	Т	Т	Т	Т	Т	Т	Т	<u> </u>	Т	Т	Т	; lg	Т	Т	Т	T	Т	8 8	Т	3 6	Т	3 8	7
d		8	ē	┰	Т	Т	Т	Т	3 8	Т	Т	Т	Т	8	Т	12	Т	Т	Т	Т	3 8	Т	Т	Т	T		Т	18	Т	7	Т	3 6	Т	8 8	Т	Т	Т	Т	5
	Special Specia	<b>₽</b>	8	Т	Т	3 2	Т	Т	8 8	Т	Т	Т	Т	8 8	1	Т	Т	Т	Т	Т		Т	Т	א פֿ פ	Т	8 8	Т	5 S	Т	8 8	Т	8 8	Т	26 E	Т	Т	Т	3 S	٦.
	Ctave	8	8	7	Т	3 8	Т	Т	Т	Т	0 4	Т	T	8 8	Т	Т	Т	2 2	Т	Т	8 8	Т	10 C	T	Т	Т	Т	60	Т	Т	Т	Т	Т	Т	23 3	Т	Т.	Т	ڪ ڇ
	at 16	8	8	8 8	Т	Т	8 6	Т	Т	Т	2 2	Т	Т	3 8	Т	Т	Т	5 6	7	Т	Т	Т	2 2		Т	8 8	Т	Т	8 8	Т	3 5	Т	Т	П	3 8	$\neg \Gamma$	Т	g	╗
	9	9	5	Т	Т	Т	8 8	Т	Т	Т	5 8	7	Т	3 8	Т	Т	Т	3 8	Т	Т		Т	8	Т	Т	Т	3 8	Т	Т	Т	5 2	Т	7	T	Т	_	2 3	Т	8
ľ	დ [	Т	$\neg$	9 8	Т	Т	Т	\$ 8	Т	Т	g	Т	Т	3 2	Т	Т	Т	0 2	5 6	2 2	8	,	25	5 8	3 8	2	3 8	8	8 8	5 8	8	3 8	3			8	3 8	2	<u> </u>
ľ		은 유		3 2	8 8	3 8	à	\$ 3	\$ 5	8 8	3 3	\$ K	2 8		3 6	. 8	į	ŧ [	3 5	_	3 8	_		_							Т	3 3	$\overline{}$			$\neg$	- 1	8	
. [	7	SS.	-	aseq	Cavity	pase	Cawity	Pase	Pase	Cavid	Cavily	nase		200	Case	Cavity Base	C C	S S	Dase	S C	ase Pase	pase	Base	П	$\neg$	Base	Cawity	Pase	٦	T	pase	Base	Cavily	Base		$\neg$	$\neg$	Base	Cavity
	Event	ist Ö			ر ا				22			3	ا ۽	٤		7 6		<u> </u>	اة	<u>.</u>	₹ 3	٥	91.5	22	12.2	89	30.5	20		S 5	3	<u></u>			15.2	30.5		5	삘
	Event	Type		Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Ar. Sim.	Ar. olm.	All Ollin	Aff. Olm.	Alt. Ollil.	Art. Sim.	Art. Sim.	An. vim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	AT. SIE	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim.	Art. Sim. 61
	Date				- 1	- 1	- 1		٠,		-1			200						•			- 1								- 1	- 1			5/11	5/11	- 1		5/11
	<u>3</u>			$\neg$	83	┰	┪	_	_	$\neg$	<sub>器</sub>	7	Т	Т	Т	Т	Т	П	Т					$\neg$	$\neg$	$\neg$	_1	Т	7	3	3	ន	231	236	236	536	38	236	236
	لت								_		_																		_				_					-	

Table D 3. Summary data for experimental .50 caliber blank fire on Fort Stewart, GA.

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem	Mic	SEL (dB)	
JUI.	Dale	Phase	Туре	Dist.	re.	Resp.	(min)	TOTAL STATE OF THE	Pos.	OEE (00)	
		& Day	liybe	(m)	DOF	ncop.	((,,,,,,,		03.	Flat	Α
 3	4/21	1-1	.50 cal.	61	90	2	1.7		Base	90.1	84.3
- 6	L	-1	.50 cal.	61	90	2	1.7		Base	89.1	83.7
6		1-1	.50 cal.	61	90	2	1.7		Base	90.8	84.8
 6	L	N-0	.50 cal.	91.5	90	2	10.8		Base	94.9	79.4
6	<u> </u>	N-0	.50 cal.	91.5	90	2	10.8		Base	84.3	77.6
6	L	N-0	.50 cal.	91.5	90	2	10.8		Base	83.1	74.5
6	4/29	N-0	.50 cal.	91.5	90	2	10.8		Base	85.1	78.4
6	4/29	N-0	.50 cal.	91.5	90	2	10.8		Base	85.5	78.1
6	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.	l		Base	100.8	95.7
6	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.5	94.7
6	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	107.9	98.0
6	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	108.0	97.9
6	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Base	92.5	87.6
6	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Base	91.0	85.8
6	5/27	Post-fled.	.50 cal.	61	90	Post-fled.	<u> </u>		Cavity	103.3	92.4
6	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	101.9	91.0
6	5/27	Post-fled.	.50 cal.	122	90	Post-fled.	<u> </u>		Base	84.8	79.5
6	5/27	Post-fled.	.50 cal.	122	90	Post-fled.			Base	85.3	79.5
6	5/27	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	95.0	83.9
6	5/27	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	95.2	84.1
10	5/24	I-10	.50 cal.	30.5	90	2	13.6		Base	101.1	96.6
10	5/24	I-10	.50 cal.	30.5	90	2	13.6		Base	102.3	97.8
10	5/24	I-10	.50 cal.	30.5	90	2	13.6		Base	101.0	96.5
10	5/24	I-10	.50 cal.	30.5	90	2	13.6		Base	101.0	95.9
10	6/23	Post-fled.	.50 cal.	15.2	0	Post-fled.			Base	103.2	98.6
10	6/23	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	107.8	97.8
10	6/23	Post-fled.	.50 cal.	15.2	0	Post-fled.			Base	103.7	98.9
10	6/23	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	108.1	98.1
10	6/23	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	107.1	96.2
10	6/23	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	100.7	93.7
10	6/23	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	107.9	96.7
10	6/23	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	101.4	94.1
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Base	96.8	88.7
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Cavity	104.2	92.4
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Cavity	95.5	84.0
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Cavity	103.1	91.3
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Base	89.6	81.2
		.1					-t	J		-	

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF	·				Flat	4
10	6/23	Post-fled.	.50 cal.	45.7	0	Post-fled.			Base	95.4	87.0
10	6/23	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	102.3	90.6
10	6/23	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	108.6	96.9
10	6/23	Post-fled.	.50 cal.	61	0	Post-fled.			Base	92.8	84.5
10	6/23	Post-fled.	.50 cal.	61	0	Post-fled.			Base	99.3	91.2
10	6/23	Post-fled.	.50 cal.	122	0	Post-fled.			Base	84.7	76.9
10	6/23	Post-fled.	.50 cal.	122	0	Post-fled.			Base	81.7	73.9
10	6/23	Post-fled.	.50 cal.	122	0	Post-fied.			Cavity	93.7	81.4
10	6/23	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	91.1	83.2
12	4/28	1-1	.50 cal.	122	90	0			Base	84.9	80.1
12	4/28	I-1	.50 cal.	122	90	0			Base	84.1	79.5
12	4/28	j-1	.50 cal.	122	90	0			Base	84.6	79.5
12	4/28	I-1	.50 cal.	122	90	0			Base	83.8	78.2
12	6/11	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	107.3	104.3
12	6/11	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.4	105.3
12	6/11	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100:5	96.2
12	6/11	Post-fled.	.50 cal.	61	90	Post-fled.			Base	97.8	92.7
12	6/11	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	112.1	105.1
12	6/11	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	106.8	96.8
12	6/11	Post-fied.	.50 cal.	122	90	Post-fled.			Base	87.2	80.4
23	4/28	I-3	.50 cal.	122	90	0			Base	86.5	79.6
23	4/28	I-3	.50 cal.	122	90	0		·	Base	87.4	80.7
23	4/28	I-3	.50 cal.	122	90	0			Base	87.4	80.2
23	4/28	1-3	.50 cal.	122	90	0			Base	88.4	81.6
23	5/3	1-8	.50 cal.	30.5	90	0			Base	90.2	82.7
23	5/3	I-8	.50 cal.	30.5	90	0			Base	93.0	84.8
23	5/3	I-8	.50 cal.	30.5	90	0			Base	92.9	83.9
23	5/3	1-8	.50 cal.	30.5	90	0			Base	95.3	86.6
23	5/3	I-8	.50 cal.	30.5	90	0	<u> </u>		Base	96.3	87.6
23	5/3	1-8	.50 cal.	30.5	90	0			Base	97.0	87.9
23	5/3	I-8	.50 cal.	30.5	90	0			Base	99.4	90.7
23	5/3	I-8	.50 cal.	30.5	90	0			Base	98.5	89.6
23	5/6	N-0	.50 cal.	15.2	90	2	5.6		Base	96.8	92.5
23	5/6	N-0	.50 cal.	15.2	90	2	5.6		Base	108.3	102.6
23	5/6	N-0	.50 cal.	15.2	90	2	5.6		Base	101.8	96.1
23	5/6	N-0	.50 cal.	15.2	90	2	5.6		Base	108.0	102.4
23	6/14	Post-fled.		15.2	0	Post-fled			Base	106.3	102.8
23	6/14			15.2	0	Post-fled			Base	107.3	104.0
23	6/14	Post-fled.	.50 cal.	15.2	0	Post-fled	·		Base	108.2	104.8

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
	1	Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	Α
23	6/14	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	117.2	107.0
23	6/14	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	118.1	107.9
23	6/14	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	118.9	108.7
23	6/14	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	116.8	105.4
23	6/14	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	119.4	108.0
23	6/14	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	102.4	95.7
23	6/14	Post-fled.	.50 cal.	30.5	0	Post-fied.			Base	101.3	94.0
23	6/14	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	103.2	95.7
23	6/14	Post-fled.	.50 cal.	61	0	Post-fled.			Base	94.8	86.6
23	6/14	Post-fled.	.50 cal.	61	0	Post-fled.			Base	95.5	87.7
23	6/14	Post-fled.	.50 cal.	61	0	Post-fled.			Base	93.8	86.0
23	6/14	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	116.8	104.3
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	96.0	83.8
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	99.5	86.9
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	100.9	88.2
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Base	81.6	75.3
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Base	84.0	77.3
23	6/14	Post-fled.	.50 cal.	122	0	Post-fled.			Base	85.0	78.4
30	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	91.0	85.9
30	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	91.7	86.5
30	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	104.1	95.1
30	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	105.0	96.7
30	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	112.5	104.3
30	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	104.6	102.2
30	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	95.1	90.5
30	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	98.1	93.6
30	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	104.5	96.4
30	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	107.7	99.8
36	5/19	N-1	.50 cal.	61	90	2	2.1		Base	89.6	82.9
36	5/19	N-1	.50 cal.	61	90	2	2.1		Base	90.9	84.2
36	5/19	N-1	.50 cal.	61	90	2	2.1		Base	90.8	83.6
36	5/19	N-1	.50 cal.	61	90	2	2.1		Base	90.8	84.1
36	5/19	N-1	.50 cal.	61	90	2	2.1		Base	91.4	84.8
36	5/21	I-8	.50 cal.	91.5	90	1			Base	89.4	84.6
36	5/21	1-8	.50 cal.	91.5	90	1			Base	89.5	84.8
36	5/21	1-8	.50 cal.	91.5	90	1			Base	90.1	84.9
36	5/21	1-8	.50 cal.	91.5	90	1			Base	89.4	84.4
36	5/21	1-8	.50 cal.	91.5	90	1			Base	92.2	86.9
36	5/21	I-8	.50 cal.	91.5	90	1			Base	91.8	86.7

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,,	(m)	DOF	·	<u> </u>			Flat /	4
36	6/15	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.8	100.3
36	6/15	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	113.3	107.0
36	6/15	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	110.9	103.4
36	6/15	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	101.1	95.2
36	6/15	Post-fled.	.50 cal.	61	90	Post-fled.			Base	91.0	83.8
36	6/15	Post-fled.	.50 cal.	61	90	Post-fled.	-		Cavity	101.0	94.6
36	6/15	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	95.3	89.0
36	6/15	Post-fled.	.50 cal.	122	90	Post-fled.			Base	85.1	79.0
36	6/15	Post-fled.	.50 cal.	15.2	90	Post-fled.	<del>                                     </del>		Cavity	107.9	104.4
36	6/15	Post-fled.	.50 cal.	15.2	90	Post-fled.	<del> </del>		Base	105.9	103.3
36	6/15	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.0	95.7
36	6/15	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	102.9	100.1
36	6/15	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.4	92.3
36	6/15	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	98.7	96.7
36	6/15	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	92.5	89.3
36	6/15	Post-fled.	.50 cal.	122	90	Post-fled.			Base	87.9	81.5
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Base	95.4	88.7
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.	-		Base	93.7	86.5
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Base	93.3	86.3
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	110.2	96.5
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	108.6	94.7
44	5/27	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	108.5	94.4
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	102.1	96.0
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	101.3	95.0
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	98.7	92.5
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	115.7	102.9
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.9	102.2
44	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	112.9	99.9
44	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	106.2	. 101.8
44	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.8	101.1
44	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled			Base	104.7	99.8
44	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled			Cavity		104.3
44	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled			Cavity		103.9
44	5/27	·	.50 cal.	15.2	90	Post-fled			Cavity		103.0
51	4/27	N-0	.50 cal.	122	90	1			Base	85.2	80.8
51	4/27	N-0	.50 cal.	122	90	1			Base	82.4	77.4
51	4/27	N-0	.50 cal.	122	90	1			Base	75.7	70.6
51	4/27	N-0	.50 cal.	122	90	1			Base	79.9	74.9
51	4/27	N-0	.50 cal.	122	90	1			Base	82.5	78.6

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF	-	:			Flat	Α
51	4/27	N-0	.50 cal.	122	90	1			Base	82.4	78.0
51	4/29	N-2	.50 cal.	61	90	0			Base	93.4	85.8
51	4/29	N-2	.50 cal.	61	90	0			Base	93.7	86.1
51	4/29	N-2	.50 cal.	61	90	0			Base	93.5	86.0
51	4/29	N-2	.50 cal.	61	90	0			Base	93.3	86.0
51	4/29	N-2	.50 cal.	61	90	0			Base	93.5	86.0
51	4/29	N-2	.50 cal.	61	90	0			Base	93.0	85.8
51	4/29	N-2	.50 cal.	61	90	0			Base	93.7	86.1
51	4/29	N-2	.50 cal.	61	90	0			Base	93.6	86.3
51	5/3	N-3	.50 cal.	30.5	90	2	1.9		Base	94.4	88.2
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.9	102.2
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.8	102.2
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.4	102.1
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	117.6	108.3
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	117.5	108.3
51	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	116.8	107.8
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.	7		Cavity	114.7	106.3
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.4	106.0
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.5	105.7
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	102.3	98.7
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	101.7	95.8
51	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	101.6	95.5
52	5/13	Inactive	.50 cal.	15.2	90	Inactive			Cavity	110.5	101.5
52	5/13	Inactive	.50 cal.	15.2	90	Inactive			Base	105.3	102.1
52	5/13	Inactive	.50 cal.	30.5	90	Inactive			Cavity	107.4	97.6
52	5/13	Inactive	.50 cal.	61	90	Inactive			Cavity	99.6	91.1
52	5/13	Inactive	.50 cal.	61	90	Inactive			Base	93.7	88.6
52	5/13	Inactive	.50 cal.	15.2	90	Inactive			Base	100.4	97.9
52	5/13	Inactive	.50 cal.	15.2	90	Inactive			Cavity	105.8	101.4
52	5/13	Inactive	.50 cal.	30.5	90	Inactive			Base	92.6	90.0
52	5/13	Inactive	.50 cal.	30.5	90	Inactive			Cavity	99.5	94.8
52	5/13	Inactive	.50 cal.	61	90	Inactive			Cavity	97.9	92.9
52	5/13	Inactive	.50 cal.	61	90	Inactive			Base	92.9	88.3
53	5/4	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.9	101.6
53	5/4	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	113.0	105.3
53	5/4	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.7	105.4
53	5/4	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	99.5	94.7
53	5/4	Post-fled.	.50 cal.	61	90	Post-fled.			Base	90.4	85.8
53	5/4	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	110.1	101.1

78

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	A
53	5/4	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	112.0	103.6
53	5/4	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.5	100.5
53	5/4	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	98.7	95.6
53	5/4	Post-fled.	.50 cal.	30.5	90	Post-fled.	_		Base	110.2	101.1
53	5/4	Post-fled.	.50 cal.	61	90	Post-fled.			Base	108.7	98.3
53	5/4	Post-fled.	.50 cal.	61	90	Post-fled.			Base	91.2	84.5
53	5/5	1-1	.50 cal.	30.5	90	0			Base	106.0	99.2
53	5/5	1-1	.50 cal.	30.5	90	0			Base	100.0	93.0
53	5/10	1-6	.50 cal.	15.2	90	0			Base	106.7	102.2
53	5/10	1-6	.50 cal.	15.2	90	0			Base	107.2	102.5
53	5/10	1-6	.50 cal.	15.2	90	0			Base	107.4	102.2
53	5/10	I-6	.50 cal.	15.2	90	0			Base	107.2	102.5
53	5/12	I-8	.50 cal.	30.5	90	0		Replication of 1st 30.5 m trial	Base	98.3	93.4
53	5/12	I-8	.50 cai.	30.5	90	0		Replication of 1st 30.5 m trial	Base	101.1	94.7
53	5/12	1-8	.50 cal.	30.5	90	0		Replication of 1st 30.5 m trial	Base	101.6	94.7
53	5/12	1-8	.50 cal.	30.5	90	0		Replication of 1st 30.5 m trial	Base	103.1	96.5
53	5/12	I-8	.50 cal.	30.5	90	0		Replication of 1st 30.5 m trial	Base	103.7	97.4
53	5/12	1-8	.50 cal.	30.5	90	0		Replication of 1st 30.5 m trial	Base	105.3	98.7
57	4/21	I-6	.50 cal.	61	90	2	2.8		Base	86.8	81.7
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	85.2	79.8
57	4/21	I-6	.50 cal.	61	90	2	2.8		Base	85.8	80.5
57	4/21	I-6	.50 cal.	61	90	2	2.8		Base	86.0	80.2
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	86.4	81.5
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	87.4	83.3
57	4/21	I-6	.50 cal.	61	90	2	2.8		Base	91.4	
57	4/21	I-6	.50 cal.	61	90	2	2.8		Base	91.3	
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	90.7	
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	91.1	
57	4/21	1-6	.50 cal.		90	2	2.8		Base	91.3	
57	4/21	1-6	.50 cal.	61	90	2	2.8		Base	91.3	
57	4/21	1-6	.50 cal.		90	2	2.8		Base	91.4	
57	4/26	N-0	.50 cal.	122	90	0			Base		1
57	4/26	N-0	.50 cal.	122	90	0			Base		
57	4/26	N-0	.50 cal.		90	0			Base		
57	4/26	N-0	.50 cal.	122	90	0			Base		
57	4/26	N-0	.50 cal.		90	0			Base		
57	4/26	N-0	.50 cal.	122	90	0			Base	82.4	75.8

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	Α
57	4/26	N-0	.50 cal.	122	90	0			Base	81.9	75.0
57	4/30	N-4	.50 cal.	91.5	90	2	10.9		Base	85.9	81.2
57	4/30	N-4	.50 cal.	91.5	90	2	10.9		Base	84.3	78.3
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	87.3	81.3
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	98.1	86.6
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	97.8	86.7
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	87.0	80.8
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	90.5	84.8
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	93.4	87.5
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	100.7	90.1
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	104.1	92.8
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.0	101.7
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	105.4	100.8
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.	<u> </u>		Base	105.0	101.6
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.7	102.1
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	111.1	99.2
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	112.8	101.5
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	94.4	84.0
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	95.1	84.5
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	84.9	79.5
57	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	84.8	79.3
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	62.7	48.4
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	87.2	81.3
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	87.2	81.4
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	98.6	87.9
57	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	98.5	88.3
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	103.7	93.6
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	104.5	94.3
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	93.5	87.8
57	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.3	88.9
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.9	96.8
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.7	96.3
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	108.6	98.9
57	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	108.7	99.0
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	102.0	92.6
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	109.1	99.7
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	110.1	100.7
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	95.5	92.3
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	102.9	100.0

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	Α
57	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.7	100.1
61	5/17	1-3	.50 cal.	30.5	90	0			Base	96.9	94.9
61	5/17	I-3	.50 cal.	30.5	90	0			Base	94.3	91.8
61	5/17	1-3	.50 cal.	30.5	90	0			Base	98.4	95.3
61	5/17	1-3	.50 cal.	30.5	90	0			Base	97.5	94.0
61	5/17	1-3	.50 cal.	30.5	90	0			Base	97.3	93.7
61	5/17	I-3	.50 cal.	30.5	90	0			Base	98.7	95.4
61	5/17	1-3	.50 cal.	30.5	90	0			Base	97.9	94.7
61	5/17	1-3	.50 cal.	30.5	90	0			Base	99.2	96.2
61	5/17	I-3	.50 cal.	30.5	90	0			Base	97.6	93.7
61	5/17	I-3	.50 cal.	30.5	90	0			Base	93.5	90.1
61	5/21	1-7	.50 cal.	15.2	90	0			Base	107.3	103.8
61	5/21	I-7	.50 cal.	15.2	90	0			Base	107.1	103.3
61	5/21	1-7	.50 cal.	15.2	90	0			Base	105.9	102.0
61	5/21	I-7	.50 cal.	15.2	90	0			Base	105.2	101.6
61	6/15	I-9	.50 cal.	30.5	0	0		Data replication. Not used in response analysis	Base	106.5	102.2
61	6/15	1-9	.50 cal.	30.5	0	0		Data replication. Not used in response analysis	Base	103.3	98.7
88	5/26	1-4	.50 cal.	30.5	90	2	14.6		Base	100.0	92.7
88	5/26	I-4	.50 cat.	30.5	90	2	14.6		Base	99.7	92.3
88	5/26	i-4	.50 cal.	30.5	90	2	14.6		Base	100.7	92.8
88	5/26	l-4	.50 cal.	30.5	90	2	14.6		Base	99.8	92.1
88	5/26	1-4	.50 cal.	30.5	90	2	14.6		Base	101.2	94.0
120	5/13	I-1	.50 cal.	30.5	90	2	5.9		Base	104.1	98.5
120	5/13	I-1	.50 cal.	30.5	90	2	5.9		Base	105.1	99.9
120	5/13	I-1	.50 cal.	30.5	90	2	5.9		Base	103.2	98.0
125	5/13	Inactive	.50 cal.	15.2	90	Inactive			Cavity		96.1
125	5/13	Inactive	.50 cal.	15.2	90	Inactive			Cavity		97.6
125	5/13	Inactive	.50 cal.	15.2	90	Inactive			Base	95.1	91.2
125		Inactive	.50 cal.	15.2	90	Inactive	<u> </u>		Base	96.7	92.1
125	5/13	Inactive	.50 cal.		90	Inactive			Cavity		96.4
125			.50 cat.		90	Inactive			Base	97.2	94.5
125			.50 cal.		90	Inactive			Cavity		91.2
125			.50 cal.		90	Inactive			Base	93.8	90.4
125	5/13	Inactive	.50 cal.		90	Inactive			Cavity		102.8
125	5/13	Inactive	.50 cal.	15.2	90	Inactive		<u> </u>	Base	100.4	98.2
125	5/13	Inactive	.50 cal.		90	Inactive			Base	93.1	90.2
125		_1	.50 cal.		90	Inactive			Cavity		90.2
125	5/13	Inactive	.50 cal.	61	90	Inactive			Cavity	96.4	91.3

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	A
125	5/13	Inactive	.50 cal.	61	90	Inactive			Base	90.5	87.7
127	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	102.5	96.7
127	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	104.5	97.8
127	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	88.3	81.7
127	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	90.9	84.7
127	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.	,		Base	88.9	82.6
127	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	90.3	84.8
127	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	102.4	91.8
127	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	103.1	92.6
127	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	114.0	104.5
127	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	113.8	104.6
127	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.3	101.4
127	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.1	101.0
129	5/17	N-0	.50 cal.	30.5	90	2	3.0	——————————————————————————————————————	Base	108.2	103.0
129	5/19	N-2	.50 cal.	61	90	2	2.6		Base	93.9	86.7
129	5/19	N-2	.50 cal.	61	90	2	2.6		Base	95.3	88.3
129	5/19	N-2	.50 cal.	61	90	2	2.6		Base	95.2	87.8
129	5/19	N-2	.50 cal.	61	90	2	2.6		Base	. 98.8	91.7
129	5/24	N-7	.50 cal.	91.5	90	2	1.8		Base	95.0	87.4
133	4/21	I-1	.50 cal.	61	90	0			Base	92.8	85.8
133	4/21	I-1	.50 cal.	61	90	0			Base	93.3	85.9
133	4/21	I-1	.50 cal.	61	90	0			Base	93.7	86.0
133	4/21	1-1	.50 cal.	61	90	0			Base	94.3	86.8
133	4/26	1-5	.50 cal.	122	90	1			Base	84.8	79.2
133	4/26	I-5	.50 cal.	122	90	1			Base	85.1	79.6
133	4/26	I-5	.50 cal.	122	90	1			Base	84.6	79.0
133	4/26	I-5	.50 cal.	122	90	1			Base	84.4	79.2
133	<u> </u>	I-5	.50 cal.	122	90	1			Base	77.5	71.8
133	4/29	I-8	.50 cal.	91.5	90	0			Base	88.0	81.9
133	4/29	1-8	.50 cal.	91.5	90	0			Base	87.0	80.7
133		I-8	.50 cal.	91.5	90	0			Base	86.2	79.8
133	4/29	I-8	.50 cal.	91.5	90	0			Base	87.0	80.6
133	4/29	I-8		91.5	90	0			Base	86.0	78.9
133	6/2	Post-fled.	.50 cal.	15.2	0	Post-fled.			Base	105.3	102.7
133	6/2	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	114.2	103.5
133	6/2	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	113.7	102.5
133	6/2	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	102.4	98.3
133	6/2	Post-fled.	.50 cal.	61	0	Post-fled.			Base	93.8	87.5
133	6/2	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	110.3	100.3

82

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
			Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,	(m)	DOF	·				Flat	Α
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	102.9	94.7
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	89.3	84.7
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	78.5	71.7
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	74.1	70.4
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	77.0	71.9
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	76.7	71.4
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	76.0	71.4
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	76.2	71.5
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	81.6	75.9
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	92.5	82.0
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.	<u> </u>		Cavity	91.2	81.8
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	91.2	82.1
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	90.8	81.7
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	91.1	82.9
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	96.9	87.1
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	101.9	94.4
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	101.1	93.6
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	87.5	82.1
133	6/2	Post-fled.	.50 cal.	122	0	Post-fled.			Base	86.7	80.8
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	92.5	85.9
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	93.4	86.7
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.		·	Cavity	110.9	101.7
133	6/2	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	112.2	103.5
139	5/4	I-6	.50 cal.	61	90	2			Base	93.0	85.9
139	5/4	1-6	.50 cal.	61	90	2			Base	93.0	86.0
139	5/4	I-6	.50 cal.	61	90	2			Base	92.9	85.9
139	5/4	1-6	.50 cal.	61	90	2			Base	93.7	86.7
139	5/4	I-6	.50 cal.	61	90	2			Base	92.9	85.8
139	5/4	I-6	.50 cal.	61	90	2			Base	93.0	86.2
139	5/4	1-6	.50 cal.	61	90	2			Base	92.9	85.9
139	5/4	1-6	.50 cal.	61	90	2			Base	93.6	86.4
139	5/9	N-0	.50 cal.	91.5	90	2	5.2		Base	89.0	82.6
139	5/9	N-0	.50 cal.	91.5	90	2	5.2		Base	89.7	82.8
139	5/9	N-0	.50 cal.	91.5	90	2	5.2		Base	90.4	83.5
139	5/9	N-0	.50 cal.	91.5	90	2	5.2		Base	91.0	84.2
139	6/14	Post-fled.	<u> </u>	15.2	90	Post-fled.			Cavity		104.2
139	6/14	Post-fled.		15.2	90	Post-fled			Base	106.2	103.7
139	6/14	Post-fled.		30.5	90	Post-fled			Base	103.4	100.4
139	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled	· <u> </u>		Cavity	112.5	103.9

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,,	(m)	DOF	'	, ,			Flat	Α
139	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	106.0	96.1
139	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Base	92.7	88.0
139	6/14	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	86.3	81.6
139	6/14	Post-fled.	.50 cal.	91.5	90	Post-fled.	<u> </u>		Cavity	99.7	90.1
139	6/14	Post-fled.	.50 cal.	122	90	Post-fled.		Mid-su-F	Cavity	98.5	87.6
139	6/14	Post-fled.	.50 cal.	122	90	Post-fled.			Base	83.6	78.5
139	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	107.2	104.7
139	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	118.2	111.9
139	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	116.0	110.3
139	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.4	100.4
139	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.0	89.2
139	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Base	109.3	102.8
139	6/14	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	104.2	97.7
139	6/14	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	87.1	83.1
139	6/14	Post-fled.	.50 cal.	122	90	Post-fled.			Base	85.9	78.9
139	6/14	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	104.2	97.0
139	6/17	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.7	100.7
139	6/17	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	112.8	105.0
139	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	108.9	98.6
139	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Base	97.6	92.6
139	6/17	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	89.6	84.7
139	6/17	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	101.2	94.3
139	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	99.5	89.8
139	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Base	84.9	78.8
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.9	102.3
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.8	102.1
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.9	103.3
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	98.9	93.9
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	99.0	93.9
143	5/27	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.2	94.0
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	114.7	104.2
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	110.8	100.1
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	113.7	103.1
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	104.0	101.4
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	99.8	96.8
143	5/27	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	103.0	100.5
148	4/23	1-3	.50 cal.	122	90	1			Base	81.5	76.3
148	4/23	I-3	.50 cal.	122	90	1			Base	88.3	84.0
148	4/23	I-3	.50 cal.	122	90	1			Base	85.1	79.5

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,	(m)	DOF	,	, ,			Flat	Α
148	4/23	1-3	.50 cal.	122	90	1			Base	88.8	83.8
148	4/23	1-3	.50 cal.	122	90	1			Base	84.5	78.9
148	4/27	1-7	.50 cal.	61	90	1			Base	90.6	87.2
148	4/27	I-7	.50 cal.	61	90	1			Base	90.6	87.1
148	4/27	1-7	.50 cal.	61	90	1			Base	90.4	86.7
148	4/27	I-7	.50 cal.	61	90	1			Base	85.7	81.9
148	5/3	N-2	.50 cal.	30.5	90	2	3.2		Base	103.0	94.6
151	5/10	N-1	.50 cal.	15.2	90	2	4.4		Base	105.2	101.6
151	5/10	N-1	.50 cal.	15.2	90	2	4.4		Base	105.9	102.3
151	5/10	N-1	.50 cal.	15.2	90	2	4.4		Base	106.9	103.1
151	5/10	N-1	.50 cal.	15.2	90	2	4.4		Base	106.8	102.9
151	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	106.5	102.1
151	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	115.1	106.3
151	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	111.4	104.6
151	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.4	97.2
151	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	109.0	100.7
151	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Base	85.7	78.5
162	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.2	87.1
162	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	93.9	86.7
162	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	111.9	103.7
162	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	112.7	104.7
162	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.9	106.3
162	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	114.6	106.5
162	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.1	96.0
162	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	109.4	104.6
162	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity		109.8
162	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity		110.5
163	5/17	I-6	.50 cal.	30.5	90	2	1.2		Base	96.1	92.7
163	5/17	I-6	.50 cal.	30.5	90	2	1.2		Base	97.8	93.9
163	5/17	I-6	.50 cal.	30.5	90	2	1.2		Base	97.4	93.5
163	5/17	I-6	.50 cal.	30.5	90	2	1.2		Base	97.5	93.8
163	5/17		.50 cal.	30.5	90	2	1.2		Base	98.4	95.0
163	5/17	I-6	.50 cal.	30.5	90	2	1.2		Base	99.5	95.4
163	6/21	Post-fled.		15.2	0	Post-fled.			Base	109.1	106.1
163	6/21	Post-fled.		15.2	0	Post-fled.			Base	109.4	
163	6/21	Post-fled.		15.2	0	Post-fled			Cavity		
163	6/21	Post-fled.		15.2	0	Post-fled			Cavity		
163	6/21	Post-fled.		30.5	0	Post-fled			Cavity		1
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled	. ]		Cavity	113.4	105.5

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	Α
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	101.0	98.3
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	101.7	98.8
163	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Base	98.7	94.9
163	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	111.8	102.3
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	107.6	97.3
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	105.9	95.3
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	90.8	84.7
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	89.3	83.4
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	106.0	97.8
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Base	88.4	84.6
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Base	88.3	84.9
163	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	109.7	103.2
163	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.		e e e e e e e e e e e e e e e e e e e	Cavity	109.4	102.7
163	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.			Base	103.0	100.3
163	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.			Base	103.6	100.7
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	96.6	90.1
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	96.5	89.7
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	107.2	100.2
163	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	107.2	100.4
163	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity	103.9	97.4
163	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Base	90.7	85.8
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	103.4	96.9
163	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	89.9	85.1
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Base	87.1	81.9
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Base	87.1	81.9
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	99.1	92.6
163	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	99.5	93.1
176	4/28	1-3	.50 cal.	122	90	2	11.7		Base	89.4	82.7
176	4/28	I-3	.50 cal.	122	90	2	11.7		Base	88.2	81.8
176	4/28	I-3	.50 cal.	122	90	2	11.7		Base	87.0	80.2
176	4/28	I-3	.50 cal.	122	90	2	11.7		Base	86.4	79.5
176	5/26	N-7	.50 cal.	15.2	90	2	7.1		Base	88.0	81.5
176	L	N-7	.50 cal.	15.2	90	2	7.1		Base	88.8	82.2
176		N-7	.50 cal.	15.2	90	2	7.1		Base	85.3	78.8
176	<u> </u>	N-8	.50 cal.	61	90	2	5.5		Base	91.1	88.0
176	5/27	N-8	.50 cal.	61	90	2	5.5		Base	92.2	89.3
176	5/27	N-8	.50 cal.	61	90	2	5.5		Base	91.6	87.1
176	5/27	N-8	.50 cal.	61	90	2	5.5		Base	93.1	88.4
194	4/19	I-5	.50 cal.	61	90	0			Base	87.4	82.4

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	.,,,,	(m)	DOF	,	, í			Flat	4
194	4/19	1-5	.50 cal.	61	90	0			Base	96.5	91.0
194	4/19	I-5	.50 cal.	61	90	0			Base	95.5	88.9
194	4/19	I-5		61	90	0			Base	94.7	88.9
194	4/19	I-5		61	90	0			Base	90.7	83.9
194	4/19	I-5		61	90	0			Base	92.9	85.5
194	4/19	1-5	.50 cal.	61	90	0	<del> </del>		Base	98.1	91.4
194	4/19	I-5		61	90	0			Base	94.0	86.5
194	4/28	N-3	.50 cal.	30.5	90	0			Base	99.7	94.3
194	4/28	N-3	.50 cal.	30.5	90	0			Base	100.9	95.1
194	4/28	N-3	.50 cal.	30.5	90	0			Base	101.1	94.8
194	4/28	N-3	.50 cal.	30.5	90	0			Base	101.9	95.6
194	4/28	N-3	.50 cal.	30.5	90	0			Base	93.6	87.0
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.	<u> </u>		Base	105.8	101.5
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.	<del> </del>		Base	105.7	101.1
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	108.0	103.2
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.	<u> </u>		Cavity	116.6	104.5
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	116.5	104.3
194	5/26	Post-fled.	.50 cal.	15.2	90	Post-fied.	-		Cavity	118.6	106.3
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.	-		Cavity	116.7	102.8
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.	<del> </del>		Cavity	116.7	102.6
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	116.9	102.7
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.	<u> </u>		Base	104.1	97.4
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	104.0	97.1
194	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.8	96.4
199	5/11	Inactive	.50 cal.	15.2	90	Inactive	-		Base	106.7	102.7
199	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	111.1	106.2
199	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	114.8	109.8
199	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	111.8	103.9
199	5/11	Inactive	.50 cal.	15.2	90	Inactive	+		Cavity	115.3	107.8
199	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	95.2	89.5
199	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	100.6	95.1
199	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	105.5	97.3
199	5/11	Inactive	.50 cal.	30.5	90	Inactive	1		Cavity	110.8	102.7
199	5/11	Inactive	.50 cal.	61	90	Inactive	+		Base	103.0	95.3
199		Inactive	.50 cal.		90	Inactive			Cavity	116.9	108.0
201	6/17				90	Post-fled			Base	107.1	102.6
201					90	Post-fled			Cavity	/ 106.1	95.7
201					90	Post-fled	I.		Cavity	/ 105.0	93.7
201					90	Post-fled	1.		Base	102.8	97.2

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	A
201	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Base	96.8	90.1
201	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	99.7	89.5
201	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	93.7	85.2
201	6/17	Post-fied.	.50 cal.	91.5	90	Post-fled.			Base	91.6	85.2
201	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Base	90.4	83.6
201	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	92.7	85.7
201	6/17	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.8	102.4
201	6/17	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	113.3	104.8
201	6/17	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	111.2	101.5
201	6/17	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	99.3	94.1
201	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Base	93.4	87.6
201	6/17	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	107.3	97.2
201	6/17	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	105.6	95.1
201	6/17	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	89.7	82.4
201	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Base	86.1	79.2
201	6/17	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	100.2	90.5
205	4/22	I-1	.50 cal.	61	90	2	5.0		Base	85.7	78.9
205	4/26	I-5	.50 cal.	122	90	1			Base	85.3	76.4
205	4/26	I-5	.50 cal.	122	90	1			Base	85.7	77.3
205	4/26	1-5	.50 cal.	122	90	1			Base	84.5	75.5
205	4/26	I-5	.50 cal.	122	90	1			Base	85.3	76.9
205	4/26	I-5	.50 cal.	122	90	1			Base	85.2	76.5
205	4/26	I-5	.50 cal.	122	90	1			Base	82.5	74.2
205	4/29	1-8	.50 cal.	91.5	90	1			Base	85.8	78.1
205	4/29	1-8	.50 cal.	91.5	90	1			Base	85.9	78.6
205	4/29	I-8	.50 cal.	91.5	90	1			Base	86.2	80.6
205	4/29	I-8	.50 cal.	91.5	90	1			Base	85.6	79.4
205	4/29	I-8	.50 cal.	91.5	90	1			Base	85.3	79.8
205	4/29	I-8	.50 cal.	91.5	90	1			Base	85.8	79.0
205	4/29	1-8	.50 cal.	91.5	90	1			Base	86.7	79.3
205	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	106.1	97.3
205	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	84.8	78.6
205	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	84.5	78.3
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	84.9	78.1
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	86.6	79.9
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity		93.6
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity		97.4
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity		103.7
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	112.3	104.1

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,,	(m)	DOF					Fiat	Α
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	95.2	86.9
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	95.6	86.9
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	98.1	91.7
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	101.2	94.6
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.0	105.2
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	113.0	105.3
205	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	115.3	107.6
205	6/2	Post-fied.	.50 cal.	15.2	90	Post-fled.			Base	104.4	101.6
205	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.3	102.2
205	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Base	85.6	79.6
205	6/2	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	106.5	94.7
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	110.3	97.7
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Cavity	108.8	96.6
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	88.1	8.08
205	6/2	Post-fled.	.50 cal.	91.5	90	Post-fled.			Base	87.6	80.5
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.		·	Base	94.9	88.7
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.1	87.1
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	112.2	100.4
205	6/2	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	110.8	99.1
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	118.1	107.3
205	6/2	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	102.7	97.5
205	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	109.8	104.7
205	6/2	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	119.9	109.9
206	5/4	I-2	.50 cal.	61	90	0			Base	103.2	95.8
206	5/9	1-7	.50 cal.	30.5	90	2	3.3		Base	96.9	89.7
206	.l	I-7	1	30.5	90	2	3.3		Base	103.2	95.5
206	5/9	1-7	.50 cal.	30.5	90	2	3.3		Base	104.6	96.8
206	5/9	1-7	.50 cal.	30.5	90	2	3.3		Base	103.4	95.7
206	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.	<u> </u>		Base	107.0	103.5
206	6/14	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity		109.1
206	6/14	Post-fled.		30.5	90	Post-fled.			Cavity		108.0
206	6/14	Post-fled.		30.5	90	Post-fled.			Base	102.5	96.8
206	6/14	Post-fled.		61	90	Post-fled.			Base	93.6	84.9
206	6/14	Post-fled.		61	90	Post-fled.			Cavity		99.7
206	6/14	Post-fled.		122	90	Post-fled.			Cavity		92.4
206		Post-fled.		122	90	Post-fled.			Base	85.2	79.4
206		Post-fled.	<u> </u>	15.2	90	Post-fled			Base	103.6	100.4
206		Post-fled.		15.2	90	Post-fled			Cavity		101.4
206	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled		<u> </u>	Cavity	110.4	103.0

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
	İ	Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF	,				Flat	Α
206	6/14	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.1	99.8
206	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.6	91.1
206	6/14	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	104.8	96.7
206	6/14	Post-fled.	.50 cal.	122	90	Post-fled.			Cavity	100.7	92.9
206	6/14	Post-fled.	.50 cal.	122	90	Post-fled.			Base	88.7	83.6
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	101.9	96.4
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	103.5	98.3
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	102.2	96.6
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	103.7	98.3
208	5/11	Inactive	.50 cal.	15.2	90	Inactive	† <del></del>		Base	102.4	97.0
208	5/11	Inactive	.50 cal.	15.2	90	Inactive	<u> </u>		Cavity	106.8	96.4
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	102.4	92.5
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	106.9	96.9
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	107.1	96.8
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	108.3	97.9
208	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	107.0	96.6
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	95.7	87.6
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	97.2	89.9
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	99.6	91.8
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	97.6	89.8
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	101.7	90.6
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	103.3	92.4
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	105.6	94.4
208	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	103.7	92.9
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	82.7	72.8
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	87.0	78.0
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	89.0	79.6
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	88.7	79.3
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	88.0	78.5
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	88.4	80.2
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	88.9	81.3
208	5/11	Inactive	.50 cal.	61	90	Inactive			Base	89.0	81.5
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	91.8	80.7
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	95.9	85.2
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	98.3	87.0
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	98.1	87.2
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	97.9	87.2
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	97.7	86.8
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	97.3	86.2

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat /	4
208	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	97.5	86.0
211	5/13	Inactive	.50 cal.	15.2	90	Inactive			Cavity	106.6	100.7
211	5/13	Inactive	.50 cal.	15.2	90	Inactive			Base	99.9	96.3
211	5/13	Inactive	.50 cal.	30.5	90	Inactive			Cavity	99.2	94.5
211	5/13	Inactive	.50 cal.	30.5	90	Inactive			Base	93.1	91.8
211	5/13	Inactive	.50 cal.	30.5	90	Inactive			Cavity	94.6	90.1
211	5/13	Inactive	.50 cal.	30.5	90	Inactive			Base	90.9	89.0
218	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	106.5	101.8
218	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	107.7	103.3
218	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	111.4	103.5
218	5/26	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	112.4	104.3
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	111.6	101.7
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	111.6	101.7
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	112.0	102.3
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.3	99.5
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.2	99.2
218	5/26	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	103.7	100.0
227	4/29	I-9	.50 cal.	61	90	0			Base	95.4	86.4
227	4/29	1-9	.50 cal.	61	90	0			Base	95.8	87.9
227	4/29	1-9	.50 cal.	61	90	0			Base	93.1	85.3
227	4/29	I-9	.50 cal.	61	90	0			Base	93.7	87.0
227	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	106.7	102.3
227	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	107.4	102.9
227	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity		108.2
227	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity		107.7
227	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	106.6	100.0
227	6/3	Post-fled.		30.5	90	Post-fled.			Base	106.4	99.6
227	6/3	Post-fled.		30.5	90	Post-fled.			Cavity		109.2
227	6/3	Post-fled.		30.5	90	Post-fled.			Cavity		108.0
227	6/3	Post-fled.		61	90	Post-fled.			Base	91.7	85.4
227	6/3	Post-fled.		61	90	Post-fled.			Base	84.0	76.7
227	6/3	Post-fled.		61	90	Post-fled.			Cavity		100.2
227	6/3	Post-fled.		61	90	Post-fled.			Cavity		91.9
228	4/26		.50 cal.	122	90	1			Base	86.2	78.2
228			.50 cal.	122	90	1	J		Base	93.0	85.2
228			.50 cal.	91.5	90	2	3.7		Base	89.2	86.0
228			.50 cal.		90	2	3.7		Base	84.4	81.3
228			.50 cal.		90	2	3.7		Base	83.9	80.6
228	4/29	1-7	.50 cal.	91.5	90	2	3.7		Base	89.0	85.9

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day		(m)	DOF					Flat	Α
228	4/29	1-7	.50 cal.	91.5	90	2	3.7		Base	84.8	82.0
231	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	113.6	107.4
231	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	114.2	108.0
231	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	115.7	109.4
231	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	107.9	103.8
231	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	108.5	104.8
231	5/11	Inactive	.50 cal.	15.2	90	Inactive		,	Base	109.9	105.9
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	105.1	100.3
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	105.7	100.0
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	101.6	98.2
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	110.0	103.3
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	110.6	104.1
231	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	106.0	99.3
231	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	102.4	95.6
231	5/11	Inactive	.50 cal.	61	90	Inactive	-		Cavity	96.9	90.1
231	5/11	Inactive	.50 cal.	61	90	Inactive			Base	95.2	89.5
231	5/11	Inactive	.50 cal.	61	90	Inactive			Base	89.4	83.4
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	108.0	103.2
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	104.2	99.4
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	109.2	103.6
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Base	106.2	100.1
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	112.6	104.0
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	109.0	100.6
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	114.1	105.7
236	5/11	Inactive	.50 cal.	15.2	90	Inactive			Cavity	110.4	101.9
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	102.2	94.8
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	102.6	95.2
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Base	105.6	98.5
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	110.0	101.1
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	110.0	101.3
236	5/11	Inactive	.50 cal.	30.5	90	Inactive			Cavity	112.8	104.1
236	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	104.5	94.4
236	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	108.5	98.5
236	5/11	Inactive	.50 cal.	61	90	Inactive			Cavity	106.4	96.2
236	5/11	inactive	.50 cal.	61	90	Inactive			Cavity	105.5	95.9
236	5/11	Inactive	.50 cal.	61	90	Inactive			Base	92.7	83.2
236	5/11	Inactive	.50 cal.	61	90	Inactive			Base	95.1	85.6
236	5/11	Inactive	.50 cal.	61	90	Inactive			Base	92.8	82.5
236	5/11	Inactive	.50 cal.	61	90	Inactive			Base	92.6	82.7

Col.	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Rem.	Mic .	SEL (dB)	
		Phase	Туре	Dist.	re.	Resp.	(min)		Pos.		
		& Day	,,	(m)	DOF	·				Flat	Α
271	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	106.5	103.5
271	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Base	105.8	103.2
271	6/3	Post-fled.	.50 cal.	15.2	90	Post-fled.			Cavity	118.6	108.3
271	6/3	Post-fled.	.50 cai.	15.2	90	Post-fled.			Cavity	118.0	107.8
271	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	115.1	103.6
271	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Cavity	115.5	103.9
271	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	99.5	95.3
271	6/3	Post-fled.	.50 cal.	30.5	90	Post-fled.			Base	100.2	97.1
271	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	111.5	99.7
271	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Cavity	112.3	100.3
271	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	94.5	91.1
271	6/3	Post-fled.	.50 cal.	61	90	Post-fled.			Base	95.0	91.3
294	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.	·		Base	104.0	101.6
294	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.		,	Base	105.0	102.3
294	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	111.3	104.8
294	6/21	Post-fled.	.50 cal.	15.2	0	Post-fled.			Cavity	112.0	105.7
294	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Cavity	109.6	103.8
294	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.	1		Cavity	109.9	104.3
294	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	101.1	96.5
294	6/21	Post-fled.	.50 cal.	30.5	0	Post-fled.			Base	101.5	97.5
294	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Base	96.7	90.5
294	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Base	96.2	91.0
294	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity		100.6
294	6/21	Post-fled.	.50 cal.	61	0	Post-fled.			Cavity		100.9
294	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Base	88.4	83.9
294	6/21	Post-fled.	.50 cal.	91.5	0	Post-fled.			Cavity	103.2	95.1
294	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	99.3	92.1
294	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	100.2	94.2
294	6/21	Post-fled.	.50 cal.	122	0	Post-fled.			Cavity	86.4	81.7
294	6/21	Post-fled.	.50 cal.	122	0	Post-fled			Cavity	87.1	82.5

Calc.		Overall SEL	90.1	1.68	8.06	94.9	84.3	83.1	85.1	85.5	8.001	100.5	107.9	108.0	92.5	0.16	103.3	6'101	84.8	85.3	95.0	95.2	101.1	102.3	101.0	0.101	103.2	107.8	103.7	108.1	107.1	/.001	107.9	4.101	80.8	7.401	5.55	103.1	0.68	95.4	102.3	108.6	92.8	99.5	84.7	91./
	3	20000	46	49	6						9/	9/	47	45	59	57	56	32	34	56	59		۶	23	88	9	28	3	æ	9 (	2 6	3	<u>ا</u> وا	3 3	۲   د	<u>,</u>	8 5	75	3 2	¥	<b>€</b>	24	2 2	3 5	47	5
		16000	52	53	22	<del>\$</del>	40	33	38	40	18	81	54	S	- 29	65	44	42	45	45	34	<u>~</u>	2	77	72	72	82	3 3	æ :	- F	£ ;	Z (	79	8 8	3 5	7 5	<del>2</del> 2	7 5	7 .	2 5	2 2	¥ ;	S (	5 5	4 5	⊋
		12500	88	59	<u>=</u>	23					82	82	59	29	71	69	48	47	52	52	35	37	2	6	92	25	<del>2</del>	3 3	8	63	3 (	6	19	2 5	3 5	7 5	£ 2	× 2	<u>۲</u> (	3 8	7 5	2/5	<u>%</u>	9 8	48	€ 
			64	64	65	22	52	53	53	54	83	82	49	63	72	71	99	54	57	57	4	45	<del>ا</del> ھ	82	<u></u>	<b>∞</b>	82	g ;	24	29	2 5	₽ ;	Z (	7 1	g	۶ <del>۱</del>	4 2	2 2	ا ج	2 2	2 5	3 :	-   	3 S	2 8	2
			29	99	2	8	58	99	27	59	83	82	89	89	74	72	63	62	09	09	52	23		83		<b>∞</b>	82	= ;	87	-	9 6	7 ;	2 5	4 6	8 8	5	6 2	2 3	3 3	g ;	<del>ا</del> ة	\$ ;	\$ E	2 3	8 2	*
		2 0 0 0 0 0	89	89	2	8	29	88	9	59	82	81	71	7	74	73	64	64	62	62	57	57	82	8	2	<u></u>	8	3	8 1	2 ;	S :	4	2 /	2 8	2 (	2 5	2 5	3 5	70 5	3	ء ا	\$ ;	9 6	5 8	3 5	٦
		2000	70	69	71	8	62	09	79	63	83	82	73	72	9/	74	89	<i>L</i> 9	63	64	58	9	8	84	<b>2</b>	2	84	2	25	22	69	9/	9 1	0 1	2 3	3 3	s s	3 5	3 8	2 5	2	S (	6	47	<u> </u>	ų,
		4000	72	72	75	65	63	19	63	64	83	82	74	73	75	73	70	69	99	99	59	99	\$	83	8	8	87	1-	82	9/	22	11	72	× [	2 8	2 3	۶ ا	3 5	3 8	2 [	7 5	72	= 1	92	হ্র হ	70
		3150	72	74	72	98	65	62	99	99	82	83	75	_				_	_	69	$\vdash$		-		-	$\rightarrow$	-		-	-	$\dashv$	-+	+	+	2 2	-	-	-	-	2 2	-+	+	+	+	8 2	$\dashv$
		2500	Ш							-	<u> </u>	83	Н	_			├	┡	_	_	ш			-+	-	-	-+	-+	-+	-+	-+		+	$\dashv$	+	+		+	-+	4 5	+	+	7 1	-+-	8 5	$\dashv$
	3	1600 2000	Н	$\vdash$	$\dashv$	-	_	Н	1		_	81	-		-	_	⊢	$\vdash$	┝		Н	-	⊣			-	$\dashv$	$\dashv$	+	$\dashv$	-+	+	-+	+		+	+	$\dashv$	+	+	$\dashv$	+	+	-+	2 67	4
انہ			4 74		74 74				-	89 8	-	1 82	-	_		_	⊢	<b>!</b>	<u> </u>	-	Н	$\dashv$	-				$\dashv$	+	-	-+	-+	-+	84 80	+	5 5	+	+	+	-	+	7 2	+	+	67 67		$\dashv$
r, GA	۲	0   1250	14		-	-		-	_	89 8		81	-			_	$\vdash$	├	┝	-	$\vdash$	$\dashv$	┪	-		-+	-	+	$\dashv$	+	$\dashv$	+	$\dashv$	十	$\dashv$	十	+	+	+	$\dashv$	76	+	$\dashv$	+	99 5	$\dashv$
Fort Stewart,	_ L	800 1000	4 74									81 82					L		L				_		_		_	_	_			_	_	4	72 73	4	4	4	4	4		_	4	_	63	4
t Ste		630	72 7		72 7	_	_	_				8 8/																					82	_	-	-	-	_	8 :	-	-		-	4	19	28
P		200	-	-	2		99 (	⊢	3 66	ш	┝		$\vdash$	5 91	_	-	3 79			5 64	-	-		-		$\rightarrow$	$\rightarrow$	_			-+	-+	_	-	-	-	+	-	-+	-	-	81 28		$\boldsymbol{-}$	28 29	_
.50-caliber blank fire on	-	315 400		02 69			62   59	59 5	61 58		-	89 82	$\vdash$	-	75 7		86 83		ι—	65 65	_	80 73	_	$\rightarrow$	68 86	_	68 86				-+	-	-+	-+		-	-+	82 81	_	-	-	8 2		-	<del>-</del>	57
<b>차 를</b>		0 220	9/	_	-			99					3 92	_	-	_	-		-	59	-	$\overline{}$	_	-	$\rightarrow$	8	-	-	-			-	$\rightarrow$			-	-	-	-	_	-		$\dashv$	-	72 64	0 61
blan	ne le	100 125 160 200 250	81 78		1		77 72	_				93 94	_		85 83	_	-	_	_	76 72	93 88	_	_	94 92	93 90	-		: _	_	_	<del></del> †			92	-+	-	89	-		86	_	-	-	-	-	73
ber	3	1251	82	82	83	77	9/	11	8/	78	68	68	65	56	08	6/	16	68	74	74	83	83	93	94	93	33	۵	102	2	2	≘	2	2		82	86					_		-	-	2 5	13
-cali			79 82	77 81	80 83	74 77	73   76	72 75	74 77	74 77	86 87	98 98	_	82 84	81 80	81 80	83 85	82 84	76 77	77 77	92				-	_			$\overline{}$	_	82	-	$\rightarrow$	$\rightarrow$	_		_	-		83 85	88	_		-	75 77	72 74
		<u>e</u>	9/		77	77	. 22	-	_	74		-	78	62		79	8		74		73	-	84	85	83	83	87	≅	88	82	82	8	82	88	8	<del>2</del>	ङ	6	75	18	79	8	78	æ :	25	72
enta	ave op	<u> </u>	73 75	72 74		81 79	12 69	64 65	69 72			_	78 78	18 79	75 77	74 76	74 76	73 74	17 17	71 72	70 70	71 71	-	$\vdash$	-	81 83			$\rightarrow$	_	-		$\rightarrow$	-	-			-		$\rightarrow$	-+	-	-	-	72 73	68 70
erim	5	25   32   40   50   63   80	-		_	80 8	9 59	9 69	9 19	68	8 62	11 8	78 7	11/	73 7	72 7	72 7	70,	89	-	89				-	$\overline{}$	_	_	_	$\rightarrow$	$\rightarrow$	_		-	$\rightarrow$	_	-	73	29	74	5	77	72	28	2	99
ectra for experimental .50-caliber blank fli	100	20 25	62 67	2 66	65 68	7 81	09 0	1 48	9 64	3 63	3 72	17 69	72 71	73 75	99 02	65 67	99 89	60 64	61 62	58 65	62 62	61 65	92	80 79	77 75	78 73	73 83	$\neg$				_	$\rightarrow$	-		63 72	$\rightarrow$	_	$\rightarrow$	_	-+	-	_	_	59 67	22 65
for	327 (0	16	+-	59 62	-	89 87	51 60	54 51	54 59	58 63	67 73	+	67 7	707	63 7	9 09	62 6	54	┿	-	58 6	57 6	75 7	73 8	72 7	69 7	81 7	$\dashv$	-	_			$\rightarrow$	_				-+		-	_	_	-	-		59
ectra	Dang	10 13	-	57	_	88					89	-	99	99	62	50	1 56		53	-	33	7 51	99 6	5 70	5 71	-	$\overline{}$	-	_	_	_		$\rightarrow$	_		4 61	$\rightarrow$	-+	$\rightarrow$	$\rightarrow$		_	_		_	2 45
g			e 50	e 48		-	e 61	Base	Base	e 67	o 2	ქ ია	Cavity	ty 55	e 59	Base	ty 26	_	56	+	ty 53	ty 47	69 a	e 75	e 76	e 72	e 66	_	-		_	_	-	$\neg$		ξ. 2		ty 43	양	-	$\neg$	$\vdash$	-	-	_	ie 42
ghted		e Pos.	Base	Base	Base	Base	Base	-		Base	H	m	ర	Cavity	Base	m I	Cavity	Cavity	Base	Base	Cavity	Cavity	Base	H	Base	H	Base	Cavity	Base	Cavity	Cavity	Base	Cavity	Base	Base	Cavity	Ö	Cavity		Base	Cavity	Cavity	Base	Base	Base	Base
unwei		Ē	1.7	1.7	1.7	10.8	10.8	10.8	10.8	10.8	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	13.6	13.6	13.6	13.6	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.
tive t	<u>¥</u>	Resp.	2	2	2	2	2	2	2	2	Po	Po	Po	Po	Po	2	12	12	P	P	P8	Po	2	2	2	2	Po	Po	Pc	Pc	Po	Pc	Po	ΡC	Pc	P.	Pc	٦ ح	Pc	L P	P.	P.	F.	Ĭ.	ĕ	P
Representative unweighted spectra for experimental	Event	Dist.	19	19	19	91.5	91.5	91.5	91.5	91.5	30.5	30.5	30.5	30.5	19	19	19	19	122	122	122	122	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	45.7	45.7	45.7	45.7	45.7	45.7	19	19	61	19	122	122
Repre	Event	Type	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
4.	Date		4/21	╁	4/21	4/29	4/29	╁	4/29	H	╁	╁╴	5/27	<del> </del>	5/27	╁	+	t	╁	╁	╁	H	5/24	5/24	5/24	5/24	6/23	<u> </u>	6/23	┝	6/23	-	Н	6/23	Н	Н	Н	6/23	$\vdash$	6/23	Н	Н	Н	6/23	$\vdash \vdash$	6/23
Table D			9	+	Ė	ŀ	ŀ	Ļ	Ė	H	H	9	9	٥	9	9	+	╁	╁	╁	╁	╁	01	2	01	2	-	-	├	⊢	┝	2	$\vdash$	H	01	Н	01	Н	10	H	Н	10	Н	Н	<u>e</u>	0

Calc.	SEL	100.9	840 840	85.0	91.0	91.7	104.1	105.0	112.5	104.6	95.1	98.1	104.5	107.7	9.68	90.9	80.8	91.4	89.4	89.5	90.1	89.4	92.2	8.16	105.8	113.3	101	91.0	101.0	2.5.5	67.01	105.9	100.0	102.9	94.4	78.7	87.9	95.4	93.7	93.3	110.2	108.6
20000	;	£ ;	₹ 4	43			41	48	64	80	57	09	49	56	1		T	T	T		30		8		=	8 5	5 5	23	52	\$ 6	63	84	70	\$	8 :	<b>₹</b>  }	5 5	\$ 8	55	56	48	46
16000	5	45	7 4	43	49	64	51	22	69	84	65	89	99	19	9 9	8 6	\$ 8 8	5 4	4	4	46	44	45	9	<u></u>	2 3	2 2	57	15	\$   \$	88	87	74	9	29	2 5	7 7	8	63	63	53	8
12500 1		£ ;	45	46	50	51	55	09	72	98	89	72	28	65	æ :	\$   £	7 47	69	15	20	53	52	23	23	22 1	5/ 5/	3 4	62	54	€   ĕ	17	88	11	62	29	4 6	46 4	9	89	29	88	25
10000	$\dashv$	4 5	+	╁	62	83	69	.3	75		Н	$\dashv$	62	$\dashv$	+	+	70 5	2 2	9	├	Н	15	53	+	+	+	+	┼-	19	+	╀	00	8/	<u>¥</u>	2 2	ž ;	:   5	122	2	20	63	=
8000 10	-	4	4 5	1	-	_	$\vdash$	-		Н	Н	77	-	$\perp$	\$	+	+	+	┼-	-	Н	$\dashv$	_	29	4	+	4	ļ	89 ;	+	╄	-	$\dashv$	$\dashv$	5 5	+	+	+	+-	71	99	_
98 0069	+	+	┿	╁	) 69	H	Н	H		Н	Н	$\dashv$	$\dashv$	-	+	+	┿	+	╁	┢	Н	$\dashv$	-	+	+	+	┿	╆	73 (	十	┿	Н	$\vdash$	$\dashv$	4 6	+	+	+	72	Н	71	$\dashv$
5000 63	_	8 8	+	╀	-	_	-	_	Н	Н	_	79	_	$\dashv$	69	+	+	+	╀	-	Н	_		$\dashv$	4	-	- -	89	Н	ة اة	+		$\vdash$	+	27 5	+	+	+	+	H	. 69	-
4000 50	-	+	+	2	<del>-</del>	_	Н	H	⊢	Н	-	-	-	. 82	+	+	+	┿	717	⊢	73 7	$\dashv$	-	$\dashv$	+	+	. 08	┿	┝╼┼	3 3	+-	$\vdash$	-		+	- 5	╁	┿	╀	Н	69	-
3150 4		+	3 5	+	$\vdash$	H	Н	<u> </u>	88	-	-		6/	$\dashv$	+	+	╀	┿	┿	╀┈	-	$\dashv$	-	+	+	+	70 8	+-	┝	3 4	╫			+	8/2	0/ 0	+	┿	+	Н		69
	-	3 3	\$   5	99	74	75	84	98	06	92	80	84	83	98	2 2	₹ £	5 2	14	74	75	75	74	11	9	2	2 ×	8 8	72	77	3 3	62	92	85	88	2 :	10	5 8	6/	9/	11	69	67
2000 2500	5	2 3	2 2	89	75	92	87	68	93	92	80	83	98	8	F :	4 5	:   ;	75	74	74	75	75	77	92	æ	3 %	88	73	73	/0	3 8	91	84	88	£ 5	S 5	5 5	78	75	75	73	92
1600	7	4/	8 8	69	77	92	75	75	90	91	62	82	8	83	4 !	į ;	1 4	75	75	75	74	74	77	1	8	<u>4</u> 8	2 98	73	84	× 9	16	92	85	94	98	7 6	5 5	76	74	73	<i>L</i> 9	95
1250		à	à %	92	76	9/	- 26	80	92	91	78	83	88	68	47	7 7	7,	75	76	76	75	75	7	1	82	2/8	83	73	78	7/	8	96	84	92	£ 8	8	20 62	74	72	72	73	17
1000	5	6	8 6	69	75	78	84	85	92	88	79	81	8	98	2	4 2	1 4	75	75	74	74	73	76	77	S	S   2	2 8	74	84	2 F	8	88	83	88	<u>و</u> ا	\$ F	5   5	2	12	71	74	=
008 0		0 5	_	-	7 76			_	_	_	_	-	_	$\rightarrow$	-	_	_	-	_		_		-	-+	-+	_			16 8	_		_	-			8 8	+	+	+	-	2 79	
500 630		9 5	10 19	64 67	+-	_	74 79		-		_	80 82			88 8				69	₩	$\vdash$	68 70	$\rightarrow$	_	-	76 26	_	+	75 78	<del></del>	+	-	-	98	_	2 5	2 02	+-	÷	70 71	82 82	— :
400	_	_	S 5	+-	89	69		Н	-	-	74			-	8	-		8	+	-	$\vdash$	$\dashv$	-	_	-	-	-	-	6/	= 5	8 2	93	$\vdash$	82	7,	2 ;	1 19	92	74	74	83	<u>s</u>
0 315	_	3 6	_	+-	_	<u> </u>	Н	$\vdash$	-	Н	$\vdash$	-	8	-		2 9		8	-	+-	_	_	-+	-	_	7 8	_	-		2 8		<u> </u>	Н	82	-	3 5	2 13	+	+-	$\vdash$	$\vdash$	→
nter Frequencies (Hz) 00   125   160   200   250	_	2 5	20 62		78 73	-	$\vdash$	_	16 66	$\boldsymbol{\vdash}$	84	-	-	$\dashv$	77 74	2/ 1/	2, 27	-	75 69	-	77 70	-	-	-+	_	111 104		-	98	<del>-</del>	9 97	97 97	$\vdash$	-	$\dashv$		7 0 7	90 85	+-	-	92 86	_
uenci 160 2		_	_		82	—			-		_		_	901			_	_1	1	1									5	_		_	ш	-		-	3 5	+			201	
r Frequen			7 7	+	8	-	93	_		_	_			8	_				-			_	_						&			-	98	8	$\rightarrow$	_	78	2 62	_		201	
100	5	<u>s</u> 6	7/ 5/	2,92	82	83	98	87	91	92	84	82	83	8	<b>≅</b> ?	\$ 5	\$ \$	8	<u>~</u>	8	81	81	83	8	8	3 8	₹ 5	82	8	€ 1	68	+-	ш	87	<b>æ</b> [8	78	§ ₹	. 8	+-	-	8	_
Band SEL (dB) at 1/3 Octave Spectrum Cer   13   16   20   25   32   40   50   63   80   1			7 7		8	82	83	84	84	68	82	_	$\rightarrow$	$\rightarrow$	$\overline{}$	_	s   ≅	_	+	79		-	$\overline{}$	$\overline{}$	_	%   %	_		-	:   ¥	_	8	ш	_		<b>≈</b> 8	-	-	-		_	83
ectr 63		_	5 5	-	79	62	80	81	-	-	78	$\overline{}$	-	-	$\overline{}$	-	ō   ā	-	-	78		-	-	$\overline{}$	-+	_	8 8	+		2   5	+-	8			-+		2 12	-	_		∞	
ve Sp	_		3 5	-	5 78	5 78	5 78	7 78	3 80	4 84	1 74	_		-	-	9 9	0 12	+-	+-	5 77	5 77	Н	$\rightarrow$	-	-+	S 8			-	7 6		88 9	-	-	-	-	2 5	-	-	-	7 79	_
2 Octs	_		00 08	-	1 76	2 76	74 76	74 7.	80 83	84 84	16 71	$\rightarrow$	76 75	_		1 0/	7 /	76 77	73 75	73 75	74 75	73 75	78 78		-+	78 82	78 /	+	-	89 69	+	98	78 80	$\rightarrow$	-+	_	7 12	+-		73 75		74 75
it 1/3			6 6	-	70 71	69 72	70 7	74 7	9/	81 8	1				-		73 7	-	69	70 7	68 7	$\vdash$	-	-	-+	75 7	-	+	-+	79 6	-	8	-	$\rightarrow$	$\rightarrow$	-	2 6	-	-	2 29	-	7 7
(S) (S)	_	_	2 5		-	2	65 7	. 99	73 7	82 8	43	$\overline{}$	6	$\rightarrow$	-	_	/0 89	_	_	69	-	$\vdash$	73	_	-	-+-	7 7	-	$\rightarrow$	3 7	$\overline{}$	84		-	-	-	3 3	-	+	65	-	12
3EL (	_		¥ 2	+	+	2	58	69	74	62	73	_	_	-		3 8	_	+	+	+	-	$\vdash$	-	-	-	-	3 2	+	-	2 3		11		-	-	-	ž į	-				19
Band SEL 10 13 16	_	-	4 4	-	-	19			<u> </u>	75	П		7	$\exists$	1	十	1	Ť	84	15	$\overline{}$	$\vdash$	$\rightarrow$	+	-+	-	3 %	+-		2 2	-	27	П	П	$\rightarrow$	<u>z</u>	3	+	+	S.	$\rightarrow$	ဒ
92		_	<b>₽</b>   <b>₽</b>	_	+	8	99	19	9/	71	78	70			1	₹ 5	5 g	;   ‰		28	_		27	23	2	2 2	5 G	65		¥ 5	12	73	65	8	ड	≥ ;	3 %	३	1 ×	8	8	જ
Mic Pos.		Cavity	Base	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Base	Base	Page	Base	Base	Base	Base	Base	Base	Base	Base	Cavity	Race	Base	Cavity	Cavity	Cavity	Base	Base	Cavity	Base	Cavity	Cavity	Bace	Base	Base	Cavity	Cavity
Rec, Time	Ē	1	1	1	+	Ę;	Ι.						- -	<del>-</del>	2.1	$\dagger$	2.1	$\dagger$	T	T		П				†	1				T	T			1	1		, -	  -	ā.		
		Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.			1	<u> ``</u>	1	L		Ц	Ц	$\sqcup$	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled
RCW Resp.		۱ م	2 6	12	1	2	P	۵	a	Pc	Pc	Pe	P	۵	7	7	7 6	1 ~	_	Ŀ	-	_			۵	٤	2   2		F P	ءُ ا	1	l a	Pc	P	۱	<u>بر</u>	¥   å			ă	Pc	
Event Dist.	<b>E</b>	122	72   22	122	19	19	19	19	15.2	15.2	30.5	30.5	30.5	30.5	19	5	10	5 5	91.5	91.5	91.5	91.5	91.5	91.5	15.2	15.2	30.5	19	19	122	15.2	15.2	30.5	30.5	19	19	771	19	19	19	19	19
Event Type		.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	S0 cal.	SO cal.	So cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	So cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	. So Cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
Date		6/14	6/14	6/14	633	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	61/5	61/5	61/2	61/5	5/21	5/21	5/21	5/21	5/21	5/21	6/15	6/15	21/0	6/15	6/15	6/15	51/9	6/15	6/15	9/12	6/15	6/15	51/9	503	5/27	5/27	5/27	5/27
Ċ.		23	2 2	2 2	e e	30	e	30	98	30	30	30	30	30	36	<u>چ</u>   ج	۶   ۶	3 /2	36	36	36	36	36	36	36	98 1	۶   ۶	3/8	36	% ;	2 2	36	36	36	36	36	2 2	2 2	4	4	4	4

Calc.	Overall	SEL	108.5	102.1	101.3	78.7	114.0	1120	106.2	105.8	104.7	116.4	115.7	114.8	85.2	82.4	75.7	6.62	82.5	82.4	93.4	93.7	93.5	93.3	93.5	93.0	93.7	94.4	105.9	105.8	105.4	117.6	117.5	116.8	114.7	114.4	1023	101 7	101	110.5	105.3	107.4	9.66	93.7	100.4
	20000 C	-	5	2	9 8	2 5	) 5	+	3 8	+	╁	65	57	288	42	39	38	38	33	39	8	8	8	8	51	8	8 3	4 2	74	192	92	89	69	2	3 8	3 2	\$ 2	5 8	3 8	3 4	25	88	36	36	78
		1	69	- -	[8]	2 5	3 5	3 5	3 6	:   =	;   8	98	45	99	43	9	39	40	<del>8</del>	<del>\$</del>	22	22	<u>*</u>	54	55	2	2 3	2 5	; P	18	80	72	72	74	19	2 9	8 5	2 5	15	5 2	72	2 5	53	46	62
	12500 16000	1	<u>2</u>	2	2 5	× 3	8 3	3 5	7 6	1 2	2 2	1 2	8	69	84	46	41	45	45	45	59	8	88	65	8	88	65	6 6	=	83	28	74	75	76	F	2	7 5	2 5	;   =	: 8	2	1 5	2	65	82
	10000 12	+	$\dashv$	-+	+	+	+	+	3 6	+	+	+-	╀	╀		$\vdash$		Н			63	-	$\dashv$	-	+	+	$\dashv$	+	╀	88	┝	+		$\dashv$	2   2	2 ;	0 4	0 2	:   ;	2 6	28	2 42	89	65	83
	8000 100	+	62 5	-	+	+	+	+	9 6	+	+	╀	╄-	72 6	-	-	-	H	_		99	$\dashv$	4		$\dashv$		96	+	+	98	╀	$\vdash$	. 08	$\vdash$	+	+	7 6	+	4	+	+	+	99	L	84
	6300 80	-+	+	$\dashv$	$\dashv$	2   X	+	+	- 6	+	+	76	╁	╁╌	┝	59	┢	H	-		Н	-	$\dashv$			$\dashv$	$\dashv$	8 8	+	╁	H	82		$\vdash$	$\dashv$	$\dashv$		+	+	╁	+	+	╁	70	88
	89 0005	4	-1	_		$\dashv$	4	+	2 8	+	-	+	╀	╄-	-	9		L	Н	_	$\dashv$		$\dashv$	_	70	$\dashv$	8		╀	+	ļ	_	_		$\dashv$	$\dashv$	\$ 8	70,2	2 6	2/ 28	   %	92	0,	17	85
	4000 50	$\dashv$	-	-	$\dashv$	8/	+	┿	1 08	+	╁	+	╁	74	├-	7	⊢	-			Н	-	$\dashv$	$\dashv$	$\vdash$	-+	7.1	-	+	8 8	┾	+	28		+	+	+	g 5	5 8	8 8	8	9 2	98	11	98
	150 4	$\dashv$		-	$\dashv$	-	+	+	c  8	+	+	8 8	╀	┼	╁	┾	├	-			73	74	73	74	73	73	23	73	2 5	16	92	88	68	88	8	%	98	) )	3 8	S 2	8	84	78	78	82
	2500 3	1	69	82	8	8 8	2 8	2 2	2 8	3 5	/0	8 8	28	8	89	65	28	63	65	99	74	74	74	74	74	75	74	73	2 2	16	2	8	16	06	90	5	68	89	g 6	3 8	3 8	8	78	78	87
	1600 2000 2500 3150		73	83	-8	5 5	Z 2	78	1000	3 8	6 8	8 8	8	18	9	19	62	65	89	89	75	9/	77	75	75	77	76	77 %	्री व	92	16	93	93	92	5	16	<u>5</u> 8	3 2	\$ 3	+	3 8	+	┿	╀	87
	1600		65	<del>8</del>	81	6/	<u></u>	× 6	6/ 00	8 8	8 2	84	83	82	73	70	63	⊢	⊢	<u> </u>	75			_	Н		76	-	:  s	+	╄	+-	├	$\vdash$	5	5	+		+	\$ 8	+	+	╁	╀	$\vdash$
	1250		71	8	8	8	æ :	<u></u>	ξ 8	3 8	3 2	2 8	8	88	72	99	9	65	20	5	74	74	75	9/	75	74	75	92 7	2 8	8 8	8	+	96	$\vdash$	-	$\dashv$	6	<b>8</b> 3	\$ 3	\$ 8	3   8	+	7	╁╴	8
	1000		69	83	8	ଛ	æ   3	\$ 3	≅  8	8 8	/0	8 8	8	8	72	19	9	49	8	99	72	7.5	72	73	73	72	73	5 1	:   8	8 8	S	2 2	8	100	<u>ē</u>	2	8	<b>≋</b>  3	ဆြ	2 8	3 2	+	75	11	$\square$
	630 800	_	-		-			-	98 8	-	2 2		+	+	4	+-	+-	+	╄	89 29		70 72	71 73	72 73	71 73	71 72	-	<del>`</del>   '	5 8		┿	+-	86 96	+			-	-+	-+	-	6 6	24 23	+-	+	85 85
	500 63		-	83 8	-	$\overline{}$	-+-		-	-+-	89 0	-	+-	_	+	-	56 5	+-	49	┼		_	_	-	-		89	60 1	-		+-	+-	103			96	97	<u>ε</u>	£ 5	-	+	1 2	3 8	73	28
	315 400		1 82	-	$\vdash$	_	=+	90 99	-	-	2 2	27 57	+	102	+	+-	┿	+-	58 58	59 57	80 73	80 73	80 73	79 72	80 73	79 72	80 73	-+	2 S	8 8	20	9 6	94 91	93 89	-		$\dashv$	-+	+	_	-	98 76	+-	+-	87 83
(HZ)			84 81	94 90	Н	-	8 2	-+	-	-	8 2	7 6	+		╁	+	+-		₩	╄		818	818	81 7	╁	$\vdash$	82 8	-+	8 5	97 6	8	3 8	93	92	92	16	6	-+	-+	-	+	8 8	+	+-	+
enter Frequencies (Hz)	100 125 160 200 250		2 90	-	Н	-	2 96	-	_	-	2 2		7 0	93	74 70	+-	+	+	+-	┿~	88 88	88 88	88 88	88 87	┰		-	88		56 56 50 56	4	_	116 109	116 108	113 106	13 106	8	-+	$\dashv$		<del>~  </del> -	26 26		+	
Fregu	125 16		106 105	-		88 98	113	112	=+	-	S 8	-	2 2	112	7.		+-	-	+	+	+-	⊢	83 8	┾	-	_	-	83 8			, 0	-	+	+	-	95 1	-	-	+		-	_			98
Center			-	-	88	_	_	_	& 8 + 6			-	_	_				_	-	-	08 0	-	-	-	-	-	-	-	$\rightarrow$	9 3	-	_	89 92	+	16 28	$\vdash$	-		-+	-	-	90 92	+	8 8	83
ctrum	63 80								82 8			8 8	00 00	8 8				_	_	73 73	_	78 80	77 8	78 80		78 80	79 80	$\overline{}$		68 88 6 88			8 98		82 8	82 8			_		_	2 5	ءَ هَ		_
ve Sne	20		87		_	-	84		-		-	8 8	_				-	-	+	-	+	3 76	3 76	3 76	+	3 76	3 75	_	-	88 88	┰	_	+-		-	80 82					-	-	20 5 C 20	-	_
3 Octs	32 40		75 76	83	80 82		_	_			_	_	00 00		2 6	_	-	_	+	+	+-	68 73	69 73	+	+	69 73	70 73	-		87 88	-	82 84	+	-	79 82	78	-	808	_	-+	-	_	3 5	+-	_
B 21	25		92	75	75	75	7	77	92	2	22	S 5	2 8	8 %	2 5	3 8	84	_	_		+-	+-	89	+-	+	+	89	-	_	8 81	-	_	+	_	1 78	80 75	-	$\rightarrow$	73 75	$\rightarrow$	_		7 /8	_	
Band SFT. (dB) at 1/3 Octave Spectrum C	10   13   16   20   25		63 68	69 78	92 69	1	_			-	_	-	77 04		-	_	-	_	_	+	+	+	69 63	-	-	-	62 61		_	77 86		2 8 87	+		18 81	73 8	77 7	_	58 7		_		7 6	_	_
Rand 9	13		\$3	99	63	29	11	73	_		_	_	_	9 6		_	_	33		-	-	-	-	-	-		_	-		3 75	-	1 6	+	_	+	1 74	2 80	7 62	1	$\overline{}$	_	-	99 5	_	
-		-	$\vdash$	69	<del>                                     </del>		-			_	$^{-\dagger}$	_	12 S	_		_	۰⊢	Base	se   55	+	+-	+-	1	1	+-	1	+	$\vdash$	$\neg$	se 83	+	se %	-	_	+	/ity	/ity 82	se 67	se   61	$\vdash$	_		_	Page	+-
M	Pos.	(min)	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	3 6	Dase		1	Base	Race	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	ž (	Base	, in a	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Base	ဒီ (	ا ا	i m
Dog	Time	=	Ι.	Jed.	Jed.	Jed.	Jed.	led.	led.	led.	led.	Jed.	led.	led.	. L					İ									6:-	fled.	. ieg	iled Fed in	1 2	fled.	fled.	fled.	fled.	fled.	fled.	fled.	tive	tive	tive	Inactive	Inactive
W.O.			Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	rost-ilea	_	-		_	+	- - -	-	-	,   _	,		0	0	2	Post-fled	Post-fled	Post-fled	Dog fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Inactive	Inactive	Inactive	luac	Inac
			+	2	5	5	2	5	5	2	2	2	2	7,	7 ,	7,	1,	1,	1,	1,	╁	+	$\dagger$	+	+	+	+	$\vdash$	.5	.2	7	2 ,	, ,	1 6	5	N	ار ا	2	5	.5	.2	.2	30.5	<del> </del>	15.2
4			+		$\perp$	_	30.5	30.5					+	+	4	77 1	+	+	137	+	$\perp$	-	╀	1	$\downarrow$	$\downarrow$	1	┡	Щ	15.2	4	+	+	15.2	+	$\downarrow$	╀-	┞	1 30.5	-		Н	4	19	_
2	Tyne	3 6	50 cal	\$0 cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	So car	.50 Cat.	.50 cal.	20 ca	.50 cal.	50 cal.	50 65	50 cal	2005	50 cal.	50 03	50 cal.	.50 cal.	.50 cal	.50 cal.	.50 ca	.50 ca	S OC.	.50 cal	50 cal	.50 cal.	.50 cal.	.50 cal.	.50 ca	.50 cal.	.50 cal	.50 cal.	.50 ca	.50 ca	.50 cal.
	Date		5/77	507	5/27	5/27	5/27	5/27	5/27	5/27	5/27	5/27	5/27	5/27	17/5	4/27	17/4	4/2/	17/4	17/1	4/20	00/1	4/20	4/20	4/29	4/20	4/29	4/29	5/3	5/26	2/26	5/26	07/0	97/5	30/5	5/26	5/26	5/26	5/26	5/26	5/13	5/13	5/13	5/13	5/13
ļ			44	14	4	4	4	4	4	44	44	44	4	4	4	2	7 :	7 2	7 2	5   5	7 2	5   2	;   =	5	7 2	5 5	:   =	12	15	12	21	12	7	7 2	:   =	:   -	5 5	12	2	12	52	52	22	2	22

Calc.	Overall SEL	105.8	92.6	99.5	97.9	92.9	103.9	113.0	113.7	99.5	90.4	1.0.1	112.0	103.5	98.7	110.2	108.7	7.16	100.0	100.0	106.7	107.2	107.4	107.2	6.97	101.6	103.1	103.7	105.3	8.98	85.2	82.8	86.4	87.4	91.4	91.3	90.7	91.1	91.3	91.3	91.4	81.9	5:5	
	20000	74	63	69	99	8	<del>∞</del>	23	63	29	57	12	8	82	9/	2 6	49	3 5	=	65	25	9/	9/	2 3	8 2	8	62	64	65	54	22	2 2	. 8	£	57	58	59	28	56	52	58	24		
	16000	75	29	2	19	19	\$	22	19	73	2	88	8	98	<u>چ</u> ا	g	2 5	3 5	=	2 8	<b>≈</b> :	æ	S	2 3	8 %	3 8	89	70	71	8	22	2 19	19	8	49	S	29	63	63	3	8	8	2	
	12500 10	1.1	70	_	89	49 /2	ا وا	∞ ∞	12	76		<u>2</u>	7	23	Σ	3 1	2 !	/ 5	<u> </u>	2 3	2	2		2 9	6 6	5   5	72	73	74	83	73 5	2 4	S   S	63	89	89	2	99	29	25	99	45	1	-
		Н		-	$\dashv$	$\dashv$	+	$\dashv$	$\dashv$	$\dashv$	-	-	-	$\dashv$	$\dashv$	$\dashv$	+	+	+	$\dashv$	$\dashv$	-	$\dashv$	+	+	5 52	╀	┝	$\vdash$		-	+	+	$\vdash$	$\vdash$	92	4	$\dashv$	-	89	$\dashv$	-	<u>-</u>	
	00001 0	Н	$\dashv$	-	+	2 2	4	_	4	4	-		4	8	+	+	4	+	4	$\dashv$	+	+	+	+	+	+	╀	⊢	Н		+	+	+-	╀	$\vdash$	4	$\dashv$	+	-	$\dashv$	-	-	4	
	8000	85	75	79	7	7	\$	8	92	78	7	1.9	8	87	<b>≅</b>	2 1	2	2   3	2	9/	+	+	+	2 87	+	5 4	┼~	$\vdash$	79	$\dashv$	$\dashv$	3 8	+	╁	$\vdash$	$\dashv$	$\dashv$	┪	+	$\dashv$	+	+	-	10
	6300	98	76	8	7	2 3	8	8	7	2	72	\$	8	82	S	8 9	77	-	2	77	87	8	<b></b>	80 2	5 / 5	76	78	8	81	8	65	ઉ દ	89	89	74	74	7,	7	2	7	73	55	26	0.2
	5000	98	11	62	7	2	3	28	≅	79	72	25	8	88	æ	<u>د</u> ا	χ (	7 2	2	7	<u></u>	8	8 8	3 5	\$   \$	78	8	8	81	9	29	3 2	67	89	73	72	73	2	2	72	74	2	58	07
	4000	98	78	≅	78	74	g	8	8	8	72	7	8	8	<b>∞</b>	8	S	2 3	\$	%	ଛ :	8	8 3	2 %	<u>ې اې</u>	2 62	-	82	84	70	20 5	9	3 8	72	75	75	73	9	74	72	75	62	59	;
	3150	87	62	- - -	79	92	g	82	83	8	73	8	82	68	<b>≅</b>	8	-	2 2	ရှ	<u>چ</u>	22	2	5 5	45 5	2   8	8 8	8	83	8	72	<b>S</b>	ž (3	3 2	72	77	9/	73	2	26	76	77	ĝ.	9	,
	2500	87	62	81	78	76	5	8	88	83	73	98	84	68	84	£	6/	2,	à	8	35	93	92	91	3 2	84	98	87	87	71	2 2	5 5	2 2	72	92	11	75	75	77	76	77	\$	90	•
	2000	68	80	8	8	77	6	8	87	8	75	81	88	8	8	82	77	73	ŝ	22	93	92	6	2 2	50 00	84	98	87	88	72	02	5/ 6/	72	75	77	78	92	76	81	29	78	8	19	,
	1600	88	79	8	65	82	35	5	88	88	77	83	98	8	84	£	8	22	2	8	5	16	16	2 2	84	8 8	84	98	87	70	19	69	8 8	72	75	75	75	75	92	75	9/	\$	09	.,
	1250 1	88	62	-	$\dashv$	6	5	62	2	<u>%</u>	26	88	68	8	88	8	٤	2 3	<u>-</u>	82	8	16	8 8	S   S	2 8	8 8	87	88	06	89	19	8 8	8 8	72	75	75	73	74	74	74	75	49	09	111
į	1000	93	6/	85	<del>2</del>	œ	88	8	2	87	92	98	16	8	84	2	9	7 8	<u></u>	28	<u></u>	8	£ 1	68 3	\$ 8	2   %	88	68	16	89	8	29	3 5	2	74	73	72	7,	73	75	75	છ	8	ļ
	800	L.	Ш	_	_	78	_	_	86	_			_	68	<u>ω</u>	8	_	+	4	-	_	-	87	98 6	2 2	2 48	98	98	88	69	89	8 9	89	72	74	72	72	2	72	73	74	65	59	!
	630	94	. 8/	$\neg$	-+		-+	-	-	81			-		-+	-	-+	-	-	$\rightarrow$	_	-+			_	ē ≅	1	+	82	-	\$	9 7	-	69	72	11	70	7	11	72	12	3	21	
	500	8		84	83	75	86	90	-	79	71	80	94	98	82	87	83	6	æ	1	8	8	8	<b>æ</b>  ₹	<u>ا</u>	2 2	+	8	82	99	-	જ   ય	┰	+	•	-	┝╼┥	-	70	٦	-	62	_	1
	400	96		-	8	-			_	$\dashv$	-	$\vdash$		8	_+	-	-	-	2	-	-	-	6	6 6		2 0	28	+	79	99 (	-	8 3	-	+	-	69 1	Н	-	2	⊢	$\vdash$	$\rightarrow$	_	*
(Z	0 31	+	76 78	$\dashv$		4 74	-	$\dashv$	-	7 83	74 67	-	_	-	_	- 1	_+	$\dashv$	_		_+	89 95	8	_	8/8	+	+-	+	95 87	26 70	-	76 70		+-	80 74	80 7	-	79 74	80 7		7	1 66	.1	
es (H	00 25	+	_	16 96	94 91	75 7		12 97		88 87	76 7	110 96	10 94		-	<del>~</del> †	07	+	$\rightarrow$	-	$\dashv$		-		2 C	+	+	+-	5 96	74 7	72 7	13		13	78	8 8	78	$\dashv$	Н	82	<del></del>	2		1
nter Frequencies (Hz)	125 160 200 250 315 400	_	-	$\vdash$	-	79 7		95 1		92 8		93 1	104	$\rightarrow$		=	긁	-	-	-	-			$\dashv$	-	7 6	+-	+-	-	75	74	4 2	+	75	╄	. 62	78	. 62	6	. 6/	79	71	9	t
Freq	1251	+	81	76	$\dashv$	82	$\rightarrow$	-		-	-	$\vdash$	$\overline{}$	_		-	=+	-+	-		-	-	_	-	$\boldsymbol{+}$	2 8	┿	8	97	-	9/	1 1	× ×	78	82	82	82	82	82	82	83	73	2	l
nter	8	82	75	7.5	92	84	82	82	83	88	80	16	98	32	<u>&amp;</u>	8	8	<b>&amp;</b>	8	8	2	93	97	22	3 3	3 2	95	95	97	78	77	12	, ×	78	83	82	82	82	82	83	-			ŀ
Ŭ E	63 80	8	16	75		$\vdash$	-	—	80	87	80	16		-		-	-	-+	-	-		-	-	_	-	3 8	+-	93	94	77	-	-	77	11	8	8	-	81	-	-		_		
ectr	63	∞	77	75	-	-		82		98	78	77	-		-	-	-					-	-+	-+		2 2 2	+	-	92	75	$\vdash$	2 2	+	-	79	7	79	1 79	-	-	-	-	89	
ve Sp	05	83	-	3 75	Н	-	-	$\vdash$	-	84	2   77	9/   7	-	_	-			$\rightarrow$	_	$\rightarrow$	_	-			8 8		+-	+	9	0 72	$\vdash$	-	2) 02	+-	75 77	75 77	73 77	75 7.	75 78	75 77	_	69 99	57 65	٠
Ö	32 40	77 79	78 76	78 73	72 74	$\vdash$	85 85	1 80	74 72	80 82	74 75	72 72	74 75			+	-	-		-	_	-	$\rightarrow$	$\rightarrow$	_	20 82	-	+-	83 86	68 70	<del>                                     </del>	+	7 6	+-	72 7	72 7	717	72   7	72 7	72 7	71 7	-	55	l
at 1/3	25 3	81 7	74 7	74 7	72 7	┝╼┥	82	11 11	72 7	75 8	99	69	192	-	$\rightarrow$	-+		-	-	$\rightarrow$	_	-	-		-	× ×	-	_	82	2		-+	\$ 5	+	+-	5	-	0/	69	70	89	63	46	
( <b>9</b> P)	2	28	┿	. 92	$\vdash$	-		75	74	$\vdash$	74	75	81		_	$\rightarrow$			~			$\vdash$	-	-+		2 5	_	-	11	ક	₩	-	<u> </u>	+-	-	62	57	62	2	63	88	28	42	İ
SEL	16	77	70	78	71	-	75	73	72	89	19	29	73	74	4	8	23	26	-		16	92	-	-	-	2 5	-+-	7	75	57	38	% :	۾ چ	3	â	65	_	2		65	55	51	42	٠
Band SEL (dB) at 1/3 Octave Spectrum Ce	13	8	29	80	72	72	76	16	74	9	99	89		78			$\rightarrow$	23		59	-	67	$\rightarrow$	$\rightarrow$		79	-	-	+	54	53	-+	χ 8	-	-	54	48	15	8	53	47	Ц		ļ
	9	90	72	98	26	12	73	74	78	69	59	72	-	81	99	72	26	<u></u>	71	09	26	11	77	ଛ :	2	2 2	1/2	8 8	19	46	Н		<del>}</del>  €	+	┰	49	┼──	52	48	54	4	ا پ	ě	
Mic	Pos.	Cavity	Base	Cavity	Cavity	Base	Base	Cavity	Cavity	Base	Base	Cavity	Cavity	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Race	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	
۲	ne (min)					П			<u> </u>		T.			П						П	0	0.0	0	0.0	1	1	T	十	T	∞i ∞i	2.8	2.8	×,	2 0 0	2.8	2.8	2.8	2.8	2.8	2.8	2.8			١
ž	Time	Inactive	Inactive	Inactive	Inactive	Inactive	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled.	Post-fled.	Post-fled.	Post-fled.			.0	Ö	Ö	0						2	7	2	7	1	7	2	2	2	7	7	7			1
RCW	Resp.	Ĩ	Ĕ	Ë	ij	Ä	Pos	Pos	Pg	Po	P.	Pos	ď	Po	Po	Po	Po	Po	0	0	0	0	0	0	0	٥		0	0	2	2	2	7 0	۱/ ۲	7	2	2	2	2	2	2	0	0	
Event R		15.2	30.5	30.5	19	61	15.2	15.2	30.5	30.5	19	19	15.2	15.2	30.5	0.5	19	19	30.5	0.5	15.2	15.2	15.2	5.2	30.5	30.5	20.5	5.5	30.5	19	19	19	-   -	5 5	1 5	19	130	19	150	19	19	122	122	
H		+	╀	L	L	Ш		L	L	L			L	L			Щ			_	ļ.,	L		Н	$\dashv$	4	+	+	╀	╀		Ц	+	_	$\perp$	Ļ	Ļ	L	<u> </u>	L	<u> </u>	$\vdash$	L	-
Event	Type	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal	.50 cal.	.50 cal	.50 cal.	.50 cal	.50 cal.	.50 cal.	.50 cal	.50 cal.	.50 cal.	.50 ca	.50 cal.	.50 cal.	.30 Cal.	50 cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 ca	.50 cal.	.50 cal.	.50 cal.	.50 cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	
Date		5/13	5/13	5/13	5/13	5/13	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/5	5/5	9/10	8/10	9/10	5/10	5/12	5/12	71/6	2/12	5/12	4/21	4/21	4/21	4/21	17/4	4/21	4/21	4/21	4/21	4/21	4/21	4/21	4/26	4/26	
Col.		+	╀	╀	╁	52	53	53	83	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	23	2   2	3 5	2 2	57	57	57	23	<u>ر</u> د	57	12	57	57	57	57	53	57	22	

Calc.	Overall SEL	81.8	82.4	81.9	85.9	84.3	5.70	96.1	0.7.0	0.78	50.0	93.4	100.7	104.1	0.4.0	105.4	0.501	105.7	-  -  -	112.8	4.4	1.5%	84.9	84.8	62.7	2.78	87.2	98.6	98.5	103.7	104.5	93.5	94.3	100.9	108.6	108.7	102.0	109.1	110.1	95.5	102.9	103.7	6.96	94.3	98.4	97.5	
	70000 70000 70000	24	24	27	£ 1	42	2 ×	\$   <del>\$</del>	9 1	÷   5	2	<del>ا</del> ۾	3 5	7 5	2 2	+	+	<b>-</b>	ة ق	50	7 5	47	£ ;	643	41	4/	41	45	45	20	22	65	S	4 2	4 8	1 2	57	19	19	74	88	28	19	58	62	63	
	16000	38	36	40	4 :	44 4	3 2	# \	£   ;	<u>,  </u>	8 ;	<u></u>	s s	¥ ;	8 8	2 2	3 2	2 (	7.9	40 6	\$   ;	04	4 3	<del>2</del>	ê ;	8	S	4	44	22	22	99 !	19	2 6	2 5	;   %	2 2	3 3	3	82	8	68	19	2	29	89	
	12500 1	45	46	47	S	8 6	2 4	\$ 6	9 3	နှ ႏ	3 3	اة	¥   ;	3 3	8 8	2   2	2   2	<u>4</u>	3	5 8	£ ;	40	£   5	\$	88	%	55	44	£	%	22	S :	=	2 2	<u> </u>	3 6	2 5	: 63	42	62	8	68	2	89	17	17	
	100001	52	52	53	22	42 2	2 2	2 2	2   5	ī (	g	≥	19	2 5	2	<del>ا</del> ه	2 2	g	3	8 .	4.5	54	χ ;	55	37	3	9	48	47	59	88	72	4 2	2 S	2 3	3 2	3 8	3 3	19	- <del>-</del>	8	5	52	17	74	73	
	8000	56	99	99	59	8 8	3 8	2 8	<u> </u>	2 (s	3 6	7	40	6	2	æ s	2 2	22	3	21	84 9	48	9 (	8	9	3	3	53	52	63	63	4	9/	8 8	2 3	3 5	19	; 8	70	92	2	96	75	73	9/	75	
	9300	58	59	59	79	3 5	3 8	6 3	Į,	9 8	2 1	2	29	2	=	3 8	3 3	35	2	92	22	26	3	62	33	65	65	57	58	69	89	75	77	98	S 5	2	55	2 2	73	2	8	68	78	92	79	78	
	2000	9	62	19	29	99	8 5	/9	g	8	7/	4	80	2 3	٥١	3 8	3	35	72	-	8	59	65	2	34	29	29	59	59	89	89	26	77	88	\$ 65	3 5	: 5	3 5	73	ê	6	88	79	76	78	78	
	4000	+-	-	62	$\dashv$	-	+	6	-+	+	-	-		-		-	-	-+	-+	-	-+		$\dashv$	<del>-</del>	-+			99	Н			75	-+	8 3		2 2	+	╁	+	╁	╁	╀	╀	╁	╀	8	
	0 3150	╀	-	63	-	8 6	-	+	2	$\dashv$	4	-	72	-+	+	-		-	-	-	+	-	-+	┥			$\vdash$	_	-	$\vdash$	$\vdash$	38		+	82	╫	╬	+	+-	+	+-	8 8	┿	╀	╀	2 83	
	00 2500	⊢	-	Н	$\dashv$	88	+	8 9	+	$\dashv$	$\dashv$	-	80 72	-	4	-+	-	-		-		-	-+	-			$\dashv$	_	-	6 26	Н	-1	-	5 85	25 S		+	+	-	+	╀	87 88	+	+-	88 84	┝	
	1600 2000		<u> </u>			69 :			_	_	_	_	_	_	_1	_	_	_		-					-				$\vdash$	<u> </u>		-			+	+		+	+-	┿	+	+-	2 6	+-	╁	+-	1
	1250 16	+-	⊢	Н	-	2 8	+	-	+	$\dashv$	$\dashv$	-	-+	_		-	-			-	-		-	-			Н			-	. 19			-	-+	-+-	-	+	+	+	+	╁	+	╁	88	25	
	1000	+	65	Н	$\dashv$	2	+	+	$\dashv$	$\dashv$	-	-	-+	75	£	· 8	26	82	<u>%</u>	98	28	29	89	69	37	69	69	09	29	89	89	75	75	<u></u>	<u>ت</u> ا	<u>.</u>	<u>ا</u> ۽	0 8	6 8	3 5	:   2	2 2	5 8	   	83	82	
	800	63	63	62	99	63	89	19	છ	89	7	73	7	23	<u>ω</u>	98	8	87	88	8			69	-							85			_	_		_	_		_			-	-	- <del>-</del> -	+	-1
'	630	19 19	ļ	-	$\vdash$	60 61	-	$\rightarrow$	-+			-	71 71	-+	-			91 88			_	0.		_	$\mathbf{I}$	_			-	-	75 80	_	_	_	80 2	-	_	_		_	2 00	_	_		76 79	┿	4
	400 500		┺-		-	63 6	_	-	-	-	$\dashv$		73	-		_	87		6 96						_	_	_	_		_	81 7	_		_	_		2 6	-	S 3	-	┿	+	+	-	+-	75	
٥	100 125 160 200 250 315 400	99	┿	19	Н	$\rightarrow$		75	_	$\rightarrow$	_		3 75		-	$\rightarrow$	1 93	_	_	-			4 65	-	⊢	_	-	85 79	╌	+	1 84	_	-	94 88	2 88	-	-+-	-	ر د او	-	+	+	+	2 5	+-	86 78	-1
Center Frequencies (Hz)	200 25	71 71	71 72	┰	78 71	-	74 7	84 79		-	<b>→</b>	_	83	-	-			-	_		91 83		$\vdash$	75 74	43 42	79 75		⊢	+-	6 101	١	8 98	-	-	_	_	_	-		_	00 00	-	+	+	+	+-	
ednen	991 2	F	72			, ,		8													68 7				5 43				_		91 98	_	_	_	_		=+		201 6	-	_	2 84	-	+	8 2	+-	4
nter Fr	00 12	74 73	74 73			73 73	_		-		_	_		$\rightarrow$	-	_		_		-	79 82						78	82	82	88	98	83	84	8	88	æ !	<u>ک</u> ا	⊋ 5	<u>چ</u> ا	ž Š	2 8	8 8	9 8	3 &	3 %	85	
		73	72	72	75	73	26	8	8	9/		80	81	84	8	68	85	98	88	85	9/	92	74	74	7 47	177 8	-			-	8		_		-	_	_	_									
Spectr	50 63	68 70	-	_	73 74			_	_	73 74	76 77	62 62	_		98 98	_	-	_		82 83	72 75	72 74	73 74	73 74	48 47	73 75	+-	73 76	+	+-	-	79 81	79 81	-		$\rightarrow$	_	-	$\boldsymbol{\neg}$	_		24 83		-		_	-
ctave.	9	99	99	19	8	8	23	72	71	11	74	1.1	72	1.1	85	82	98	87	87	82	69	69	70	70	49	71	72	71	72	75	76	9/	77	80	81	_	$\rightarrow$	-	-	-	-	78 6		, ,	_	_	
Band SEL (dB) at 1/3 Octave Spectrum (	20 25 32 40 50 63 80	09	_	4	63	-		_	29 29	29 29	68 71	72 74	69 29	71 73	82 83	-	85 84	85 85	88 88	77 78	65 67	65 67	99	65 67	51 50	68 70	-	69 29	+-	+-	-	72 74	72 75	78 79		-	-+	$\rightarrow$	-+	-		₹ 6 8	2 F	5 5	-		
(B)	20	š	35	57	57 (	-		_	62	63	09	19	28	29	80	78	81	84	82	82	57	57	28	28	53	59	19	28	8	29	2	62	8	69	89	8	8	-	73	4	7	<u>ب</u> ا		8 7		2 2	
nd SEI	3 16	45 56	_	45 52	48 57	-	52 63	$\vdash$	48 58	47 59	52 61	99 89	48 56	55 66	62 69	82 89	74 82	72 81	79 84	73 80	53 60	52 61	49 61	48 60	54 54	46 63	-	+		_	_	52 67	55 67	57 73	-	_			_	_	_	2   S	8 (S	5 5	0 19	30 85	3
m	10 13 16	1	84		34	-		-	25 4	25 4	54	59	46	28	73 (	70	. 92	8	. 62	81	52	48	46	46	26	8	-	+	2   2	8	-	22	57	62	-	જ	છ	SS	2	8	-	67	3	3	Т	, 9	3
Mic	Pos.	Race	Base	Base	Base	Base	Base	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Base	Base	Cavity	Cavity	Cavit	Cavity	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Pase	Base	Dogo	T Cast
;	Time		$\dagger$	$\dagger$	$\dagger$	6.			<u> </u>				Ι.	Ι.				_	<u> </u>	<u> </u>		١.	١.	<u> </u>	L	L		1	1		T															T	
Rec.		1		<u> </u>	10.9	10.9	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Poet-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	4	4	1	4
RCW	Resp.		}	, 0	2	2	ĕ	P	ď	Ĕ	P.	ď	ď	Ĕ	ď	_	_	a di	Å		-	l a				٩		1		1		1	12		_	Ь	Δ.	Ч	٦					-   ·	<b>-</b>		>
Event	Dist.	(E)	127	122	91.5	91.5	122	122	91.5	91.5	19	19	19	19	30.5	30.5	15.2	15.2	15.2	15.2	122	122	122	122	91.5	5 16	91.5	\$ 10	210		5 5	19	13	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	15.2	15.2	30.5	30.5	50.5	C.VC
Fvent	Type	15.00	SO call.	.30 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	So cal	50 cal	50 03	So cal.	Co car.	.50 cal.	.30 cat.	50 cal	50 cal	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 car.
Date			4/76	4/20	4/30	4/30	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/3	6/2	679	2/9	\$	7/0	7 5	7/0	7/0	0/9	2 63	2/9	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	5/17	5/17	2/17	5/17
-5		-	7 5	+	┿	57	57	57	57	57	57	57	57	57	57	57	57	52	23	25	22	15	22	5	5 5	5	5 5	5	2 2	2 2	2 5	25	5 5	22	57	27	22	57	57	57	57	27	22	19	19	5	T 19

Calc.	Overall SEL	97.3	98.7	97.9	99.2	97.6	93.5	107.3	107.1	105.9	105.2	106.5	103.3	100.0	99.7	100.7	8.66	101.2	104.1	105.1	103.2	102.6	104.0	95.1	2.96	101.3	97.2	6'96	93.8	108.9	100.4	93.1	92.8	96.4	501	104.5		S. 8.	6.09	88.9	90.3	102.4	103.1	114.0	113.8	103.3	103.1
	20000 C	Н	79	+	$\dashv$	$\dashv$	-	-			-	$\vdash$	┢╌	-	99	99	65	┢	-	$\vdash$	-	65	-	H		69	70	20	53	92	78	88	8	\$ 3	3 5	84	î	1		84	52	46	47	29	29	75	9/
	16000	99	88	29	8	99	62	88	88	98	98	83	79	17	72	71	70	73	77	28	9/	29	69	69	70	70	72	65	28	1/	<del>-</del> 8	۶ ا	2	3 2	5 5	2 2	5 5	7 ;	£ 2	¥	98	21	53	69	72	08	80
	0	70	77	11	72	69	99	68	68	88	88	88	82	74	74	74	74	9/	80	≅	62	89	71	72	73	11	75	99	63	52	83	22	77	96	3 5	3 8	3	- -	4 /	ŝ	29	53	57	74	74	83	83
	10000	73	75	74	76	72	69	90	90	88	88	98	83	92	9/	9/	75	78	84	8	83	83	84	75	76	81	78	9/	72	68	8	4	4/	//	90	3 2	5 8	75	۶	١٥	49	59	62	9/	79	84	84
	æ	75	76	76	78	74	70	91	90	68	68	87	83	78	11	11	9/	78	84	88	28	82	83	77	78	80	79	75	73	88	82	2/2	9/	ر د اد	5 2	5 8	3 3	ž (	3 3	S	8	3	64	78	79	98	85
	9		_	_	4	4					L	┡	<u> </u>		<u> </u>	L	_	ļ	_	_	<u> </u>	$\vdash$					_	$\dashv$	4	_	4	-	4	4	+	╀	+	4	-	4		4	_	-	8	$\vdash \vdash$	98
	00 2000	$\dashv$	8	-	-		-		-		⊢	├	┝	_	_	_	⊢	ŀ	-	-	-	Н			-	$\vdash$	$\dashv$	-		$\dashv$	$\dashv$	-+	+	+	+	+	+	+	+	-	-	{	_	Н	$\vdash$	-	88
	-		85 82		+	-	$\vdash$	$\dashv$	_	Щ,		├	-	_		<u> </u>	⊢	⊢	┞	╌	⊢	Н	$\dashv$	$\vdash$	$\vdash$	-	-				-+	-+	+	+	+	+-	+	+	+	+	-	-	-	86 85	Н	H	87 88
		$\dashv$		-+	-+		$\dashv$	$\dashv$		-	├	-		_	_	├	┝		⊢	├-	-	Н		Н		-	-		+		-	+	+	+	+	+	+	+	+	+	-		-	Н	Н	06	$\dashv$
	)	85	87	82	87	84	8	92	95	16	16	93	68	62	62	62	42	82	87	68	87	84	98	79	81	84	84	78	8.	8	88	6	5 5	6 1	: 8	8 2	à	7/	٦ ;	=	76	77	78	88	88	16	16
	1600	86	88	98	88	85	08	92	92	06	91	92	88	80	08	80	79	81	87	68	87	82	83	79	81	83	84	77	<del>.</del>	87	88	62	62 5	3 5	5	7,	3 5	2 2	e E	7/	74	73	74	90	8	93	93
		83	8	98	84	8	8	93	92	06	8	8	98	80	08	08	8	8	87	88	87	-		-		$\dashv$	$\dashv$	┥	┪	-	$\dashv$	$\dashv$	+	+	+	+	3 6	2	2 8	7/	7.	92	77	06	8	92	90
	-		8	_	_	_		_			<u> </u>	68	<u> </u>			ļ	ļ	Ļ		╙	7 87	Ц	_	08		$\Box$	_	_	_	_	_	_	4	4	4	4	8 7	4	2 6	4	_	-		7 93	Ш	Ш	88 06
	630	08   22	78		_	—∔	$\vdash$	-		_				_					-	-	-	86 87	_	_			-		-	_	-	75 7				_	-	-	74 74	-+		76 83	9/	06	8	87	87
	00 200	ш	76 76	_	78 77		71 70	-			_	├-	-	-	_	⊢	<u> </u>	<del></del>	-		31 85	89 85		87 78		-	-	-	75 76	$\overline{}$	$\rightarrow$	92 97	-	-		-	2 9	-	27 59	-	_	84	_	-		88 06	_
	315 400	79	8	62		77	9/	94	93	93	91	8	87	68	68	06	68	16	68	16	68	98	87	81	83	88	28	≅	2/9	2	88	73	74	6/2	2 5	1 5	;	\$ (	وا	4	7	77	78	88	88	35	16
er Frequencies (Hz)	0 125 160 200 250	_		88 87	_	_	85 82	_	_	_	-	96 86	95 93	-	68   66	-	-			-		85 87	_	-		_			76 74		-	83 79	-	-	_	2/ 20	-		2 2	75	-	96 76		94 87		-	91 92
requen	160	68 98	87 91	88	-	-	2 85		_	90   92	_											66 9																							113	90 92	92
enter F	100 17	82	98	82	98	82	81	93	63	76	96	94	16	68	68	96	68	96	96	16	95	98	68	82	82	85	84	81	88	8	88	8	2	92	0/	3 8	ه ه	2	<b>2</b> 8	82	83	79	18	87	68	68	68
trum C	93 80 100	-	-	-	-	-	$\overline{}$	90 92	$\overline{}$	$\overline{}$	88 90	92 94	89 91	-	68 48	06 88	87 89	16 68	90 92	90		-	_	79 83	_	_	79 85	-				-	-	_	4 6		8 8	-	-+	_	_		72 76		_		83 85
ve Spec	50	18	82	<u>8</u>	82	82	77	88	68	68	87	8	87	85	85	98	85	87	8	68	87	79	83	75	78	77	79	74	78	82	%	8	2	72	5 6	o ç	2	7.		2	71	69	89	92	78	81	18
/3 Octa	32 40	62 92		_	_	$\overline{}$	$\rightarrow$		-		86 87	85 87	82 84	83	18 62	81 84	80 82	82 85	85 87	86 87	83 85	-	$\overline{}$	75 75	81 11	81 81	26 80	_	_	-	$\rightarrow$	$\rightarrow$	-	-	27 22	0/ 5/	-	-	_	_	71 72	89 69	69 89	92 62	81	81	
dB) at 1	25	-	_	$\rightarrow$		73 75	-	_	_	_	86 81	74 83	73 80	74 78	<i>71</i> 89	08 92	72 77	76 76	80 81	76 84	78 80	77 75	I	75 71	-	81 75	78 76	78 76	-	_	_			-	7/ 5/	70 00	-	_	_	_	99 99	99 69	25 69	78 74	77 76	78 79	_
Band SEL (dB) at 1/3 Octave Spectrum Cente	10 13 16 20 25 32	-	89	71	7	20	69	80	92	28	76	78	75	70	89	70	72	7	79	8	77	29	75	29	89	62	72	72	09	78	7,	2	8	7	ò	_	_	_		-		89	99	78		. 92	
Ban	10 13	49	_		હ		П			80 74	83 77	99 79	64	63 56	25	73 64	59 63	59 59	59 72	68 73	73 74	15 71	80 71	75 62	-	08 06	15 67	81   76	_	_	_	$\rightarrow$	$\overline{}$	82 76	6	-	3	+	<u>\$</u> ;	89		99	64 58	72	20	72	19
Mic	Pos.	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	${}^{-}$	Cavity		Base	Base	Cavity	Base	Cavity	$\overline{}$	$\neg$	Base	Base	Cavity	Cavity	pase	Cavity	Cavity	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Base	Base
Rec,	Time (min)	_												14.6	14.6	14.6	14.6	14.6	5.9	5.9	5.9			, c		Г					ve			1	2 7	1	1	-g	-g	eq.			<u> </u>	<u> </u>	<u> </u>	<del>                                     </del>	eg.
RCW	Resp. 1	0	0	0	0	0	0	0	0	0	0	0	0	2	2	2	2	2	2	2	2	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Post-ned	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fl	Post-fled.
Event R	Dist.	30.5	30.5	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	30.5	30.5	19	19	15.2	15.2	30.5	30.5	19	=  -  -	اة	5	<u>=</u>	19	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2
Event	Type	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	.50 cai.	So cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
Date		-	Н	Н	_	5/17		5/21	5/21	5/21	$\vdash$	╀	⊢	-	5/26	5/26	5/26	╀	╁	╁	╁╴	┢╌	5/13	5/13	H	5/13	5/13	5/13	Н	H	5/13	5/13	ᅱ	╅	+	+	+	+	6/3	٦	6/3	6/3	6/3	╁	╁	╁	H
Co.		19	19	19	61	19	19	19	19	19	19	19	19	88	88	88	88	88	120	120	120	125	125	125	125	125	125	125	125	125	125	125	125	125	2   2	127		127	127	127	127	127	127	127	127	127	127

1		=	1.	1	ı	ı	i	ı		ı	ı	1	ı	ı	ı	1	ı	.			l.	ı	I _	I _	۳ا	ا_	۲.	141		ا سا	a۱	_	1	ı	_  _	. 1.	۔ ا۔	.  .	ا.	ر ا	را ہ		. _	ا	اه	1-	ام	_	2	ţ
The control of the			SEL SEL	108.7	93.9	95.3	95.2	8.8	95.0	92.8	93.3	93.7	043	2 2	84.8	85.1	84.6	84.4	77.5	88.0	87.0	86.2	87.0	86.0	105.	114	113.	102.	93.8	10.	105.	89.3	78.5	74.	77.7	9	76.0	7.0	6	16	91.	g	12	96	=	101	87.5	86.7	92.5	
Part   Part		20000		39		37		37	33	45	43	4	46	}	£ 3	43	43	41	39	42	41	8	9	8	78	99	3	73	62	63	ες.	22	42	42	4	47	4 5	3 5	4 8	28	8	8	8	3	29	63	\$	47	55	
Part   Part			i	5	48	ος (	49	12	48	55	22	55	25	5	9	46	46	46	40	45	44	4	4	44	8	89	99	28	19	64	23	22	14	9	£ 3	9	₽  -	₹	2	52	8	88	29	3 3	2	63	47	45	53	
Part   Part		12500	í	22	48	53	42	54	51	99	99	19	3 3	7 5	3	Ω	52	52	45	20	49	48	49	47	85	73	70	83	19	65	99	54	6	39	42	<del>우</del>	을 달	\$ 5	7 05	69	23	8	9	1.9	49	2	47	49	55	
Part   Part	Ì	000	1	<del>∞</del>	19	3	8	99	64	65	65	5	3 8	3 3	2	82	28	58	20	55	55	54	54	54	87	74	73	85	64	69	9	28	43	40	4 3	<del>2</del>	43	5	, 89	99	89	4	9	3 =	2	282	53	52	9	
The control of the			1	8	8	88	8	۶	89	89	89	8	3 8	2 :	<u></u>	<u>-</u>	8	19	53	9	09	58	59	28	88	78	9/	98	19	71	64	79	48	44	84	84	47	48	3 5	5 5	3 3	3 2	· %	3 5	74	2,6	88	28	49	
The continue   The		6300	1	98	8	69	8	73	70	6	5	92	5   5	2	\$	3	63	63	55	64	63	62	62	19	96	79	77	87	70	77	69	99	22	48	22	22	12	25	5 5	3/3	3 4	9	3 8	5 2	1 2	11	[29	19	89	
The control of the	Ì	2000	1	8	70	73	11	75	72	72	17	. 2	1 5	2 ;	8	8	64	64	57	99	9	2	8	49	16	8	82	87	72	81	73	69	55	12	55	52	54	4. S	27	71	7	, C	2, 2	74	74	77	3	2	69	
		4000		8	72	73	73	78	73	73	73	1	5 5	ŧ	29	67	99		⊢	-	-	⊢	+-	જ	+-	⊢	╄	₩	ļ.,		_	<u> </u>		-	-+		-+	-+-	+		┿	4-	+		+	+-	+-	+-	+-	4
Part   Part		0 3150		-	$\dashv$			Н	├	┿	+	+	+	+		$\dashv$		<u> </u>	⊢	┢	├	+	╁	╀	╀	┼	+-	╄	⊢	-	<u> </u>	-	-	$\dashv$	-+	-	$\dashv$	+	+	┿	+	+	+	+	╫	┿	┿	+	┼~	4
No.   No.		0 250	-		$\dashv$	-	_		⊢	╀	╀	╁	+	+		-		$\vdash$	┝	╁	┝	╀	╁	╄	┼-	+-	╀	╀	├	Н	-			$\dashv$	-		$\dashv$	-	4-		┿	+	+		┿	+-	╀	+	+-	4
State   Stat		00 200	-	-		$\dashv$		$\vdash$	├	╀	┿	+	+	+	$\dashv$	_	<u> </u>	├	┝	┞	┝	╁	+	╀	╀	╀	╀	┿	⊢	⊢	-	H	$\vdash$	Н	-	┥	-	+	+	+		+		+	┿	+	┿	+	+	4
Poster         Formal         Rev. No.         Rev. No. <t< td=""><td></td><td>250 16</td><td>_</td><td></td><td>Н</td><td><math>\dashv</math></td><td>_</td><td>-</td><td>H</td><td>+</td><td>┿</td><td>╌├╴</td><td>+</td><td>+</td><td></td><td>_</td><td>_</td><td>⊢</td><td>╀╌</td><td>╁</td><td>⊢</td><td>╀</td><td>+-</td><td>╀</td><td>+</td><td>╁</td><td>-</td><td>┿</td><td>ļ.,</td><td>-</td><td><u> </u></td><td>⊢</td><td>-</td><td>Н</td><td>-</td><td></td><td>4</td><td>-+</td><td>+</td><td>-</td><td>+</td><td>+</td><td>+</td><td>+</td><td>+</td><td>+-</td><td>+-</td><td>+</td><td>+-</td><td>1</td></t<>		250 16	_		Н	$\dashv$	_	-	H	+	┿	╌├╴	+	+		_	_	⊢	╀╌	╁	⊢	╀	+-	╀	+	╁	-	┿	ļ.,	-	<u> </u>	⊢	-	Н	-		4	-+	+	-	+	+	+	+	+	+-	+-	+	+-	1
Type         No.         No.         No.         Bits         Post of the control         No.         No.         Post of the control         No.			$\dashv$		Н	$\vdash$	_	-	H	╀	╀	+	+	+	$\dashv$			╁	╀╌	╁	╁	╁	╁	╁	╁	╁	93	85	9/	8	98	74	19	19	62	3	09	5	3 8	2 5	2 3	6 3	8 8	6 4	2   8	2 8	3 5	1/2	14	
719.         Porell         Freel         Porell         Porell <td></td> <td>908</td> <td>-</td> <td>68</td> <td>71</td> <td>72</td> <td>74</td> <td>9/</td> <td>28</td> <td>75</td> <td>7,</td> <td>2 4</td> <td>ر ا</td> <td>72</td> <td>89</td> <td>0/</td> <td>69</td> <td>69</td> <td>15</td> <td>17</td> <td>17</td> <td>92</td> <td>, 5</td> <td>89</td> <td>16</td> <td>62</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td>_</td> <td><math>\boldsymbol{-}</math></td> <td>_</td> <td>_</td> <td>_</td> <td>-</td> <td>—</td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td><math>\boldsymbol{+}</math></td> <td>+-</td> <td><del>- </del></td> <td>-</td> <td>_</td>		908	-	68	71	72	74	9/	28	75	7,	2 4	ر ا	72	89	0/	69	69	15	17	17	92	, 5	89	16	62	-	-	-	-	-	-		_	$\boldsymbol{-}$	_	_	_	-	—		-	-	-	-	$\boldsymbol{+}$	+-	<del>- </del>	-	_
Print         Print <th< td=""><td></td><td>630</td><td>_</td><td>-</td><td>_</td><td></td><td>_</td><td></td><td>+-</td><td>-</td><td>_</td><td>_</td><td>_</td><td>_</td><td></td><td>_</td><td></td><td>-</td><td>+</td><td>+</td><td>-</td><td></td><td>+-</td><td>+</td><td>+</td><td>-</td><td>-</td><td>+-</td><td>_</td><td></td><td></td><td>_</td><td>_</td><td>-</td><td><math>\boldsymbol{\vdash}</math></td><td>_</td><td>_</td><td>_</td><td></td><td>-</td><td></td><td>+</td><td></td><td>-</td><td>-</td><td></td><td>-</td><td>_</td><td>-</td><td>→</td></th<>		630	_	-	_		_		+-	-	_	_	_	_		_		-	+	+	-		+-	+	+	-	-	+-	_			_	_	-	$\boldsymbol{\vdash}$	_	_	_		-		+		-	-		-	_	-	→
Print         Five this         RCM         RRA, Time         Mic         Base         71         1         1         20         1         20 <td></td> <td>400 50</td> <td></td> <td>16</td> <td>75</td> <td>75</td> <td>75</td> <td>62</td> <td>75</td> <td>: 8</td> <td>3 3</td> <td>8 5</td> <td>٥</td> <td>8</td> <td>09</td> <td>19</td> <td>89</td> <td>19</td> <td>S</td> <td>2</td> <td>63</td> <td>च</td> <td>: 6</td> <td>8</td> <td>22</td> <td>8</td> <td>8</td> <td>98</td> <td>73</td> <td>+</td> <td>-</td> <td>+</td> <td>57</td> <td>55</td> <td>28</td> <td>99</td> <td>99</td> <td>95</td> <td>[9]</td> <td>=  </td> <td>/9</td> <td>-</td> <td>g (</td> <td>ءَ اَ</td> <td>4 6</td> <td>2 2</td> <td>2 2</td> <td>5 E</td> <td>3 2</td> <td></td>		400 50		16	75	75	75	62	75	: 8	3 3	8 5	٥	8	09	19	89	19	S	2	63	च	: 6	8	22	8	8	98	73	+	-	+	57	55	28	99	99	95	[9]	=	/9	-	g (	ءَ اَ	4 6	2 2	2 2	5 E	3 2	
919         Fig. 1         Rey         Nic.         Nic.         Base         7         7         1	(Z)	315			<u> </u>	-	⊢	╄~~	1								1		_			_		_	_			_	_	+	٠	-	_		-	-	-	_		-		-	-	-	-	-	-	-		_
Attace         Postart         Event         Revert         Resp.         Time         Prost         (H)         Attack	icies (H	200 25					_	-	+	-								70	63	75	14	74	77	. 4	:   &	₹ [ @	3 8	3 8	86	92	83	77	99	28	65	65	64	64	۶ ا	= !	6	6	5	ا و	2 8	3 8	۲, ۲	5 5	2 %	3
Attace         Postart         Event         Revert         Resp.         Time         Prost         (H)         Attack	requer	25 160											_	_	_		-	-		-	+-		-	_								_	+			_	_		_	_	_		_	_	_	_	_	_	_	_
Attace         Postart         Event         Revert         Resp.         Time         Prost         (H)         Attack	enter F	100		26	82	98	82	8	8	3 %				98	73		73	73			ĕ	1				3 %	3 5	, 68	2	8	2	8	2	88	89	89	19	29	73	12	7,	4	-	11	-+	2 8	-		-	_
Date         Event         Resp.         Time         Pos.         III           5/17         50 cal.         30.5         2         3.0         Base         61           5/19         50 cal.         61         2         2.6         Base         61           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         0         2         2.6         Base         62           4/21         50 cal.         61         0         1.8         Base         62           4/21         50 cal.         61         0         Base         64         475           4/22         50 cal.         11         2         1.8         Base         7           4/22         50 cal.         11         2         1.8         8         6           4/22         50 cal.         11         2         1.8         8         6           4/22	trum C	80		-	+	-	┼~	+-	-	<del>-</del>	-	$\boldsymbol{+}$	-+	_	⊢	-	+	-	-	+	-	_	-		-	-			-		+-	_		-	┼	┿	-		_	_	$\rightarrow$	-	_	_	-+	5 2				
Date         Event         Resp.         Time         Pos.         III           5/17         50 cal.         30.5         2         3.0         Base         61           5/19         50 cal.         61         2         2.6         Base         61           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         0         2         2.6         Base         62           4/21         50 cal.         61         0         1.8         Base         62           4/21         50 cal.         61         0         Base         64         475           4/22         50 cal.         11         2         1.8         Base         7           4/22         50 cal.         11         2         1.8         8         6           4/22         50 cal.         11         2         1.8         8         6           4/22	e Spec	20		+-	-	8	+-	+-	8	3 6	2 8	2 2	8	81	-	├	+	13	1 5	75	7	2 2	7,	; ;	, %	3 2	5 8	3 2	Š	8	92	+-	19	2	┼	2	┼	-	8	છ	S .	99	$\rightarrow$	-	-		-	_	-	
Date         Event         Resp.         Time         Pos.         III           5/17         50 cal.         30.5         2         3.0         Base         61           5/19         50 cal.         61         2         2.6         Base         61           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         0         2         2.6         Base         62           4/21         50 cal.         61         0         1.8         Base         62           4/21         50 cal.         61         0         Base         64         475           4/22         50 cal.         11         2         1.8         Base         7           4/22         50 cal.         11         2         1.8         8         6           4/22         50 cal.         11         2         1.8         8         6           4/22	3 Octav	32 40		+	+	-	+	+	-		-	-	_	_	⊢	69	68 71	+-	+-	┰	+	+			+	+			_	+	+	+	┰		-	┿~	┰	Н	-	-	-	-		-	-+	-	-	2 8	3 2	-
Date         Event         Resp.         Time         Pos.         III           5/17         50 cal.         30.5         2         3.0         Base         61           5/19         50 cal.         61         2         2.6         Base         61           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         0         2         2.6         Base         62           4/21         50 cal.         61         0         1.8         Base         62           4/21         50 cal.         61         0         Base         64         475           4/22         50 cal.         11         2         1.8         Base         7           4/22         50 cal.         11         2         1.8         8         6           4/22         50 cal.         11         2         1.8         8         6           4/22	B) at 1/	25		84	92	72	65	73	7,	5 5	2 8	7	72	73	99	-	-	+-	+	-	-	-	-	-			_	_		-	+		-	-	+	+-	+	-	-		-		$\rightarrow$		_	_				
Date         Event         Resp.         Time         Pos.         III           5/17         50 cal.         30.5         2         3.0         Base         61           5/19         50 cal.         61         2         2.6         Base         61           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         2         2.6         Base         62           5/19         50 cal.         61         0         2         2.6         Base         62           4/21         50 cal.         61         0         1.8         Base         62           4/21         50 cal.         61         0         Base         64         475           4/22         50 cal.         11         2         1.8         Base         7           4/22         50 cal.         11         2         1.8         8         6           4/22         50 cal.         11         2         1.8         8         6           4/22	SEL (d	16 20		-	-		+-	_			-	-+		_	-	+	+-	-		_	-			-	-				-	┿	+-	-	+-	4-	+	+-	-		$\overline{}$	-	-	-+	-	-	ভ	S :	3 (	3 2	10	٥
Date         Event         Event         Resp.         Time         Mic.           5/17         .50 cal.         30.5         2         3.0         Base           5/19         .50 cal.         61         2         2.6         Base           5/19         .50 cal.         61         2         2.6         Base           5/19         .50 cal.         61         2         2.6         Base           4/21         .50 cal.         61         2         2.6         Base           4/21         .50 cal.         61         0         1.8         Base           4/21         .50 cal.         61         0         1.8         Base           4/22         .50 cal.         61         0         Base         4/26         88e           4/22         .50 cal.         61         0         0         Base           4/24         .50 cal.         61         0         0         Base           4/25         .50 cal.         122         1         Base           4/26         .50 cal.         122         1         Base           4/27         .50 cal.         122         1         Base	Band	13		_	_	ļ	Ļ	┵~	-	+	-			_		+	-		-	_	-	-	-	-	+		-	-	-		-	-		_	-	+-	+	-	$\vdash$		-	-	_		_	$\rightarrow$	-			_
Date         Event         Event         Resp.         Time         Profinal           5/17         .50 cal.         .90.5         .26         .30         B           5/19         .50 cal.         .61         .2         .26         B           4/21         .50 cal.         .61         .0         B         B           4/21         .50 cal.         .61         .0         B         B           4/21         .50 cal.         .122         .1         B         B           4/22         .50 cal.         .122         .1         B         B           4/22         .50 cal.         .122         .1         B         B           4/22         .50 cal.         .122         .1         B         A         A           4/22         .50 cal.         .122         .1 <td>_ </td> <td></td> <td>-</td> <td>┢</td> <td><u>بر</u> ا</td> <td>Base</td> <td>-</td> <td>+</td> <td>╈</td> <td>-+</td> <td>+</td> <td>_</td> <td>_</td> <td>┝</td> <td>-</td> <td>+-</td> <td>+-</td> <td>+-</td> <td>+</td> <td></td> <td>+</td> <td>╅</td> <td>+</td> <td>+</td> <td>+</td> <td>+</td> <td>-</td> <td>-</td> <td>十</td> <td>-</td> <td>+-</td> <td>_</td> <td>+</td> <td>+-</td> <td>+-</td> <td>+-</td> <td>+</td> <td>1</td> <td>Н</td> <td>-</td> <td>-</td> <td><math>\rightarrow</math></td> <td></td> <td>-</td> <td></td> <td>-+</td> <td>-</td> <td>_</td> <td><math>\neg</math></td> <td>_</td>	_ 		-	┢	<u>بر</u> ا	Base	-	+	╈	-+	+	_	_	┝	-	+-	+-	+-	+		+	╅	+	+	+	+	-	-	十	-	+-	_	+	+-	+-	+-	+	1	Н	-	-	$\rightarrow$		-		-+	-	_	$\neg$	_
Date         Event         Event         Resp.         Time           1ype         1ype         Dist.         Resp.         Time           5/17         .50 cal.         61         2         2.6           5/19         .50 cal.         61         0         1.8           4/21         .50 cal.         61         0         1.8           4/22         .50 cal.         11.2         1.8         1.8           4/26         .50 cal.         11.2         1.8         0.0           4/26         .50 cal.         11.2         1.1         0.0           4/26         .50 cal.         11.2         1.1         0.0           4/26         .50 cal.         11.2         1.2         0.0           4/26         .50 cal.         11.2         1.2 <t< td=""><td>Σ</td><td></td><td>- 를</td><td>Ba</td><td></td><td></td><td>12</td><td>1 6</td><td>16</td><td>2   2  -</td><td>2   E</td><td>E B</td><td>Ba</td><td>Ba</td><td>l<sub>E</sub></td><td>la a</td><td>16</td><td>1 2</td><td>1</td><td>مُ ا</td><td>1</td><td>ă   c</td><td>ا ا</td><td>1</td><td><u> </u></td><td>ž į</td><td>3 0</td><td>ا گ</td><td>3 6</td><td>عُ اِقْ</td><td>3 2</td><td>5   2</td><td></td><td>i m</td><td>m</td><td>m</td><td>m</td><td>m</td><td>B</td><td>ర్</td><td>ర్</td><td>ర్</td><td>రి</td><td>ర్</td><td>ర్</td><td>రి</td><td>ပ္ပို</td><td>7</td><td>7</td><td>ceil</td></t<>	Σ		- 를	Ba			12	1 6	16	2   2  -	2   E	E B	Ba	Ba	l <sub>E</sub>	la a	16	1 2	1	مُ ا	1	ă   c	ا ا	1	<u> </u>	ž į	3 0	ا گ	3 6	عُ اِقْ	3 2	5   2		i m	m	m	m	m	B	ర్	ర్	ర్	రి	ర్	ర్	రి	ပ္ပို	7	7	ceil
Date         Event         Event         Funt         RCY           7/ype         1/ype         Dist.         Resp.           5/19         .50 cal.         30.5         2           5/19         .50 cal.         61         0           4/21         .50 cal.         61         0           4/21         .50 cal.         61         0           4/21         .50 cal.         112         1           4/22         .50 cal.         112         1           4/22         .50 cal.         112         0           4/22         .50 cal.         112         0           4/24         .50 cal.         112         0           4/25         .50 cal.         112         0           4/29         .50 cal.         112         0           6/2         .50 cal.         112         0	Rec.	Time	٤	9	2.6	2.6	96	26	2 -	2	-									Š	3	3	3 3	0.0	3 .	Ted.	- <u>t</u> eg.	iled.	1100	fled.		- Feb	- Ped	-fled	-fled.	-fed	-fled.	-fled.	-fled.	-fled.	-fled.	-fled.	-fled.	-fled.	-fled.	r-fled.	-fled	r-fled.	r-tled.	t-tled.
Date         Event         Event           7ype         (m)           5/17         .50 cal.         30.5           5/19         .50 cal.         30.5           5/19         .50 cal.         61           4/21         .50 cal.         61           4/21         .50 cal.         122           4/21         .50 cal.         122           4/22         .50 cal.         122           4/26         .50 cal.         122           4/29         .50 cal.         122           4/20         .50 cal.         15.2           4/20         .50 cal.         15.2           6/2         .50 cal.         15.2           6/2         .50 cal.         122           6/2         .50 cal.         122           6/2         .50 cal.         122           6/2         .50 cal. <td>ΝÇ</td> <td>Seso.</td> <td></td> <td>,</td> <td>1/2</td> <td>1/2</td> <td>1</td> <td>1,</td> <td>1,</td> <td>7</td> <td>0</td> <td>٥</td> <td>0</td> <td>0</td> <td>-</td> <td>1-</td> <td>†-</td> <td>+</td> <td>- -</td> <td>- -</td> <td>, ,</td> <td>١,</td> <td>0</td> <td>-</td> <td>٦</td> <td>Post</td> <td>Post</td> <td>Post</td> <td>io l</td> <td>Los Los</td> <td>100</td> <td>Post</td> <td>Posi</td> <td>Pos</td> <td>Pos</td> <td>Pos</td> <td>Pos</td> <td>So</td> <td>Pos</td>	ΝÇ	Seso.		,	1/2	1/2	1	1,	1,	7	0	٥	0	0	-	1-	†-	+	- -	- -	, ,	١,	0	-	٦	Post	Post	Post	io l	Los Los	100	Post	Post	Post	Post	Post	Post	Post	Post	Post	Post	Post	Post	Posi	Pos	Pos	Pos	Pos	So	Pos
Date         Event           7/17         1 ype           5/19         .50 cal.           4/21         .50 cal.           4/21         .50 cal.           4/21         .50 cal.           4/22         .50 cal.           4/24         .50 cal.           4/26         .50 cal.           4/29         .50 cal.           4/29         .50 cal.           6/2         .50 cal. <th>Г</th> <th></th> <th></th> <th>30 5</th> <th>196</th> <th>19</th> <th>5 2</th> <th>5   2</th> <th>3 3</th> <th>91.5</th> <th><u>=</u></th> <th>19</th> <th>19</th> <th>19</th> <th>122</th> <th>132</th> <th>122</th> <th>1 2</th> <th>771</th> <th>771</th> <th></th> <th>C.1%</th> <th>91.5</th> <th>91.5</th> <th>91.5</th> <th>15.2</th> <th>15.2</th> <th>30.5</th> <th></th> <th>5 5</th> <th>10 2</th> <th>21.5</th> <th>2,12</th> <th>122</th> <th>91.5</th>	Г			30 5	196	19	5 2	5   2	3 3	91.5	<u>=</u>	19	19	19	122	132	122	1 2	771	771		C.1%	91.5	91.5	91.5	15.2	15.2	30.5		5 5	10 2	21.5	2,12	122	122	122	122	122	122	122	122	122	122	122	122	122	122	122	122	91.5
Date           Pate           S/17           S/19           S/10	ŀ			+	$\perp$	Cal C	100	Cal.	+	4	0 cal.	0 cal.	0 cal.	0 cal.	0 cal	lea 0	, cair.	o cal.	o cai.	Cal.	Cal.	0 cal.	4	-	+	o cal.	50 cal.	o cal.	o car.	o cai.	o car.	o cal.	0 Cal.	.0 Cal.	in cal	in or	30 cal	50 cal.	50 cal.	50 cal.	50 cal.	50 cal.	50 cal.	50 cal.	50 cal.	50 cal.	50 cat.	50 cal.	50 cal.	50 cal.
	$\vdash$		•	+	+	+	+	十	+	1	-		┝	+	╁	╁	+	+	+	╁	+	+	┪		+	$\dashv$	$\dashv$	$\dashv$	$\dashv$	+	+	+	+	+	╁	+	+	+	+	┝	H	├	$\vdash$	┝	$\vdash$	Н		H		┨
	┡			+	+	+	+	4	+	$\dashv$	-	_	-	╄	╀	+	╬	+	+	+	$\dashv$	-	$\dashv$	$\dashv$	-	-	-	4	4	+	+	4	+	+	+	4	+	╀	╀	┡	╀	_	L	_	L	Ш		Н		

Z .	Calc.	SEL	93.4	110.9	112.2	93.0	93.0	92.9	93.7	92.9	93.0	92.9	93.6	0.68	89.7	17.7	0.17	2,71	103.4	1125	0 701	0.00.0	7.7.7	200	7.66	98.5	83.6	107.2	118.2	116.0	103.4	0.15	104.3	1 1 2 1 1 2 1	85.9	104.2	103.7	112.8	108.9	97.6	9.68	101.2	99.5	84.9	113.9	113.8	114.9
ľ	3000		22	22	57	43	4	40	43	15	51	51	20	40	4	<del>,</del>	<del>1</del> 5	3 8	2 2	2 8	3 5	÷ 5	, 44	;	4 ;	<del>0</del>	9	28	74	65	<del>∞</del>   3	2 3	2 5	, 84 84	43	4	78	99	22	52	48	47	43	44	36	8	7
	16000 3		55	55	55	22	57	57	58	22	58	88	58	43	43	;	#   4	3 5	2 2	3 5	3 5	3 3	3 5	;	€   	2	#	98	12	3 3	<u>چ</u> ا	8 3	۲ <del>ز</del>	F 5	4	4	82	26	72	2	22	47	42	45	89	<u></u>	3
	12500 1		99	99	55	2	8	64	64	64	65	64	99	49	48	3 5	2 0	3 5	,   ×	3 5	3 2	ţ 9	6 5	; ;	\$   S	<u></u>	8	88	6/	9 9	2 87	2   5	, t	. ×	49	45	84	89	Se	8	22	20	42	49	63	्र	3
l	100001		00	32	98		66	66	69	89	96	- 69	69	99	55	+	+	+	+	+	+	+	+	+	+	$\dashv$	-	$\dashv$	+	$\dashv$	+	+	+	+	╀	-	Н		┥	-	$\dashv$	Н	႕	54	9	67	- 8
	8000 10		9	Ц		$\dashv$		_			L		$\vdash$		9 5	+	-	+	+	+	+	+	+	+	4	-	4	-	4	+	-	+	+	+	59	<u> </u>	Щ		-		65		_	Н	6	2	69
	6300 18	$\overline{}$	-		85	72	$\dashv$		Н		$\vdash$	_	Н	$\dashv$	59	+	+	+	+	+	+	+	╁	╁	+	$\dashv$	+	+	+	واء	13 87	: 1	g :	2 5	159	52	87	62	2	92	89	63	56	19	70	12	7/
	5000		70	81	85	23	74	74	75	73	74	74	75	89	29	9 9	3 6	7 6	22	5 2	;   [	; ;	: 5	- 5 \	۶	\$ <del>\$</del>	2	5	% i	æ	3 5	:	20 5	3 5	2	Se	68	-8	7	77	69	62	57	62	7	=	72/
	400	4000	73	82	98	74	7,	74	75	74	74	74	75	70	6 5	=   =	=   8	3 5	, 08	6 8	3 5	7/	2 9	3 5	8	8	99	92	£	28	2 %	۶ ج	2 8	3 5	99	88	96	84	28	79	72	73	70	99	23	74	47
	2150	0010	75	82	98	75	75	75	9/	75	75	75	75	72	72	Ç }	1 8	3 8	7 00	8 8	G 7	3 5	, 0,	? ;	- ;	63	99	8	8	8	5 5	; ;	Ç (5	3 5	19	63	90	87	8	81	73	77	73	29	74	76	11
	2500	4.300	=	-	98		┥	-		_	-		Н		-	+	+	+	+	╬	+	+	+	+	+	$\dashv$	+	-+	+	+	+	+	+	+	9	├-	Н	$\dashv$		-	-	$\vdash$	_	Н	+	<b>≈</b>	
	0006 00	707	2 76	Н	\$8		┥	_	Н		_		Н	$\dashv$	-+	+	+	+	+	+	┿	+	+	+	-+	$\dashv$	-	+	$\dashv$	+	+	+	+	┿	89	├	-	$\dashv$	-		_	$\vdash$		69 0	$\dashv$	+	8
	1250 1500			_	86 84	$\dashv$					$\vdash$	_	$\vdash$		71 72	+	+	+	╀	+	+	70 74	+	1 2	+	74 68	-	92	$\dashv$	$\dashv$	88 8	+	8/ 83	+-	89 69	⊢	Н	Н		┥	Н		_	69 70	+	+	84 84
	1000 112			Н	88	$\dashv$	$\dashv$		-	Н	$\vdash$	Н	$\vdash$	$\dashv$	17	+	+	+	+	+	╅	+	+	+	+	+	88	$\dashv$	┪	$\dashv$	88 5	+	2 2	┿	89	╁	H		-	818		88		H	+	ω ω	_ 
	000				3 06										72								L								88 1	_	_	┸	69	┖	Ш			_		Ш		Ш	_	£	5
	023	0.50	-	28 /	$\vdash$	_	$\rightarrow$	-	-	-	74 74	$\overline{}$	_		72 72	-	_	_		60 63	_	_	_	_	-	_	63 67	$\rightarrow$	-	_	88 6	-	86 87		64 67		-	$\overline{}$	$\rightarrow$	_	70 72	3 78	02   29	-	-	82	) (2)
	215 400 500	004	27 77	$\vdash$	-	74 74		-	$\vdash$	⊢	_	_	74 7	-	_	-	-	2 8		6 0		, 6, 2,	_				-+	92	66	-+	-+	-+	8 9		+	-	-	94 8	-		70 7	73 7	64 6	₩			26
		30 313	62 62	16 50	106 91	8 72	7 71	77 71	_	12 8	7 72	-	78 71	_	78 74	-	-	-	+	71 07	-	0/ 10	-	9 8	-	-	99 99		116 113	_	93	_	107	70 67		102 99		88 84	-		74 69	85 80	78 72	Н	-	-+	89   94
	inter Frequencies (HZ)	7 007	84	109	110		82	82	83	83	82	83	83	79	ଛ :	5 5	<b>7</b> 5	, 8	_	2 8	2 8	6 8	3 7	2 8	22	92	89	42	8	6	2 2	2	¥ 8	7 2	9	68	6	68	16	82	8/	87	. 83	74	8		96
	enter Frequencies	201	_		_	_		_	_			-	-	_	82 81	-	_	_			_	2 2		_		_			88		22 5		82 86		-	82 84	-	_	101 101		80 79	-	68 93		88	= 00 1	<u></u>
			83	84	98	28	84	84	85	84	84	84	82	08	æ :	ē 6	2 2	, 6	è 6	è è	2 8	7, 6	20 62	: [	98	8	75	94	88	87	2	<u>و</u>	22	9 6		+	-	94	96	68	18	87	82	_		-	6 92
	ctrum	2	81 83	79 82		80 82	_	79 82	-	_	_	79 82	80 83	77 78	$\rightarrow$	-	80 80	60 00		-		9 5			-	73 77		-	-	-	_	-	29 81	_	-	74 76	85 89	83 88		68 98	8 8/	77 82	73 7			85 86	84
ľ	Band SEL (dB) at 1/3 Octave Spectrum C	00 0	-	75 78	80 81	76 78		76 79	_	62 92	62 92	62 92	77 79	73 75	_	-	14 /0	CO CO		+0 70 77		0/ 0/		-		-	-	_	-	_		-	77 78		+-	71 72	82 84	80 79	_		-	72 75	12 89			77 82	79 83
	1/3 Oct	36	75 7	72 7	77 8	73 7	73 7	72 7	74 7	73 7	73 7	72 7	73 7	_	_	-	-	3		70 02	٠ ۲	۲ ر	ر <u>د</u>	-	_	9	_	_	-			_	_	, ,	-	69	8 08	78	11	1.1	11	70	99	29	79	8	79
	(dB) at 1		66 73	17 17	72 75	20 68		67 72	68 71	69 69	68 70	67 72	68 70	68 63	-	-	λ λ 80 8	00 00	-	10/	-	60 00	-	-	65 65	_	_	_						C 2	_	<b>2</b>	72 79	73 78	72 76	68 75	89 19	89 09	56 64	_	_	79 75	_
	SEL (	9	69	71	73		63	54	-	89	62	63	59	55	88	مَرُ	2 5	7 7	2 3	8 5	? {	70	۶ و	3	22	49	5	77	%	72	છ	5	<u> </u>	: 5	3 2	88	77	<u>~</u>	7.1	89	R	ဒ	9	59	77	77	78
1	Band	21	63 60	73 67	72 71	64		53	09	57 49	58 51	57 51	-	56 48			2 S	2 8	_	2 8	-	6 G	_	۶   ۱	$\rightarrow$	_	_	_	_	_	-			8 8		52 59	99 29	73 72		21 59	49 52		55 56			99	_
	S E	Š	-	Cavity	Cavity		Base	Base	Н	┰	Base	-	Base	-	$\vdash$	十	_	✝	-	Dase	-+	Cavity	Base	-+		_		_	-		$\neg$	Base	Base	Cavity	+-	Cavity	Base	Cavity	Cavity	Base	Base	Cavity	Cavity	Base	Ī	_	Cavity
	Rec,	- (min										_		5.2	5.2	7,	7		iled.	$\dagger$	1	Ť	ried.					П			fled.	fled.	1	1	fled	T.				·fled.	·fled.					Post-fled.	7
	RCW	resp.	Post-fled	Post-fled.	Post-fled.	2	2	2	2	2	2	2	2	2	2	7	7 2	Post-ried	rost	Post-ried.	Post-fled	Post-fled	Post-fied.	Post-nea.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled.	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post	Post
	Event	i (i	91.5	91.5	91.5	19	61	19	19	19	61	19	19	91.5	91.5	21.5	51.5	7.51	7.01	50.5	c.ue	اة	10	71.C	91.5	122	122	15.2	15.2	30.5	30.5	19	61	51.5	122	122	30.5	30.5	19	19	91.5	91.5	122	122	30.5	30.5	30.5
	Event	- lype	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.Su cal.	.50 cal.	.50 cal.	.So cal.	.50 cal.	.yo cal.	.So cal.	.50 cal.	.yu cai.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.yo cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
	Date		6/2	6/2	6/2	5/4	5/4	5/4	5/4	5/4	5/4	5/4	5/4	6/5	6/5	6/6	5/9	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/17	21/9	6/17	21/9	21/9	6/17	41/9	21/9	5/27	5/27	5/27
	Col.	•	133	133	133	139	139	139	139	139	139	139	139	139	139	139	139	<u> </u>	<u> </u>	<u> </u>	<u>2</u>	<u>6</u>	2 3	3	139	139	139	139	139	139	139	139	139	65	130	139	139	139	139	139	139	139	139	139	143	143	143

Calc.	SEL	6.86	0.66	100.2	114.7	110.8	1010	0.4.0	97.0	0.501	500	88.3	85.1	88.8	84.5	90.0	90.6	90.4	25.7	103.0	105.2	105.9	106.9	106.8	106.5	115.1	111.4	100.4	85.7	94.2	93.9	111.9	112.7	113.9	100	109.4	117.6	118.4	96.1	87.6	97.4	97.5	98.4	99.5	109.1
9000		73	74	٤ :	\$ 6	3 8	2 8	3   2	100	40 5		44	e	<del>4</del>	75	48	75	74	£	4	7	77	11	-	8	99	99 2	5 2	2 4			Se	57	3 3	3 89	8 8	99	17	99	19	99	19	89	89	\$
, 0000,		78	78	28	3 :	\$ 6	à	8 2	3 3	ک کو	<u>چ</u> :	2	e	45	× 1	2	S S	22	49	27	<b>&amp;</b>		<del></del>	æ	8	2	63	2 3	2 5	15	20	19	5 t	/9	2 2	2	74	9/	72	72	72	73	74	74	96
1 00361		08	80	@ E	7 5	6	3 8	8 8	3 5	<u> </u>	<del>-</del>	23	44	\$ ;	<del>2</del>	2	3 3	3 3	3	5	2	S S	<u>ω</u>	83	88	75	99 8	<u> </u>	3 2	53	51	42	જ	1 2	1 2	2 68	92	62	75	76	75	2/2	78	77	26
, 0000	1	81	81	- E	2 5	% F	-   8	8 8	\$ 5	, ;	4	62	25	26	<u>~</u>	8	8 .	29 5	3	2	26	84	88	8	£	11	۶ ا	\$ 3	3 8	63	63	89	8	2 5	£ &	8 8	8	158 158	77	78	77	78	œ	79	16
0000		18	81	2	2 6	2 ;	4 8	6 8	8 8	200	75	8	57	8 ;	2	2	3 3	3 3	\$	74	8	8	8	88	8	62	27	2 5	3 6	19	29	72	23	5 6	2 ~	8	:   &	2 8	78	62	79	79	18	18	26
_	0000	18	81	<u>-</u>	9 1	27	C 8	6 6	\$ 8	8 8	×	۶	29	8	3	7.1	2 :	=	29	11	88	8	8	8	&	81	92	è :	: 4	69	69	75	76	8 8	3 8	3 6	2	98	78	79	78	8	82	81	95
_ <b>L</b>		18	81	08	- 1	72	/ 8	88	S   E	<u>ک</u> و (	3	=	99	99	3	2	2	72	62	79	82	98	82	84	88	&	8 3	\$ 1	2 %	7	11	 8		8 2	. S	3 6	2 28	88	79	8	79	81	84	82	94
999	4000	81	81	82	29	75	ر 8	8	S S	8	63	22	67	8	8	74	2	4 3	3	8	98	84	88	8	68	81	83	2 F	+	73	⊢		8	8 8	8 8	9 6	8	12	8	8	83	83	Н	H	94
1	3150	84	82	83	8	- 3	≅   8	+	\$ 8	+	-		-	$\dashv$	-+	-	+	-+	-+		8		-		8		+	8 8	+	7	₩	Н	-	8 8	╬	+	+	╁	+	+	+-	Н	Н	$\vdash$	92
1	0067		83	-+	-+	-	× 8	+	-	+	$\dashv$	-	-+	+	$\dashv$	+	-+	+	7				$\dashv$	$\dashv$	$\dashv$	Н	98	+		75	╀╌	91	$\dashv$	$\dashv$	╬	+	+	+	╁	╁	╀	$\vdash$	Н	Н	94
	2000	┝	Н	82	-+	+	+	+	+	+			-	+	-+	-	$\dashv$	$\dashv$			-	$\dashv$	$\dashv$		68		$\dashv$	2 8	+	╁	+	-	$\dashv$	3 33	╫	┿	┿	+	┿	╀	┼	-	3 83	$\vdash$	96   ‡
	0 1600	⊢	H	82	$\dashv$	-+	€ 3	+	+	+	-	-	2	$\dashv$	$\dashv$	$\dashv$	+	+	$\dashv$	-	$\dashv$	$\dashv$			$\dashv$	-	3 93	+	+	+-	+-	Н	-	2 8	+	-	╁	+	+	╀	╁	$\vdash$	$\vdash$	Н	4 94
	1250	83	84	83	$\dashv$	+	æ  8	+	£ 8	$\dashv$	-	$\dashv$	2	+		$\dashv$	$\dashv$	+	$\dashv$		Н			$\dashv$	88		┝┼	2 8	╅	╁┈	┿	Н	-	2 2	+	Ť	+	╁	+	╁	+-	+	83	Н	04
L	<u> </u>	82		82			<b>%</b>	_	_	_	_	_	69	_		_	_	75	_	_	Ш		_	94		<u> </u>	66	4	_	3 8	1			8 2	_	4	_	1	_	$\bot$	1	╄-	81	Ш	0
	<u></u>	╄	-	78 79		82	-	88 8	-+	-	-	_		$\dashv$	67 68	76 76	2 76	7 76	╌	-	-	87 94	-	-	-	94 101		${}^+$	2 2	-	77 78	-	-	-+	77 6	-+-	-	1	+	67	+	+	79 80	-	00
	200   630	78 7	-	-	-		8 6	_	_	-	-	-		-	-		75 7	74 7	$\dashv$		-	_		$\vdash$	Н	95 9		$\rightarrow$	2 5	+-	72 7	$\vdash$	$\vdash$		2 8	-		-	-	┿		+-	76 7	1	8
	400	L	₩		-	$\rightarrow$	25			_	_					7	1			-	┝	06	-	_	_	86	$\vdash$	-	2 5	+	┿	-		+	2 6	-	+	-	-	:  =	12	11	11	-	8
l	315	+-	84	-	-+	8		_	_	_		_	99		_	8	2	ଞ	64	90	94	94	96	65	94	16	84	8	2 V	3 2	5	87	98	8	£ 6	S 8	2 2	2 2	,  ≅	2 8	8	8	8	81	g
	250	87	98	88	2	8	g	5	87	8	62	89	64	89	99	74	75	75	70	66	26	66	100	100	66	92	83	8	\$ 2	3 %	78	8	91	8	7 2	ည် ရ	3 8	8 6	, 8	8	8 8	88	8	_	ý
3	125 160 200	98	88	68	86	8	_	_	_	68	69	74	72	76	73	79	79	6	74	64	96	26	86	86	8	95	-		<u>2</u> 5	¹ <u>≅</u>	8	101	108	60	3   3	2 8	-	1   1	} ≋	+	8 8	8	8	-	5
enter r requencies (nz)	<u> </u>	2	_	93	=	릐	_	8		-	8		L				26		73	_	├	-	68	⊢	8	Ē	-	_	8 2	_	-	_	Ξ	$\equiv$	_	7 5			:   %		+		88	+	8
1	<u> </u>	-	-	8			<u></u>	_		-	-		74	_	-				_	56 t	-		3 93		1 .	108	104	_	104		88						2 2	_		-	_	-	4	-	+
	<u> </u>	+	88	$\vdash$		_	8	$\overline{}$		:_1	3 73	0	7 76	_		1	~	_	7	~	_	~	3	<u>_</u>	6	7	84 90		82 5	, c	00	8	8	84 8	2 9	$\infty$	0 2	7 0	2 S	1 4	, E	<u>22</u>	47 80	<del> </del>   <u>9</u>	9
	<u>~</u>	86 85	-	-	$\overline{}$	$\overline{}$			-	84 8.	72 7	8 8/	76 7		75 76	78 8	77 82	_	74 7	68	6 16	6	93 9	91 9	8 06	85 8	_	_	_	0, 0,		8						2 8		_				88	5
Band SEL (dB) at 1/3 Octave Spectrum of	9	82 8	+	85 8	82 8	$\rightarrow$				$\rightarrow$	69	76 7	74 7	77 7	72 7	76 7	77 7	76 7	72 7	87 8	87	-	—		87.9	82	-	_	-	Į (×	_	182	-	-		-	-	2 5		+	-		+	_	-
ra ve	송 	98	+	82	92	89	-			-	29	73	71	74	69	_		-		85	87	-	88	-	98	-	-	_		7 8	_	-	11		-		-+	_	۶ ۶		-	-	-	_	-
	32	78	+-	1	82	75	-	-		83	64	71	69	72	19	71	20	_	99	82	+	98	98	87	88	82	9/	8	=	=   {	. 27	11	11	78	76	6 8	% :	∞ 5	3 5	, ,	77	19/	77	79	Į
	22	74	23	75	78	75	9/	8	79	79	19	<i>L</i> 9	9	89	79	89	89	69	63	77	84	85	84	84	81	9/	67	72	63	3 6	, (ê	73	74		છ	22	8	S 8	3 3	_	_	1 55	2		
٤	20	73	-	75	81	69	72	82	-	$\rightarrow$	22	63	8	64	99	63	63	-	09	78	8	85	87	98	+-	+	71	75	-	8 8		-	9/	$\boldsymbol{\vdash}$			-	æ  s		-	-			-	-
3	92	89	-	89	72	89	_	-	$\rightarrow$	$\overline{}$	52	62	88	-	53	65	63	_	8	71	17	77	78	8	+	-		_		7 5	_		99		26	_	_	_		8 8	_	3 5			
Banc	10 13	64	+	19	75	62	-	-		65	20	09	36	65	47	E9   1	52	59	54		Ļ	63	Ļ	3 76	+	+-	+	-	-	3 8	_	3 65	1 55	<del>  </del>		$\rightarrow$	-	2 3		9	_	14	65	-	-
	=	189	╈	19	78	, 68	-1	-1			38	49	47	8	45	19	51	55	4	62	╁	7	77	73	T	+	+	71	-	¥ 5	ە ⊢	y 73	y 7	++	x 28	_	_	× 8	— ₁	base 52	_	+	+	+	+
Mic	e Pos.	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Cavity	Cavity	Base	Cavity	Base	Base	Cavity	Cavity	Cavity	Cavity	Base	Base	Cavity	Cavity	a la	Base	Base	Base	Base	
Rec,	Time (m)		led.	led.	led.	led.	Jed.	led.	led.	led.										3.2	4.4	4.4	4.4	4.4	Jed.	Jed.	fled.	fled.	fled.	tled.	led led	Jed.	fled.	fled.	fled.	fled.	fled.	fled.	] <u>:</u>	2   2	7.1	17	12	2	
RCW	Resp.	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	-	-	-	-	-	-	-	-	-	2	2	2	2	2	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	7	7 (	7 6	1/2	1 2	
Event R	Dist. R	30.5	0.5	30.5	15.2	15.2	15.2	15.2	15.2	15.2	122	122	122	122	122	19	19	19	19	30.5	15.2	15.2	15.2	15.2	15.2	15.2	30.5	30.5	19	19	10 19	19	150	30.5	30.5	30.5	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	3
		+	╀	╀	-	<u> </u>			L	_	L	╀	1	<u> </u>	$\vdash$	L	L	-	lacksquare	╀	╀	Ļ	$\downarrow$	$\downarrow$	╀	+	+	L	Н	4	4	1	$\downarrow$	╁	Н		$\dashv$	$\dashv$	4	_	$\downarrow$	$\perp$	+	+	4
Event	Type	100 05	╁	╁	┼-	$\vdash$	.50 cal.	┢	┝	┢	$\vdash$	.50 cal.	╁	╁╴	╁	┢	7 .50 cal.	H	+	t	╁	┿	╁	+	+	+	┿	+-	$\vdash$	$\dashv$	.50 cal.	+	50 cal.	╁		.50 cal.		H	+	寸	+	7 SO cal.	1.	7 50 cal	-
Date		5/17	+	+	5/27	╀╌	┞	├	├-	┝	╄	╀	╀	4/23	╁	4/27	╀╌	╀╌	╀	╀	╀	╀	╀	+	+	+	╫	6/14	Н	4	5/9	+	6/3	+-	L	Н	Н	5/9	$\dashv$	$\dashv$	$\dashv$	5/17	+	- -	-
Sol.		15	1 2	5   5	143	143	143	5	143	143	148	148	148	148	148	148	148	148	148	4	15	2	2	2	2	1 2	2 2	151	2	25	79   5	2   3	162	192	162	162	162	162	162	2	<u>s</u>  :	S   2	2 2	8   8	3

3	Calc.	SEL	109.4	116.3	117.0	110.9	113.4	101.0	101.7	98.7	111.8	9'201	105.9	8.06	89.3	0.901	88.4	88.3	109.7	109.4	103.0	103.6	9.96	96.5	107.2	107.2	103.9	90.7	103.4	6.68	87.1	87.1	99.1	5.66	88.2	87.0	86.4	88.0	88.8	85.3	91.1	92.2	91.6	93.1	87.4	26.5	73.3
İ	00000		94	=	74	62	8	8	82	99	28	52	51	53	52	22	53	69	57	85	84	98	8	9	48	48	42	55	45	80	47	47	45	£			30	30			49	20	48	49	8	S 8	٦
	1,000		26	76	77	63	89	8	98	74	19	54	25	59	28	SS	22	55	52	88	87	68	7	11	49	49	46	62	44	57	8	8	4	44	46	44	41	47	\$	47	59	65	59	09	29	3	S
	13500		26	67	8	2	72	8	88	78	99	22	55	64	63	22	63	8	8	8	8	8	2	23	22	22	47	99	4	62	22	25	42	7 5	;   S	47	47	53	æ	22	Ê	8	3	65	59 ;	2	8
	10000		- 26	82	84	8	2	87	88	08	82	11	73	29	99	82	67	65	8	8	8	68	75	74	55	99	8	69	4	65	8	8	14 5	24 63	8 65	88	99	09	19	85	19	89	19	89	9 7	4 8	?
	0000		26	8	98	<b></b>	8	87	87	81	82	9/	72	69	89		89	29	29	3	8	88	75	75	28	65	%	0/	2	29	63	29	4 :	£ 2	5 3	62	09	64	જ	5	69	71	69	7.1	19	=	7,
١	7300		94	8	87	\$	8	8	98	82	84	11	74	70	70	18	17	69	26	8	87	87	76	76	63	63	19	71	57	69	65	65	51	7 3	99	26	63	99	67	3	2	72	71	72	69	× ;	ŧ]
	2000	2000	94	8	88	88	8	8	98	82	85	78	75	11	71	82	72	71	23	5	87	98	76	92	29	29	150	72	19	69	99	99	55	ς Ş	62	99	65	89	8	99	72	74	71	74	2 2	6 1	
	4000	200	-	-	-+	-1	$\dashv$	$\dashv$	-		-	-	80		-	-	$\dashv$	-	-	┵	8			-	-	જ	-	_	62	-	89		-	2 5	┰	$\vdash$	Н	$\vdash$	-		-	79	-	$\dashv$	-	<b>≈</b> ‡	-
	00 2150	215	94	$\dashv$	90	-+		-	$\dashv$	_	Н	<u> </u>	2 78	-		-	$\dashv$	-	2	-	87	-	28	$\dashv$		75	-	{			9	-	+	3 6	+	+-	$\vdash$	Н	2 72	-	-	$\vdash$	6 75	$\dashv$	+	8 8	`   
	0026 0000	00	95 95	$\dashv$	94	-	$\dashv$	-	-	$\dashv$		_	86 82		-	-	-		$\dashv$	$\dashv$	$\dashv$	$\dashv$			-		-	-	$\dashv$		$\dashv$	-+	73 70	+	17 17	┼	Н	Н	72 72	-		79 8	-		+	78 80	
	02 0021	000	93 9	-		$\dashv$	+		-		Н	-	77 8	Н	$\dashv$	-{			-	$\dashv$					$\dashv$	-		-	-	76 7		-+	-+	+	717	╄	Н	┥	-	-1	$\dashv$	79 7	-	-	-+	08 6	<u> </u>
	1350 17			25	$\dashv$	+	-			-	Н	$\vdash$	. 82	-		-1	<del>-</del>	$\dashv$	-+	-+	$\dashv$	$\dashv$	-	$\dashv$	$\dashv$	82			-		$\dashv$	+	+	7 6	+	92	Н	┥	$\dashv$	$\dashv$	-	79		$\vdash$	+	2 2	<u>,</u>
	1000		93	96	96	8	8	£	84	83	16	98	84	73	71	83	73	74	92	8	68	68	78	77	88	88	83	26	83	7,4	73	2	6 2	2 5	;   <u>-</u>	89	29	69	2	99	73	74	73	74	89 1	F   6	e !
	900	000	$\vdash$	8	66	8	8	8	84	_		_	98	$\vdash$	20						89	_	-	-	95	-	93	-	_	76	-		-+	3 8		+	29	Н	{				74	-	69		
	067 002				_	∸	-		82 84		-	_	92 92	$\vdash$							88 88	85 87		_	_	84 89	_	$\dashv$	81 85	-				87	1 2 2	-	20 69	Н	68 70	99	_	Н	71 72	$\vdash$	99	73 75	<u>وا</u>
	21001212		65	93	8	5	93	82	80	74	87	83	80	70	69	85	64	\$	8	8	82	98	9/	75	85	82	82	88	79	65	42	2	æ [	æ [	ર જી	99	9	9	29	63	72	72	-	Н	2 8	_	0
	Hz)	316	95 97	_		_	$\rightarrow$	-	89 85	81 75	85 87	_	84 80	Н	$\dashv$	82		_	~	-	-		85 78				102 89	$\rightarrow$	102 88	$\rightarrow$	09 29	_	-+	2 5	2 4	+	72 68	H		68 64	73 69	-	_	⊢⊣		79 74	2/8/
	enter Frequencies (Hz)	7 700	100	25	5 95	8		-	93				68 5	-		2 87	7	77	8	107	8	94	88	87	26	6	66 /	_		78	69	_	-	3 2	5 4	57	17.	7.3	7 74	1/ 1	08	╌	Н	3 82	-	98	2
	Freque	01 C71	91 99	105 115	105	=	-	-	16 88		101 111		96 105	80 82	78 81	_	78 80		87						_	82 88	_	_	_	_		75 70	-+	82	0, 87	+	76 73	79 7	80 7.		-		80 81	82 83	79 78	88 8	88 88
	7 T		$\vdash$				$\rightarrow$	_			-		-		_	_	_	-	_	_		_	_	-		_	$\overline{}$		-		9 79	-		76 78		+	-	-	$\vdash$	-	80 81	-	$\vdash$	_	77 79		_
	ctrum	0)		83 87			68 68		88 48	_		9/	72 76	80	78 80		77	76	81 79		82 89	8 28	84 87	84 8			82 92	79 8	11 1	80 82	78 79				v 5		77 7	79	08		80	81	81	82	75 7	\$	84 2
	ave Sp	U 3U	89 89		-		-	$\rightarrow$	_	83 85	75 78		68 70		73 76		72 74	_	82 84		84 85		79 82	82	-	78 78	-	75 78	73 75	_	-	-	-	71 73	0/ 0/	-	73 75	-	75 78		75 77	76 78	77 79	_		% 28 28 38 38 38 38 38 38 38 38 38 38 38 38 38	78 81
	1/3 Oct	76	68	81	83		22	78	18	18	74	17	19	73	72	72	70	2	81	79	81	83	11	78	82	8/	69	70	10	72	69	69	67	8 6	5 2	2	5	70	71	19	73	74	75	9/	19	7	74
	dB) at	C7 03		_	_	-		75 76	_	75 78	73 72	69 59	56 62	_	69 65		65 66		_	-	80 82			65 76	74 79	62 69	73 69	11 19	69 99		65 70	_	$\rightarrow$	_	8 3	_	2 2	_	11 99	51 63	69 89	67 73	20 02		60 64	69 75	
	Band SEL (dB) at 1/3 Octave Spectrum C	00 00 00 00 00 00 00 00 00 00 00	83	78	81	8	75	29	74	69	73	B	9	99	99	29	57	28	81	78	11	08	0/	0/	75	15	69	19	79	64	19	62	88	કું	5 5	39		19	62	28	63	2	_	49	28	99	8
İ	Banc	CI NI	83 75	_		-	$\overline{}$	-	-	54 69	67 75	57 62	54 54	51 50	50 50		52 50		82 84	_	72 66		28 85	_	64 71	09 09	-	52 49	53 53	57 53	56 53	_	53 48		2 2		5	64 51	51	15	62 63	-			47 50		
Ì		ros.	Base		$\overline{}$	$\dashv$				_	Cavity		<del>-</del>	-	$\vdash$	-	Base		-				Base	-	Cavity	Cavity	Cavity	Base	Cavity	_			Cavity	_	Dase	+	10	Base	Base	Base	Base	Base	Base		_	Base	_
ŀ		<b>−∄</b>										١.			П								-	-	<u> </u>						H				十	+	+	f	_	-	5.5	$\vdash$	5.5	$\vdash$	H	+	-
Ļ		. Lime	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled.	Post-fled.	7:1	11.7	11.7	7	7.1	7.1	2	2	2	<u></u>	Ц	$\dashv$	4
ļ	RCW	Kesp.	ď	P.	<u>a</u>	ď	ď	Ъ	Δ.	<u> </u>	<u> </u>	<u> </u>	_	<u></u>	ď	Ь	Ь	Ь	d.	d	ď	_		_		_	_		_		۵	Ь			7	1 2	2	7	2	2	7	2	7	7	0	0	
	Event	(m)	15.2	15.2	15.2	30.5	30.5	30.5	30.5	19	19	91.5	91.5	91.5	91.5	122	122	122	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	19	19	91.5	91.5	122	122	122	122	2   2	122	122	15.2	15.2	15.2	19	19	19	19	19	19	19
	Event	lype	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	So cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
ŀ	Date		12/9	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	12/9	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	12/9	6/21	12/9	6/21	6/21	6/21	4/28	4/28	4/28	5/26	5/26	5/26	5/27	5/27	5/27	5727	4/19	4/19	4/16
ł	Co.		163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	163	176	13/2	176	176	176	176	176	176	176	176	19	194	194

Calc.	Overall	94.7	7.06	92.9	98.1	94.0	0.60	100.9	6 101	93.6	105.8	105.7	108.0	116.6	116.5	118.6	116.7	116.7	1011	104.0	103.8	106.7		114.8	8.111	55.7	100.6	105.5	110.8	103.0	116.9	107.1	105.0	102.8	8.96	7.66	93.7	91.6	90.4	92.7	105.8	CCII
-	<u>50000</u>	+	215	╁	09	$\dashv$	4 7	+	5 69	+	+-	╀	79 1	$\dashv$	-+	+	+	+	+	╁	╁	+	81	-	₩	-	+	52	$\vdash$	$\dashv$	-	£ 5	+	+	57	53	43	20	84	46	83	3 :
	16000 20	+	╁	19	Н	9 9	+	+	╁	╁	: E	┼-	Н		$\dashv$	$\dashv$	-	+	+	+	╀	+	+	┼-	74	+	┿	+	Н	-	+	+	3 3	十	+	+	42	Н	7	47	98 98	
		+-	+-		Н	+	+	+	+-	╀	+	83	-	$\dashv$	$\dashv$	+	+	3 7	╬	+	74	+	87 8	├-	$\dashv$	+	+	99	Н		+	+	╁	╀	╁	╁	-	19	-	$\dashv$	88 5	+
	12500	-	┿	65	$\vdash$	+	+	+	+	╁	+	╀╌	Н	Н	$\dashv$	$\dashv$	+	+	+	+	+	╁	+	⊢	╀	+	+	+	Н	$\vdash$	+	+	+	+	+	╀	$\vdash$	Н		$\dashv$	+	+
	8000 10000	_	+	88		1	4 /2	4	-	+	+	84	Н		26	4	4	3   3	+	+	+	. 6	+	╀	72	+	_	1		$\vdash$	+	+	+	+	+	-	┝	Н	_	3 54	$\dashv$	
			+	╫	$\vdash$	69	+	+	+	+	+	8	H	$\vdash$	+	$\dashv$	$\dashv$	5 5	+	+	╫	\$ 8	╁	╁	75	+	+	╁┈	-	$\vdash$	$\dashv$	+	+	+	+	+	┝	Н		8 58	+	+
	6300	75	_	╄	Ц	72	4	4	4	╀	+	┿	Н	80		-	4	76	+	+	+	+	+	╄	$\vdash$	-	- -	19	-	$\vdash$	-		4	+	12/2	+	-	70	$\dashv$	89	+	+
	0 2000	77		+	-	72	-		+-	+	+-	+-	$\vdash$	$\vdash$	-	-	-	-	-	+	+	┿	+-	⊢	78		┰	+	-	$\vdash$	+	-	+-	+	73	╁	╁	Н	$\dashv$	┝╌┼	8 8	+
	4000	+	+	+-	╌	75	+	+		┿	+-	+-	+	Н	$\dashv$	1	-	+	+	+	+	+-	+-	┼-	7 81	+		+-	┢	Н	-+	+		┿	╁	╁	╀	Н		Н	26 8	+
	00 3150		-	╫	-	5 75	+	+		+		8	<del> </del>	Н	$\dashv$			6 6	+	+	+	3   2	+	╁╌	+	8 4	-		⊢	-	-	-	5 27	+	+	+	⊬		-	$\vdash$	-	° ò
	00 2500	+	_	-	-	5 75	-	+	4-	+	+-	8 2	<del> </del>	Н	┥		-+	-+	+		+	+	+-	+-	+	+		73 7	⊢	Н	-+	-+	+	┿	+-	╁		Н		$\vdash$	$\dashv$	°
	1600 2000	77	+-		-	76 75		-	+-		+	+-	+	╌	Н		-+	$\dashv$	+	-+-		┰	+	╀	87 8	+	0 2	-	├	$\vdash$	$\rightarrow$	68		+	+	+-	╄	Н	Ь.	Н	+	2
	1250 16	-	-		⊦	77 77	-	-	+	+	-	+	$\vdash$		Н	-	-	-+	-	+		╌	+-	+	╀┤		-	81	┼		$\dashv$	$\dashv$	—	+	+-	╫	+	74	Н	69	-	~ %
	1000 12	+	+	74 7	╁╌	Н	$\dashv$	+	70 68	+	+	┿	+	⊢	$\vdash$	$\dashv$	$\dashv$	+	+	+	+	+	2 6	╁	H	$\dashv$	+-	8 8	╁	Н		-	+	╁	+	+	╁	Н	-	Н	68	+
	800 10	4	717	+	ļ	$\vdash$	$\dashv$	4	82 8	4	2 2	┸	88		Ш	94	_	88	4	4	\$ 2	+	+	+	$\perp$	25 5	×   &	+	<del> </del>	<u> </u>	_	4	8 5			$\perp$	┸.	72	_	Ы		2
	630		5 69	+	+	$\vdash$	-		2 8	7 5	± 8	8 8	8	95	95	97	2	8	3 3	\$ 8	3 8	3 8	2, 56	8	86	102	5 2	9 16	96	83	94	16	<b>%</b> 5	2 8	8 8	29	9	73	0/	28	8	ç
	005 00		1 / 4	+-	┿	<del>  </del>	-	28 5		-	+	89 92	94	_	102 87		-	98	-			2 6	-	+		-+	8 8	┯	+	₩	${}$	$\rightarrow$	85 86		8 8	79 27	70 65	-	76 71	72 66		20,28
	315 46		5 8	+	76 73	╌	<del>-</del>	-+	8 8	+	-		+	92 10	-			-	┰		2 2	-	_	102	-		23 8	+-	92	┰	<u>e</u>	$\dashv$	-		7 8	+-	+	+-		80 7	35	2
s (Hz)	100 125 160 200 250 315 400	$\boldsymbol{-}$	8 4		┰			-	-	7 6	+	+	+-	+	-	4 95	-	-	-+	$\rightarrow$		2 2		_		+	\$ 6 \$ 6	+	107 108	95 95			+	+	74 79	-	+-	+-	84 84	-	-	112 95
enter Frequencies (Hz)	160 20	_	8 8	2 48 8 8	89 87		_	-	-	2, 20	+		-	1000		_			- 1	-	-+	2 2	_	2 20	_		8 8	+	1	-	1	$\vdash$	66		7,	+	-	+	8 62	-		106
ır Freq	125	2	à 8	8 8	8	8	5	25	2 2	2 2	S S	3 8	95	911	116	118	116	116	911	8 8		_	3 8	2 2	94		_	$\rightarrow$	-	+	-	$\rightarrow$			/8			18	_	-	16 6	-
7.			8 8 8 8	-	+	++	-	_	S 5	-	S S	-	94 95	89	90 101				$\neg$	_	_	$\neg$	2 6	$\neg$	86 87		80 82		Т.	_		- 1	—†~	_+:	0. S	\ \	. —	6	75 7	77 80	_	89 9
ectrum	63 80	8	£ 8	° 28	8	82	88	87	‰ °	8 8	2 8	<u>ه</u> ه	22	8	98	88	28	98	8	<b>8</b>	æ 8	æ [8	<u>ئ</u> 8	Ĭ.	85	16	5 8	g 92	82	16	88	8	8	5 S	ءَ ۾	<u> 2</u>	5	9/		-	ಜ	8
Band SEL (dB) at 1/3 Octave Spectrum C	10 50	}-	25 27	_	-	+	-	-+	-		C 8	—	-	84 85	-	88 87	_	-	_	-+		-	% % % %	-		_	74 77	_		-	87 87	-	_	_	S 8	0 0		+-	72 73	72 75		78 77
1/3 Oct	10 13 16 20 25 32 40	_	4 E	3 5	-	-	2	ଛ :	<b>≅</b> ₹	<u> </u>	2 6	è &	8	8	-	84 8	_	_	8	84	8	2 2	8 8			16	7.	۶ ۲	· 8	84	84	82	<b>2</b>	<b>3</b>	80	0 %	2 8	2	5	9	98	73
1B) at 1	0 25	_	4/ 4		-	-				-	0/ 79		_	-	84 77	85 79	83 79			$\rightarrow$	-	8/	1	000	+	$\vdash$	69 2	69 72	-	-	78 78	+ +	-		+	2 2		+	+-	+-	-	73 75
SEL (d	16 2		19 63		+	-	-	-	$\overline{}$	-+	-+	6 2	77	76 8	-	73 8	-	_	_	$\rightarrow$	-+	69	_	00	_			60 89	_	-	-			-	_	80	_	_		8	26	81
Band	13	-	S 2	7 2	85	54	$\rightarrow$	$\rightarrow$	_	7	3 5	0 47		78	-	4 77	77 2	_			_	63					-	70 0	-	+	-	-	_	$\rightarrow$	-	2 28		-	+	-	_	1 70
<b>L</b>		· F	e 57	_	+-	+	$\vdash$	┪	_	+	ج ا ج	十	+-	+-	+	ity 84	ity 82	Н	$\neg$	$\dashv$	-	_	% S	+		Cavity	0 F	9 9 £. g	+	+-	ity 66	+-1		-	-+	S :	_	+-	1	+	-	ity 71
Mik	Pos.	<u></u>	Base	Base	Base	Base	Base	Base	Base	Base	Base	Pase Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Base	Dasc	Cavity	Ű		Pase Cavity	Cavity	Base	Cavity	Base	Cavity	Cavity	Base	Pase	Cavity	Base	Base	Cavity	Base	Cavity
Rec,	Time	(min)									-	ed led	led.	ē	led.	led.	led.	Jed.	Jed.	Ed.	eg.	ا اق	i ke	<u>.</u>	<u>s</u>	ive	ž.	ءِ اج	<u>ءِ ا</u> ۽	<u>.</u>	i.e	led.	Jed.	fled.	led.	fled.	led.	i ed	g	Jed I	fled.	fled.
<u> </u>		1		5 0	,	0	0	0		-		Post-fled.	Post-fled	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled.	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.
RCW			7	15	1	╁	Н	$\vdash$	$\dashv$	$\dashv$	4	+	+	╀	-	+	$\vdash$	-	Н	$ \cdot $	-	-	+	+	+	$\vdash$	H	+	+	+	+	-	H	$\parallel$	$\dashv$	+	+	+	+	+		-
Event	Dist.	Œ	ع ا	2 2	5   5	19	30.5	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	30.5	15.2	7.51	15.2	15.2	30.5	30.5	20.5	3 3	5   59	15.2	15.2	30.5	30.5	<u>s</u>	٥	9 5	122	122	15.2	15.2
1		$\neg$	-j-	- E	So cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	- F	.50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	50 cal.	50 cal.	.50 cal.	SU cal.	.50 cal.	50 cal.	.50 cal.	.50 cal.	So cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	50 cal.	.30 cal.	.50 cal.	.50 cal.
Event	Туре	. ]	န္တါ	န္တါန	३।इ	3   2	S	l & l	នា	ଝା	%।	ير اير در اير	ب ا د	110	! ! ~ ,																		. 1	. 1		- 1						1
Date Event		-	+	4/19 .50 cal.	+	+	4/28 .50	Н	-	$\dashv$	$\dashv$	+	C: 07/C	╁	+	╀	╁	+	5/26	H	Н	$\dashv$	$\dashv$	十	5/11	+	Н	2/11			11/5	21/9	21/9	21/9	21/9	21/9	6/17	71/9	+	+	╁	21/9

3   3	Calt.	SEL	99.3	93.4	107.3	105.6	89.7	86.1	100.2	85.7	85.3	85.7	84.5	85.3	85.2	82.5	85.8	85.9	86.2	85.6	85.3	85.8	86.7	106.1	84.8	84.5	84.9	9.98	102.4	106.2	112.0	112.3	27.56	98.1	101.2	113.0	113.0	115.3	104.4	105.3	85.6	106.5	110.3	108.8	88.1	87.6	94.9
	20000		89	25	5	4	45	47	46	43						1	42	5	45	42	43	42	£	37		27	28		34	38	4	£	g	88	19	52	20	29	8	98	30	37	52	47		7	25
	16000		71	8	2	<del>ئ</del>	69	46	44	45	41	39	39	9	우 :	<u>۳</u>	4	4	47	5	47	<del>2</del>	9	42	37	36	39	42	36	42	47	5 ;	¥ 2	, 9	69	26	55	65	68	8	43	4	8	54	9	\$	\$
	12500 1		74	63	28	22	55	49	46	51	45	44	43	£	4	5	<del>2</del>	<del>\$</del>	23	22	51	8	2	4	41	9	45	46	40	45	15	23	3 8	8 2	73	65	59	89	<u>-</u> 6	8	49	49	65	99	24	25	88
	100001		9,	53	8	<u>¥</u>	<u>ئ</u>	72	48	99	52	22	51	22	15	<u>ا</u>	2	<u>ت</u>	29	57	99	<u>2</u>	<u>8</u>	92	20	20	54	99	43	50	2	وار	2 3	33 62	75	62	62	=	22	8	- 99	53	29	63	8 	8 8	2
	8000 10		. 62		4		4	_	54	ш	Ш	_			-	-	4			$\dashv$	_	4	_	_	_	_	_	Ш		99	$\dashv$	4	+	+	↓_	_	$\vdash$	4	-				4	65	63	8 8	2
	6300   8		08	-	69	$\dashv$	+	-	-	_	Н	H	Н	$\dashv$	$\dashv$	$\dashv$	+	$\dashv$	$\dashv$	$\dashv$	-	$\dashv$	$\dashv$	$\dashv$	-	$\dashv$		Н		55	$\dashv$	+	╁	+	8/	-	Н	92	-		-	-		69	65	2 ;	2
	2000		08	23	19	8	67	62	09	65	09	19	09	19	9	27	\$	8	29	19	65	99	3	53	62	62	63	65	15	57	\$	9 8	7/ 52	192	62	17	70	6	96	16	99	19	25	75	29	9 2	2
	4000 5		84	2	75	-	5	65	89	99	19	63	19	79	5	8	9	2	29	89	89	89	99	2	65	49	99	- 62	20	57	89	3 8	2/2	2 92	62	73	73	8	8	8	29	29	=	11	89	88	2
	3150		83	28	75	92	7	-62	29	-62	64	63	19	63	63	ξ, ξ	8	99	17	89	71	19	69	28	99	99	99	89	99	62	17	=	2 2	78	<u>-</u> 8	75	75	8	16	91	89	72	11	76	89	69	<u>''</u>
	2500		82	78	76	78	71	67	69	89	63	99	62	B	63	19	99	63	2	69	70	89	89	29	89	63	29	69	22	62	73	4	5 2	5	≅	78	79	83	16	8	69	74	78	8	2	2 8	2
١	2000		84	_			-	_	69	Н	Н	⊢	62	$\dashv$	<u>a</u>	ᅪ	8		$\dashv$	$\dashv$		$\dashv$	$\dashv$	$\dashv$	_	-		69	-	Н	$\dashv$	-+	+		┿	⊢	Н	$\dashv$	$\dashv$	-	_	-	-		-	8 1	-
	1600		83	$\dashv$	-		72		19 (		H		-		$\dashv$	+	-			89 /			-	-	Щ	89 8		Н	<u> </u>	-	$\dashv$	8 :	+	+	╄	⊢	Н	┥	98 9		_	-		$\vdash$	-+	2 3	
	0 1250		81			-	$\dashv$	_		_	Н	H	19	-	-+	+	+	$\dashv$	$\dashv$	-	_	$\dashv$	-	$\dashv$	-	89	-	$\vdash$	<u> </u>	69	$\vdash$	+	+	2 8	┿	├-	Н	┥	98			-		2 84	$\dashv$	8	$\dashv$
	0 1000										L				L				_											81 82			$\perp$		1_	<u> </u>		_				7 81		5 82	_	89 19	
	630 800		79 7	_	_	_	-		_		_	_	_	_	20	-+			<u>4</u>		9 9		$\overline{}$	_			_	_	_	77 8	_	94 9	_	2 8	_	╄	-		_	8 8			_	8 99		9 19	
Ī	200		83 83		83 84	-+	—	_	8 78			┡	-	-		$\rightarrow$	-	-	-	-	_	-		83 80		_	68 64		9 75	83 81	-	98 98	6 72	2 8	+	89 87	89 87	$\overline{}$	-	_	19 89	-	73 76	┝╾┥		70 68	2
	315 400		8 98		87	_			81 7		-	-	-	-	$\rightarrow$	-	_	-+					71	68	69 7		$\vdash$	-	87	16	93 8	-	81 2	-	+	95 8	_	_	-	91   9	11	11	13	80		73 7	
(11)	125 160 200 250		94 88	_	106 92		82 75	_	98 6	-	-	_	-	-	-	-+	78 77	-	_		77 75	-	$\overline{}$	99 105	77 72	_	_	80 74			104	절 글 [3	-+-	60 60		102 112	103 112	108		94 94	72 74	33 82	98 86	98 86	77 77	76 77	85 87
Processing (III)	160 2/												:	92	92	4	9	25	26	75	74	75	9/	88		92	75	11	85	68	76	25	8 8	8 8	16	88	87	26	93	6   6	. 82	106	110	108	81	80	8
100	100 125		98 98				_		$\blacksquare$	-	2 2	_	_		76 78	_	-+	_	-	76 75		9/ 9/		_					_	82 87		_		_	-	-	-	_	84 87	68 98	77 27	82 91	_	84 93	-	77 79	84 85
Š		3	98	82	81	81	-	75 7	77	192	73 7	74 7	73 7	_	-	$\rightarrow$	_	-	75 7	72	75 7	76 7	77 7	76 7	74 7	73 7	75 7	77 7	76 7	80	8	8	88	3 %	88	8	6/	98	8   88	88	75	126	28	78	92	9/	22
	sopecific	;		78 80		75 79	75 78	72 76	72 76	72 74	02 29	69 73	99	69 72	_	$\rightarrow$	-	$\dashv$	72 75	72 74	71 74	72 75	73 74	71   73	70 73	69 73	71 73	73 74	71 72	75 76		_	80 83	_	-	78 77	77 77	85 86	86 87	88	72 74	71 73	75 78	74 77	74 77	_	81 81
	40 4		80	74	92	72	73	71	100	69	64	29	63	67	ŝ	ङ	69	69	69	69	69	69	10	70	69	69	69	20	69	73	78	71	<u>ئ</u>	ý Š	82	77	78	06	98	87	70	89	72	72	73	72	77
9,5	13   16   20   25   37   40   50   63   80		75 78	70 73	73 75	68	69 71	99	69 99	89 59	54 62	65 67	51 59	62 65	$\rightarrow$	-	-		99 19	62 65	62 65	99   69	64   66	65 67	99 69	99 29	99 59	99 99	64 67	68 70	-	-	-	00 27	-	76 76	27 77	06 16	84 84	80 87	69 59	64 68	11 29	11	02 29		74 74
á	) (ab)		69	62	69	19	89	09	2	19	25	54	52	53	26		23	59	62	09	19	79	19	09	62	99	63	ક	79	65	8	≅	2 5	8 3	3 2	74	79	94	81	98	62	63	89	99	. 65	29	89
201	10 13 16	2	61 72	53 66	62 70	60 63	51 64	54 62	64 66	53 52	35	99	22	47 60	28		-	-	51 54	45   55	50   55	48 55	48 57	62	89	57	57	9	57	99	68 77	11 19	19	2 2	-	50 78	70 78	95 94	68 77	74 80	47 56	56 57	51 59	56 61		53 61	99
٤	10		53	51	29	22	46	54	19	46	9	57	   	53	_	26	_	4	46	33	20	38	48	53	53	54	22	29	È	22	75	-	_	2 %	8	69		92	73	8	59	, 47	Ţ,		$\overline{}$	22	g g
	MIC	. (0	Base	Base	Cavity	Cavity	Base	Base	Cavity	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Cavity	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base
	Kec, Time	mit (min)	d.	d.	Ġ.	d.	d.	d.	ė.	5.0														òd.	Ġ.	ž.	ä	8	ă	'n.	Ġ.	j.	-j	9 3	;	ē.	j.	g.	ģ.		ē.	ed.	ed.	ed.	ed.	ed.	-gg
L			Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	_	H	$\vdash$	┝	H	$\dashv$	$\dashv$			_	H	-	-		Post-fled.	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled.	Post-fled	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled.	Post-fled.
r	RCW Desn							_		2	F	F	F		$\exists$	$\exists$	_	_		L	L	F		_			-		-	╀		-	+	+	+	+	+	$\vdash$	_	$\vdash$	-	├				H	$\dashv$
,	Event	Ē	30.5	19	61	91.5	91.5	122	122	19	122	122	122	122	122	122	91.5	91.5	91.5	91.5	91.5	91.5	91.5	122	122	122	91.5	91.5	91.5	91.5	19	19	<del>1</del> 9	30.5	30.5	30.5	30.5	15.2	15.2	15.2	122	122	91.5	91.5	91.5	91.5	19
	Event	adkı	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
	Date		6/17	21/9	6/17	21/9	6/17	6/17	6/17	4/22	4/26	4/26	4/26	4/26	4/26	4/26	4/29	4/29	4/29	4/29	4/29	4/29	4/29	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	2/9	2/0	2/9	279	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	6/2	2/9
⊦	5		201	201	201	201	201	201	201	202	205	205	205	205	202	205	205	205	202	205	202	202	205	202	202	205	205	205	205	205	202	202	205	503	3 6	Ş	205	205	205	205	205	205	205	205	205	202	205

Calc.	Overall	SEL	1.4.1	110.8	118.1	102.7	8.601	119.9	103.2	6.96	103.2	104 6	103.4	107.0	118.2	118.0	102.5	93.6	11.0	103.0	85.2	103.6	108.2	110.4	103.1	94.6	104.8	100.7	88.7	6'101	103.5	102.2	103.7	102.4	106.8	102.4	100.9	107.1	107.0	0.57	97.2	7.00	97.6	101.7	103.3	105.6	
	20000	7	£ [	7 5	3 3	17	25	72	26	57	; E	9	3 5	÷ 8	3 12	2 9	75	5.4	6	14	44	×2	9	3 5	: 8	65	94	43	51	74	78	73	78	75	38	2	10	50	5 2	9	5	3 8	S 8	; <del>  4</del>	9	48	
	16000	- e	8 5	3 8	3 8	77	95	92	8	29	1 8	3 8	3 2	5 0	;   p	) <u> </u>	2	; \ <del>z</del>	22	64	40	) S	₹ 5	3 2	2 2	જ	64	41	57	62	82	77	82	5	2 2	3 3	8 3	5 4	3 8	3 5	ر د	3 2	5 9	; E	S	88	
	12500 1	+	3 8	6 5	3 2	   @	96	8	9	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1 8	1 8	2 8	8 8	,   	75 25	:   &	3 4	1 %	14	: 5	3 8	2   2	3 8	3 8	8	55	44	19	82	83	- 62	82		99	63	8 5	3 9	6 8	3 8	70 9	5 8	3 2	3 3	5 2	   	;
		+	+	+	23 52	╄	┞	╀	╀	╀	┿	╀	+	+	+	+	╀	╬	+	╀	+	╁	+	╁	£ 26	+	9	├	-		98	81	98	<u>Ω</u>	<del> </del>   88	2 3	6 6	4	-   9	) ¥	3 5	3 8	5 5	3 8	9 65		-
	00001	+	+	+	75 7	+-	╀	╀	╀	+	4	╀	+	5 2	+		╀	+	╌	╀	+	-	+	╁	┿	+	59	$\vdash$	-	-	Н		Н	$\dashv$	4	-	2 5	+	+	+	+	2 5	+	2 5	+	3 2	$\dashv$
	0008 00	+	+		╁	╁	╁	╁	╁	╁	+	78 7	+	+	+	2 8	十	+	十	+	, 9	+	+	+	2 6	+	99	╁	╁╌	85 8	Н	84 8	$\dashv$	-	$\dashv$	9 :	+	0 1/2	+	5 6	+	╁	+	+	+	8 89	┨
	00 900	+	+	4	80	+	╀	╀	1	+	╀	+	4	6 G	+	+	+	+	+	+	+	- -	+	+		+	9 02	Ļ	╀-	<u> </u>	_		85 8	_	-	+	+	4	-	+	4	4	4	2 5	1	92	4
	4000 2000	+	+	2 2	82 82	+-	╁	87 8	╁	+-	+-	20 20	+	+	+	-	+	+	+-	┿	+	) o	+	+	9 9	╫	+	⊢	╄	├	-	├-	8 98	-	$\dashv$	-	-+	+	+	┿	+	2 2	+	+	╌	3 89	$\dashv$
	3150 40	-+-	9 1	-	+	98	╀	┿	╀	┿	+-	+	+	╁	+	+		┿	+-	+	┿	+	+	+	8 8	╫	+	╀	+-	├	┥	H	85	-	$\dashv$	$\dashv$	-+-	╅	+	┰	0 5	╫	+	0 2	. S	3 8	3
	2500 31	+	+	28 83	+	╁	╁	8	+	╅	╁	╬	3   2	+	7, 50	+	+	┿	+	┿	┿	┿	+	┿	£ &	+-	+	╀	┼	├-	<del>   </del>	-	98	-	-	73	┰	0 2	┿	+	C E	:	2 5	: 8	8 8	\$	-
	2000 2	+	+	8 2	+	88	╀	╀	+	┿	+	+-	+	7 8	+	+	+	+	+	+	╌	5 8	+	+	70 6	+	+-	╄	┿	┿	-	-	87	$\vdash$		$\dashv$	+	£ 5	2 5	2 1	C %	0 8	2 8	\$ 5	7,5	2 12	7
	1600 2	+	ᅪ	2 8	2 8	2 2	16	:   2	, \ <u>%</u>	3 5	2 2	3   3	3 8	2 2	7 2	3 2	2 8	3 5	1 2	5 8	3 9	6 8	8   8	2 2	5 8	₹   %	92	92	74	82	83	83	84	82	5	92	2 6	2 8	2 6	0 2	9 8	2 8	2 8	6 5	7 4	1 7	2
	1250 1		74	8 8	6 8	, 18 18	S	3 6	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	5 %	2 5	3 8	3 8	2 8	8 8	3 8	7 5	3 6	1 8	3 5	:   9	3 6	٥	3 8	6 6	3 2	2	75	73	82	88	84	85	83	83	8	<b>25</b>	2	\$ 8	S	Ç [	2 8	⊋ [8	8 5	/ 82	9	,
	1000	1	2	24	နှင့်	2 8	2	3 8	2 8	8 8	0 2	3   2	\$   S	£ 8	2 8	8 8	2 2	\$ F	- 8	3 6	7 8	8 8	١	8 8	8 8	3 8	3 ∞	92	17	83	8	82	83	82	85	128	8	<u>د</u> ا	\$ 3	ž č	C 8	æ [	× [	8/2	٥ ا	£   S	6
	008		74	8 8	3 5	1 %	S	्रेट	3 8		-+-	7 6	\$ 8	_	-	2 2	-	2 7	t	+	+	-	-	3 3	¥ 8		+-	74	72	<u>~</u>	+	82	$\vdash$	$\vdash$			$\rightarrow$	-	-	2 2	2 :	۱ ۲	- 1		70 78	+	-
	500 630	-+	-+		8 00	+	+-	+=	-	20 27	+		+	-	2   2 2   3	_	_+	84 80	C 00		-	-+	-	_	2 2	-		+-	69	85 85	+-	84 85	-		-	82 82		$\rightarrow$	68	-	9 2	۹ (۶ ارج	74 79	7/ 6	2 2 2 2		⊣
	400 50		$\rightarrow$	20	-	┿	┿	+	-+-	+	+		-	-		2 2	-	-	0/	+	-	-+-	-	-	7 2	-	7 8	+-	+-	+-	+	68	+	-	-	$\dashv$	-+	-+	-	-	-+	2	22 8	-+	S 5	+	4
٦	315			98	+	+-	+-		+	+	-	-+	+	-+	=+	-	-+-	+	6/ 6	-	-	-	٠.	-	99 99	-+-	<del></del>	-	+	╫	+-	2 90	┿	2 90	_		$\dashv$	-+	-+	-	-+-	-	$\rightarrow$	-+	8 8	-	ᅴ
enter Frequencies (Hz)	100 125 160 200 250 315		-	8	86 2	-	20 00		_	-		-	+	-+		_	<del>-</del> -	-	2 2	-	16	-+	+	-	50 20	-+	+	+	+	+	-	96 92	+	96 93	94 91	Н	-	-+	-	-	-	-+	<del></del>	-+	15 6	┿	ᅥ
edneuc	91 9		98	112	0 :	0 70	-		_	8 6	+	-+	+	-+	4		-+	$\boldsymbol{+}$	G :		4	-	-	-	7 2	-	+	+-	1-	┿┈	+	92	+	93	2 103					=	-+	2	-	-	8 6		100 107
ter Fr	00 125	_		37	98 5	3 6			2 2	_	-	-	-	-	_		-	-	2 2	-+	-	-	-	-	S 8	-	+	┿	+	┿	+	+	+	88	90 102	-	-+	-+	$\rightarrow$	-	$\rightarrow$	-	-+	-	96 88	-	91 16
m Cer		$\rightarrow$	82	82	- K	8 8	) E	8	è	3 3		2 3	7 2	<u>چ</u>	26	S 2	5 8	$\rightarrow$	ž (	9 6	<u>ب</u>	٥ ز	<u>و</u>	6/ 5	<b>%</b> 8	2 3	\$ £	3 5	: 8	8	8	8	8	68	83	81	_							_	8 8		
Band SEL (dB) at 1/3 Octave Spectrum C	50 63	_	_		-	2 % 2 %	-	7 20	_	2 2	_	8 8	-	82	-	-	-	-	2 E	-	_	-	-	_	25 28	_	_	+		86			4	98	67 77	72 77	$\rightarrow$	$\rightarrow$	_	_	_		84 85	_		6/ 5/	80   82
ctave 5	40 5	-	_		$\overline{}$	2 8 8 8		-	-	_	-	-	_		_	-	-	-	-	-	-+	-	-	_	-+	7 i				$\overline{}$	-	-	-	85	79	72	80	8		8	%	8	8	٤ ا	75	9 1	77
1/30	33		75		2 26	8 8	_	_	-	_	_		_	_	-	_	-	_		-	-	_				_	65 2	-		-	-	-	<del></del>	1 84	5 81	75 76	-	73 80	$\neg$	-	_			$\overline{}$		72 75	4 78
(dB) a	20 25	$\dashv$	-		70 76	2 2	_	77 29		-	$\boldsymbol{-}$	_	-	$\overline{}$	-+	_	_	_	-	_		63 65		79 78	_	_	_	20 5	-	2 8		+-	-	80	78 7	73 7		-	_		-	_	-	-			73
SEL	10 13 16 20		69	71	77 5	17	: 2	ž 8	2 8	Z i	7	25	4	5	-+	_	-	_	-	_				-	_	_	8 3	-	-		-	_	+	+	69	6	19	75	89	_	_	29 9	_	_		67	
Banc	0 13	-	65	-	-	8/ 03	+	-	-	80	_	-+		-+	-	-	-+		_			+	_	_	-	_		70 9	-		_	_	75 77	72 77	$\vdash$	73	71	72	76 72	89	9	99	-				72 71
<u>ء</u>		.	Base 6	והו	_	-			_		o١	_	-	$\neg$	_		-	_	_	-		_	$\rightarrow$	$\rightarrow$	_	_			Cavity	+	十	+	╅	_	Cavity	Cavity	Cavity	Cavity		Cavity	Base	Base			-	$\rightarrow$	Cavity
Mic		(min)	Ba		Š	T	<u>- ا</u>	-	1	m	-	1	┪		Ba	ق	ريّ	m	B	క	ථි	Ä				H I	m  c	3	3	ă lă			m	M		ర	చ	Ca		ర్							
/ Rec.			Post-fled.	Post-fled.	Post-fled.	Post-fled.	rost-ried.	Post-fled.	Post-fled.		3.3	33	3.3	3.3	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	rost-med.	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive
RCW	Resp.		P.	P	ă	۲	¥   4	<u>بر</u>	ă	0	2	2	2	2	ď	ď	Ā	ď	Ã	ñ.	Á	Ā	Ā	Ā	ď.	Ã	-	1	1	1	1	1	1					L						П		-	
Fvont	Dist.	Ê	19	19	19	30.5	coc	15.2	15.2	61	30.5	30.5	30.5	30.5	15.2	15.2	30.5	30.5	19	19	122	122	15.2	15.2	30.5	30.5	19	ا ة	22	77	2.61	2.51	15.2	15.2	15.2	15.2	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	30.5	30.5
Fyont	Туре	:	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	So cal.	.30 car.	So cal.	SO cal	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cat.	.50 cal.	.50 cal.
Posts	1		H	$\vdash$	6/2	+	+	$\dashv$	6/2	$\dashv$	$\dashv$	-		6/5	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	6/14	11/5	11/6	11/5	11/2	11/5	2/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11
3			205	205	202	205	202	202	205	206	206	506	506	506	506	206	206	206	206	506	206	506	506	206	506	206	506	506	8	500	807	\$07	8 8	802	208	208	808	208	808	208	208	208	708	208	208	208	208

Calc.	Overall	SEL	103.7	2.7	87.0	0.68	8.7	88.0	88.4	6.88	0.68	91.8	95.9	98.3	98.1	67.6	7.76	97.3	97.5	9.90	6.66	99.2	93.1	94.6	6.06	106.5	107.7	111.4	112.4	9.111	111.6	112.0	103.3	103.7	95.4	95.8	93.1	93.7	106.7	107.4	119.5	118.9	9.901	106.4	120.3	118.6	/16
L.,		+	) 20	×	~	~	~	~			34 8	6	6	6	34 9	$\dashv$	32 9	_	_		75 9				_	1 08		1 69		58 1	$\dashv$	28	十	1 2	+	├	H	-	89 1	-	Н	$\dashv$		76 1	+	2 5	-
	00 20000	+	$\dashv$	_	$\frac{1}{2}$		_			_	H		_		Н	-	$\dashv$	-		_		_	_				_	$\dashv$	_	$\dashv$	$\dashv$	+	+	+	+	┝		$\vdash$	H		Н	_		$\dashv$	+	+	
	00091	1	8	9	8	<del>8</del>	42	<del>8</del>	45	43	47	38	40	41	4	43	45	36				_	10	_	62	83		$\vdash$	$\vdash$	$\dashv$	$\dashv$	9 !	+	1	╁	19	-	85	Н	94	Н	69	81	-	+	+	79
	12500	- -	8	8	4	4	4	45	20	51	53	48	20	46	52	49	2	49	46	75	18	72	74	19	99	85	87	76	75	69	2	2 3	Σ   ξ	18	29	99	62	63	93	94	74	73	83	84	25	7	8
	10000	,	8	22	24	8	55	8	58	29	59	48	20	20	54	23	22	23	20	82	83	61	91	13	11	28	88	9/	78	7.7	73	27	2 2	:   &	19	69	99	67	93	95	77	76	82	84	8/	7 3	ŝ
	0008	!	જ	55	28	29	29	29	62	62	63	51	54	55	55	56	58	57	55	84	83	8/	28	72	73	88	89	78	79	75	75	76	ğ 8	3 2	69	71	89	17	93	94	82	79	87	84	82	72	
	6300	,	9	57	19	3	62	62	64	64	65	54	99	23	57	29	59	09	28	82	84	79	28	73	7.5	87	68	83	82	92	26	92	S   2	š	8 2	73	70	72	92	93	83	82	87	85	28	<b>2</b>	7.1
	2000	1	8	59	62	2	4	8	65	99	29	09	19	63	62	64	65	63	63	84	84	78	62	73	9/	88	68	88	83	80	29	79	\$ 2	š	8 8	74	17	73	16	92	84	83	87	85	98	22	2/
	4000	7	6	59	8	જ	65	65	29	89	89	54	99	28	57	59	28	59	28	85	85	79	08	74	11	68	06	83	84	58	84	84	86	3	22	9/	72	75	92	06	88	98	88	87	88	98	5
	3150		8	29	99	99	99	99	69	71	70	25	99	55	99	58	09	57	25	87	85	81	81	9/	8/	68	16	98	86	83	84	88	80 8	3 8	74	78	74	77	91	16	88	87	88	88	88	8	2
		i	2	59	65	63	29	65	70	71	71	99	09	62	62	19	64	63	62	87	84	81	81	8/	8/	68	16	85	98	87	88	68	3 8	3	1/92	76	73	77	68	06	96	88	88	88	2	<u> </u>	2
	2000 2500		75	29	99	67	29	65	69	70	71	09	29	99	29	65	69	69	<i>L</i> 9	87	84	83	18	11	28	88	65	82	88	87	87	88	3 8	9	) 192	77	75	77	88	68	88	87	87	88	8	8	2
	1600		75	28	65	67	99	64	89	69	70	9	99	29	99	99	89	29	29	82	85	82	82	9/	78	68	06	06	06	85	88	98	<b>≋</b>   8	8 8	76	77	76	78	98	98	16	06	82	82	32	2	2
	1250		62	28	65	63	99	64	69	70	71	19	29	19	99	65	89	19	19	8	82	82	8	62	62	68	16	87	87	16	91	16	87	3 8	75	76	75	76	87	98	8	96	98	82	93	8	74
	1000		29	29	2	99	જ	63	99	89	89	89	74	73	74	74	75	74	73	68	85	84	18	8	79	96	06	92	92	87	87	87	£   €	2 6	75	9/	74	75	98	98	92	16	82	98	93	6	22
	800		88	28	8	65	જ	64	99	89	29	73	78	78	-	08	13	8/	11	-	85	87	┡	84	77	88	06	16	-	-		_	88			_	•	_	-	88	-	6	-	_	_	8	72
	500 630	-	-	_	_	66 64			Н	_	-	9 19	71 72	72 72	Н	72 74	73 73	73	71 72	94	84 83	86 83	76 78	81 81	77 77	⊢	93 91	-	-	94 90	-	$\rightarrow$	86 8	-	+	72 75	+	69 72	83 86	83 85		-	83 85		_	103 93	27 17
	400 5	-			$\dashv$	69		9 99	-		99	⊢	<u> </u>	76 7	$\vdash$	ш	75 7	74 7	74 7	6 16	84	85 8	-		0/	94	_	_	_	88	_	88	-+	5 6	+-	89	╌	╄	92	93	-		68	_			88
٦	80 100 125 160 200 250 315 400	$\rightarrow$		19	27	75	74	5 73	171	5 72	5 71	73	⊢	80		18 2	6/ 5	2 2	4 78	92	3 85	84	├	6/ /	├	-	_			₩	-	68	-	6 6	-	+	3 67	+	-	8 92	-	-	9 93	₩	-	$\rightarrow$	78 70
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	00 25	-	93 87	-	$\dashv$	_	-	-	82 74	-	82 76	98	├-	92 86	92 87	⊢	98   86	91 85	91 84	101	88 68	92 82	73 74	89 77	74 68	98 100		109 105	110 106		106 94	-	<del>-</del>	2 2	-	82 75	+-	80 73	99 97	001		-	101	101			84 7
daenc	Z 091				79			81	Н	$\vdash$	╄	88		94	⊢	L	64	93	94	102	98	93	78	_	-	-	_	66				-	8 8	7 2			8	98		94	119	118	76	26	120	118	82
er Fre	0 125	-+		-	$\dashv$	_	3 78			-	+ -	-	-	١.	١.	-	t 90	16	16	1	┢	<u></u>	+	1 74	7 75	<del> </del>	╌	<del> _</del>	<del> </del>		_	_	<u></u>		2 88 2 89	10	+	+	+		94 101		93 95	-		-	82
Cent	80 10		82 86	73 73			_	-	77 78	_	78 78	74 79	77 82	80	79 84	_	79 84	79 84	79	82 8,	98	8	78 80	717	80 7	6 06	91 92	85 90	85 90	88 91	6 88	-	_	_	85 %	-	-	83 87	93 93	93	_	_	94	8	_		82
ectrum	63	_	78	72	75	_	_		-		-	92	74	17	75	75	11	77	77	8	82	26	78	89	92	88	88	88	85	82	82	8	_	8 8	_	-	+-	-		35		85	16	16	-	$\rightarrow$	8
ve Sp	9 20		_		73	74	$\vdash$	3 72	1 75	3 76	4 75	99 /	17	1 73	8 72	9 70	0 73	2 74	2 74	0 81	83	2 7	7 78	1 70	76 79	98	7 87	83 83	3 84	•	85 85	<del>- 1</del>		8 8	28 8	+	74 77	75 78	+-	06 68	98 98	80 85	87 89	68 98	_	_	75 78
3 Octs	32 40	_	76 76	60 55		70 72	68 71	89 99	69 71	71 73	71 74	56 57	69 9	17 69	65 68	63 66	98 70	70 72	70 72	80	84 84	78 77	77 77	72 71	75 7	98	86 87	74 8	78 83	81 83	8 18	-	<del>-</del> +	-	26 7	-	+	+-	+	-	-	-	84	28	-	$\vdash$	
) at 1/	25		73	46	99	_		2	65	-	29		62	99	R	88	65	99	89	82	8	62	74	72	7	77	2	82	83	75	72		-+	_	0/ 1/9		-	+-	+	-	-	-	8	82		1	2
(dB	20	$\rightarrow$		49	_	99	-	5 62	_	2 67	-		+	-	+	58 57	54	<b>2</b>	-	+	83	9	7 75	2 76	65 71	69	76 85	69	2 73	68 75	65 76	-	-	+	1 05	+	-	+	+	85 84		+		76 81	87 85		
and SF	10 13 16		68 67	H	63	19	64	55	53	62	19	9	68	56 53	19	2	5	9	88 60	77 83	75 80	76 76	63 67	71 72	9 19	+	75 7	78 6	74 72	9 19	9			-	-   °	-	-	+-	+-	-		_		_	83	_	$\dashv$
Ä	=	_		55	99	88	55		26			8	_	9	-	57	2	50	_	-	81	85	7	78	99	જ	8	9	9	99	ŝ	72	= 1	3	્ દ	3 5	29	26	74	[	12	72	89	72	-	72	
Mic	Pos.	Œ)	Cavity	Base	Base	Base	Base	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Cavity	Base	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Bace	Base	Base	Base	Base	Cavity	Cavity	Base	Base	Cavity	Cavity	Base
RCW Rec,	Resp. Time	(min)	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	0	0	0	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Post-fled.
Event		(m)	30.5	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	15.2	15.2	30.5	30.5	30.5	30.5	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	30.5	19	19	. 19	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	19
Event	Type		.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	.50 cal.	So cal	.50 cal.	.50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.	S0 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	SO Cal.	50 cal	50 Cal	.50 cal.	S0 cal	.50 cal.	.50 cal	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
Date			5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	\$/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/11	5/13	5/13	5/13	5/13	5/13	5/13	\$/26	\$/26	5/26	\$/26	5/26	5/26	5/26	5/26	5/26	2/26	4730	4/29	4/20	6/3	6/3	6/9	6/3	6/3	6/3	6/3	6/3	6/3
<u>S</u>			208	708	208	208	208	208	308	208	% %	208	80%	208	208	208	208	208	208	٦	=	=	1 =	=	117	218	218	218	218	218	218	218	218	218	218	177	33	33,	227	727	227	227	727	227	227	227	227

Calc.	Overall	3E.L	0.4.0	102	86.2	93.0	89.2	84.4	83.9	89.0	84.8	113.6	114.2	115.7	107.9	108.5	109.9	103.1	105.7	101.6	110.0	110.6	106.0	102.4	6.96	95.2	89.4	108.0	104.2	106.2	1126	109.0	114.1	110.4	102.2	102.6	105.6	110.0	110.0	112.8	104.5	108.5	106.4	105.5	7.76	73.1
	20000	2	1 8	s 4	2 8	84	3	41	41	4	4	65	65	99	æ	Z .	\$  ;	7 8	7.7	7.5	29	8	55	55	51	55	52	84	2 3	S 5	: 1/2	3 3	19	63	62	99	99	26	54	59	53	55	23	:   x	¥ 2	ž
	16000	ę	2 4	3 5	3 4	64	51	46	84	15	84	6	71	73	25	æ	% i	2 8	8	-	29	8	62	26	52	28	36	æ	\$ 8	2 8	3 5	5 29	89	99	89	5	73	58	57	62	22	52	22	2 2	2 2	4,
	12500 1	=	3 3	3 5	1 8	22	57	52	53	88	22	2	74	23	24	g :	<u> </u>	2 2	2	8/	2	17	2	19	22	2	19	8 3	2   2   8	3 8	3 8	99	17	89	72	7	92	63	62	29	49	23	51	22	2 5	ر ک
	100001	+	+	+	+	288	├	╀	╀	╀	-	⊢	9/		-	+	+	+	$\dashv$	+	$\dashv$	_	١		. 2	9	65	2		2 8		5 2	4	7.1	15	74	6	19	29	7	22	26	24	2	;	5
	8000 10	+	+	2 5	+	+	-	╀	<u> </u>	$\vdash$	62 5	┼-	-	$\dashv$	$\dashv$	4	2 3	+	+	-		-	-	_	Н	$\dashv$	89	$\dashv$	S 8	┿	+	+	╄	73		-	$\dashv$	-	$\dashv$	$\dashv$	$\dashv$	-	$\dashv$	-	+	2
	900 80	+	+	+	+	99	╁	+	╀	╁╌	1-	╁	7 67	$\dashv$	$\dashv$	+	+	$\dashv$	$\dashv$	+	-	$\dashv$	89			_	70	$\dashv$	┽	16 8	+	╁	╁╴	$\vdash$		$\dashv$	┥	$\dashv$	$\exists$		$\dashv$	$\dashv$		+	1	2
	2000 63	+	+	0/9	+	+	╀	49	╀	╀	├-	┾	Н	83	$\dashv$	+	2, 8	+	87	-	75	-	72	_	Н	. 22	Н	+	4	2 %	+	+	-	<u> </u>		_	_	_				-	$\dashv$	-	/ 6	2
	4000 50	+	2 8	+	+	9 2	╀	╀	╀	+	$\vdash$	╀	H	85 8		-+	95	+	+		$\dashv$	-	_		-		74	$\dashv$	+	8 8	+	┿	╁	╁				-	74	-	$\dashv$	-+	$\dashv$	+	8 7	=
	150 40	┿	+	S 2	+	+	╀	89	╀	╆	┢	┼	-	$\dashv$	+	$\dashv$	_	+	$\dashv$	-	-	-		_	-	Н	72		+	68 8	┿	+	╫	-	-	=	-1	-	74		-1	69	89	=	2 6	77
	2500 3150	+	3 8	+	╁	╁	╁	+-	╀	╁	╀	8	-	$\dashv$	$\dashv$	+	-+	+	+	87	84	85	80	83	75	62	71	87	\$	×   ×	3 8	78	98	81	78	28	83	92	77	80	64	64	<del>-</del>	Z (	2 6	7/2
	2000		2 3	3 2 3	2 8	3 52	77		12	12	72	2	92	92	8	5	2	3	<u></u>	88	84	87	82	88	13	80	71	8	8	28	3 2	82 8	87	83	78	11	81	28	80	82	65	99	19	5	26	=
	1600	1	\$ 3	1 5 E	) @	92	77	4	2	2	75	16	92	66	5	6	94	8	88	82	8	96	85	82	62	62	72	8	22	28	3 8	8 8	8	85	11	28	82	83	83	98	89	71	65	88	67	=
	1250	Ţ	3 3	<u> </u>	1 09	32	77	73	1	78	74	92	93	95	9	8	92	88	88	85	88	89	84	78	74	79	72	8	88	8 8	6	8 8	88	85	81	18	84	81	84	98	72	92	89	92	3	\$
	1000	Į,	8	S =	- 5	2 2	76	2 2	=	: 5	72	83	92	93	8	68	5	8	88	82	90	16	98	8	74	79	73	5	82	8 8	8 8	3 8	95	92	81	81	83	68	6	93	72	11	70	77	99	ŝ
	630 800	-	7 5			-	┿	12	+-	47		+	-	_	-		-	-			) 94	1 95	06 /	80	2 76	5 78	-	_		2 8	٠+.	+	┥~	+	5 81	⊢	-	_	3 85	88 9		9/ 6/	_	75 78	_	1 68
	500 63	_	99 99	87 87	+	+	+-	1	+	-	+-	+-	+			_	-	-+		_	91   90	-	87 87	85 82	79 7	92 92	-	_	-	96	2 5	3 8	86	+-	88 85	89 85	92 8	⊢	94	96 96	82 7	Н	H	-+	73	76 71
	400	ŀ	<u>و</u>	⊋ ;	# 14	3 5	19	3 8	5	+-	+	+	-	-	-	95	26	$\dashv$		82	16	26 9	_	68	83	72	99	94		96	-	_	+-	+-	68	-	⊢	₩-	-	94			_	88	-	6
[Z	125 160 200 250 315 400 500		70	2 F	-	+	┿	-	+-	+	+-	:15	10 105	12 111	95 98	95 98	$\overline{z}$	-+	-	86 87	106 104	107 105	007 100	98 95	92 90	75 71	69 67	99 10	-	101	-	50 00	٠	+	95 93	95 93	98 97	103 96	103 96	105 98	97 93	102 97	66 68	-	-	88 83
Frequencies (Hz)	200	$\overline{}$	-	86		7 62	+	+	┿	+	+-	- -	104	106	Н	66	≘	8	$\rightarrow$	68	101	101	97 1	95	8	82	9/	86		8 8	¢ :	3 3	3 =	80	95	95	66	107	107	Ξ	101	105	103	102	8	88
regue	190	-	_	E   3		28 80	+	, 7	2 6	3 5	72 68	1 8 2 8	+	┖	95 99			-	-	-	92 92	<u> </u>	88		82 84	+-	82 80		89 92	2 8		91 106	92 107	-	91 92	92 93	94 95	93 101	93 100	94 103	91 97	95 101	93 99	$\vdash$	-	85 83
enter F	100		-	87	-	, 8	-	76	7	2 08	+-	-	-	-	-		-	-	6 96		_	┡-	87	87	82	ļ	82		-		¥ 8		3 8	+	8	6	93	85	+-	87	-	↓	⊢	-	-	82
Lum C	80			8	8 6	86				: 8			5 84		1 93		4 95				1 84	83 84			2 80	83 86				94 95		84 84			_	87 88	89 91	83 83	_	_		_		80 84		
Spect	50 6		_	_	_	6/ 28	_	_	-	_	_	━		8 98	6 16	I	93		ı	_	-	_	80 79	_	_	+	+	-	-			8 8	-	-	-	+	-	-	82 8	+		+	-	_		81
Octave	32 40 50 63		99	-	F [	7 2	: 1	_	_	3 6	-		-		_	68	_			18	_	79	1 76	87	-		_	-	58 1	-	-+	83	-	-	+	83	88	+	+	-	+	18 (	8 79	-	3 76	78 79
at 1/3	25 32		_	68 74	_	73 69				00 59		-		79 85	-	84 89		_	82 85	78 80	74 79	76 80	73 74	71 78	+	-	+	87 87	_	$\rightarrow$	_	80 82		—	-	79 79	81 82	76 78	-	-		88	72 78	_	_	74 7
(dB)	702	_	5	22	99	۶ %	_	3 3	3 8	કે છ	<u> </u>	5 8	8	82	88	-	68	81	08	9/	76	75	69	73	99	73	99	88	79	98	\$	6 6	7 6	78	9/	-	79	47	74	79	+	93	76	_	_	78
Band SEL (dB) at 1/3 Octave Spectrum C	3 16	$\dashv$	$\dashv$	3	-	5 5	-	26 25		00 05 00 05	_	-	-	72 71	77 79	18 91	81 80	72 73	69 1.1	71 71	89 19	71 64	<b>2</b>	+-		+	+	73 80	89	$\vdash$	$\rightarrow$	68 72		67 74	+	62 71	68 75	-	+	+	-	+	98	-		80 78
Ba	10 13	1	29	_		414	+	7 10 10	-	-	_	+		78	-	85		. 9/	. 92	73	73	9	63	4—	-	-	-	83	-		-+	76	-	┰		+	-	+-	+	+-	-	-	73	-	$\overline{}$	11
Mic	Pos.	(E)	Base	Cavity	Cavity	Bace	Dasc	Base	Dasc	Base	Race	Cavity	Cavity	Cavity	Base	Base	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Base	Base	Base	Cavity	Cavity	Cavity	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Cavity	Base	Base
Rec.	Time	(min)	fled.	fled.	fled.		,	3.7	7.7	3.7	3.7	).' mi	ive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	tive	live	ive ive	five	tive	tive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	tive	Inactive
RCW	Resp.		Post-fled	Post-fled.	Post-	- -	-	7 (	۱,	7 (	1	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inactive	Inac	Inac	luac	Inac	Inac	Inac	Inac	Inac	Inac
Fvont		(m)	19	61	19	122	77	91.5	21.2	51.5	21.5	521	15.2	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	30.5	30.5	19	15 15	19	19	15.2	15.2	15.2	15.2	15.2	7751	15.2	30.5	30.5	30.5	30.5	30.5	30.5	19	19	19	19	19	19
Fyont	Type	-	.50 cal.	.50 cal.	.50 cal.	.50 cal.	Su cai.	.50 cal.	.So cal.	.50 cal.	.50 cal.	So cal.	50 cal	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	50 cal.	50 cal.	So cal	50 ca	50 cal.	50 cal	50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	So cal.	50 cal.	50 cal	50 cal	50 cal	50 cal	So call	50 cal	50 cal.	50 cal.	.50 cal.	.50 cal.	.50 cal.
Date			$\vdash$	6/3		+	+	+	+	+	4/29	+	+	╁	╁	5/11	5/11	5/11	╁	╁	+	十	+	+		+	+	十	╁	Н		Н	+	11/2	$^{+}$	+	十	+	+	+	╁	+	╁	+	-	5/11
3			227	227	227	878	4	-+	+	$\dashv$	+	+	23   52	231	231	231	231	231	231	231	231	231	331		157	122	1 2	236	236	236	236	236	236	236	250	35,5	356	33,5	33,6	23.6	236	236	336	236	236	236

<u>ا</u>		SEL	92.8	97.6	106.5	105.8	118.6	118.0	115.1	115.5	99.5	100.2	111.5	112.3	94.5	95.0	104.0	105.0	111.3	112.0	9.601	6.601	101.1	101.5	7.96	96.2	107.5	8.901	88.4	103.2	99.3	100.2	86.4	87.1
l	_	70007	22	51	16	68	24	51	\$	46	8/	79	36	39	63	65	98	16	69	71	62	64	75	74	19	19	89	19	20	45	45	45	44	4
	-	100001	53	51	94	93	63	62	54	\$	83	84	51	52	69	7.1	68	93	72	74	99	89	80	80	89	29	\$	29	58	47	43	45	20	51
	-	00671	99	54	94	94	89	99	99	28	83	84	55	57	72	74	8	93	76	11	72	73	82	82	17	=	99	70	63	55	47	20	57	58
	-	10000	99	59	93	94	69	89	29	29	83	85	09	62	74	75	8	93	81	81	77	61	83	84	73	73	72	75	99	65	59	62	19	62
		2000	2	62	93	93	73	71	8	\$	83	98	61	63	76	16	96	92	84	83	80	82	82	85	7.5	75	75	77	69	69	63	99	2	65
		0300	99	2	35	92	76	74	69	67	8	98	99	69	78	78	16	92	81	83	78	80	85	98	76	76	76	77	70	64	09	09	29	29
		nnac	89	99	91	92	9/	75	69	89	83	98	64	29	79	80	96	90	83	83	81	82	85	98	78	77	79	80	71	10	89	89	89	69
	0007	4000	8	29	91	93	79	78	2	72	82	88	69	72	80	80	96	88	82	98	84	88	84	98	78	79	-8	82	11	74	74	74	69	2
	0,00	<u>د</u>	2	89	32	92	82	81	2	72	8	82	20	73	8	82	86	06	87	88	84	84	84	87	78	79	84	84	73	73	71	74	71	7
ľ	0000	2500	2	89	2	92	85	84	76	9/	84	82	11	80	82	82	91	92	88	68	87	28	83	98	79	82	82	98	73	74	72	74	71	72
	0000	2000	2	69	93	16	88	98	79	78	84	98	75	77	83	82	91	91	92	63	16	6	85	98	8	82	8	16	73	82	62	81	72	72
	,	1600	2	89	68	88	16	8	83	83	84	87	73	73	79	79	$\vdash$	06		16	88	68	98	98	8	79	84	98	73	78	77	80	71	72
	-	0671	69	69	8	88	93	93	84	84	82	83	77	11	77	78	90	06	96	6	65	96	83	85	79	8	92	93	73	85	82	68	72	73
	000	1000	99	29	68	88	93	92	88	87	81	82	81	81	26	78	88	88	66	66	66	100	82	84	79	78	94	65	72	06	87	68	70	72
	0000	400 500 630 800	_	5 67	_	-		-	_	0 92	$\rightarrow$	-	16 91	$\vdash$	2 76	9 28	$\vdash$	4 87	3 94	2 95		0 93	$\vdash$			8 78	88	4 87	2 72	83	1 79	1 79	9 70	0 71
	27 000	900	-	73 65	-				98 90	-	80 81	_	98 98	82 86	74 75	74 76	87 84	87 84	96 93	6 6	$\vdash$	92 90	83 84	83 83	-	79 78	84 85	83 84	72 72	92 92	72 71	72 71	69 49	02 29
		400	_			-	_				77	78	58	88	69	69	88	68	_	06	_	84	85	82	11	78	18	18	89	15	72	72	49	64
۽ ا		1315		79	-		_	_	-	-	-	-	98	98	11	9/	98	88	90	16	-	98	84	-	18	18	82	82	10	82	12	9/	62	63
nter Frequencies (Hz)		125 160 200 250	82 81	84 85	$\vdash$	90 94	110 95	_	107 93	_	88 91	88 91	102 91	105 91	82 81	82 81	94 94	94 94	108 95	96 601	106 90	106 91	92 90	93   90	88 83	87 83	104 90	103 89	77 70	100 85	96 84	83	73 69	75 72
nenci		12 09	_	_	-	6 98	117 11	117 [11	114 10	_	8 8	_	110 10	111	8 8	8 8	6 06	6 06	102	106	102 10	105	-	$\vdash$	88 8	87 8	103 10	102 10	78 7	99 10	94   9	95 9	75 7	77 7
Fred		125		84	_	16	97 [1	-	94	94  1		68	94	94	88	98	87		92	92	16	93	-	06	88	87	92	16	75	98	28	87	9/	11
enter		<u> </u>		_	63	16	16	_	_	68	90	68		-	98	_	68	06	_	-	$\vdash$	-	90	-	87	86	86	98	77	83	_	⊢		77
Rand SEL (dB) at 1/3 Octave Spectrum Co		<b>2</b>	83	85	6	16	18	98	83	88	87	87	84	98	84	82	87	88	80	82	83	8	68	68 /	87	88	82	8	80	8	98	8	92 9	2 28
Trock.		0	_	8 80		68 /	88 88	88 /	-	85 85	3 85	3 85	1 82	2 83	18 6/	79 82	86 87	86 87	80 82	81 82	77 80	78 81	85 87	85 87	82 85	82 84	08 62	79	82 92	75 78	74 76	74 76	75 76	75 76
Save		95 S	26 80	75 78	88 28	87 87	8 28	86 87	82 84	83 8	80 83	81 83	80 81	82 82	1 91	18 7	83 8	85 8	8   11	77 8	77 7	7 97	83 8	84 8	8 8	8 08	78 7	77 7	74 7	73 7	72 7	72 7	73 7	73 7
Č		32	79 7	76 7	8 98	8   18	8 28	8 8	8 62	80	8 62	8 62	8 6/	80 8	73 7	74 7	82 8	83	73	75	78	79	81	818	8 82	3 //	11 11	77 7	71.	17	6/	70	70	71
1		52	72	72	85	84	08	80	83	81	75	74	9/	9/	89	71	82	82	6/	6/	62	8	78	78	74	73	75	72	65	2	65	63	65	8
E		20	52	69	81	84	8/	82	9/	82	10	13	75	74	<i>L</i> 9	100	9/	81	75	80	73	8	69	9/	72	72	74	75	89	29	65	99	99	99
SEI		<u>9</u>	75	62	82	⊢	8	80	18	80	74	72	72	75	9	2	8	62	83	18	79	74	75	69	19	64	17	19	55	99	55	57	55	28
Reg		10 13	7 72	63 64	3 70	70 78	74 72	Ļ	1 72	73 73	7 57	99	6 72	69 89	99	99	71 70	92 99	73 71	87 78	69 9	08 29	60 62	59 73	58 55	61 53	62 63	64 62	59 52	60 52	57 48	55 52	56 49	50 50
+	_	_	e   77	-	e 73	-	-	ty 77	ty 71	-	e 57	Base	ty 66	-	-	-		-	$\vdash$		├-	<del> </del> -	t			$\vdash$	_	_	<del> </del>	-	-	-	•	
Mis		— Pos. in)	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Base		Cavity	Cavity	Base	Base	Base	Base	Cavity	Cavity	Cavity	Cavity	Base	Base	Base	Base	Cavity	Cavity	Base	Cavity	Cavity	Cavity	Cavity	Cavity
١	ner,	Time   (min)	بو	٥	٠	نچ		Ę.	٠	Ġ.	Ġ.	ij	Ġ.	Ę.	- <del>.</del>	ė.	ė.	Ď.		Ę.	ų.	Ę.	- i	ij	ė.	j.		-j	<u>ني</u>	Ę.	Ď.	<u>ن</u> پو	j.	ايو
L	_		Inactive	Inactive	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled.	Post-fled.	Post-fled.	Post-fled	Post-fled.	Post-fled.	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled	Post-fled.	Post-fled	Post-fled.	Post-fled	Post-fled	Post-fled.	Post-fled
MJa	\ -	Resp.			_	_	_	_		_	_	_				_				_				Ĺ	<u> </u>	<u></u>	<u>-</u>						Ĺ	
Paront	Event	Dist.	19	19	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	19	19	19	19	15.2	15.2	15.2	15.2	30.5	30.5	30.5	30.5	19	19	19	19	91.5	91.5	122	122	122	122
Pront	Eveni.	Type	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.	.50 cal.
	Dale Dale		5/11	5/11	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/3	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21	6/21
3	 5		236	236	271	271	271	172	27.1	172	27.1	172	271	172	172	172	294	294	294	294	294	294	294	294	294	294	294	294	294	294	294	294	294	294

Table D 5. Summary data for passive M-16 live fire noise on Fort Stewart, GA.

Cluster	Date	Nesting	Event	Event	Azimuth	RCW	Recovery	Hemarks	Mic	SEL (dB)	at mic
		Phase	Туре	Dist.	re.	Response	time (min)	1	Pos.	Flat	Α
		& Day		(m)	DOF						
3	5/17/99	1-8	M-16		90	0	0	0	Base	71.5	63.2
3		1-8	M-16		90	0 ·	0	0	Base	72.0	63.6
3		1-8	M-16		90	0	0	0	Base	75.2	66.5
3	5/17/99	I-8	M-16		90	0	0	0	Base	73.9	65.7
3	5/17/99	I-8	M-16		90	0	0	0	Base	70.1	61.5
25	5/5/99	1-2	M-16		20	0	0	0	Base	66.3	63.2
25	5/5/99	I-2	M-16		20	0	0	0	Base	74.7	72.2
25	5/5/99	1-2	M-16		20	0	0	0	Base	67.8	63.7
25	5/5/99	1-2	M-16		20	0	0	0	Base	72.1	69.8
25	5/5/99	I-2	M-16		20	0	0	0	Base	68.1	65.6
25	5/5/99	1-2	M-16		20	0	0	0	Base	68.7	65.8
25	5/5/99	1-2	.50 cal		0	0	0	0	Base	76.0	50.2
25	5/5/99	I-2	M-16		20	0	0	0	Base	67.6	63.6
25	5/5/99	1-2	M-16		20	0	0	0	Base	71.4	69.5
25	5/5/99	I-9	.50 cal		0	0	0	0	Base	74.9	50.2
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	68.3	61.7
103		N-2	M-16	20-434	280	0	0	0	Base	67.2	61.8
103		N-2	M-16	20-434	280	0	0	0	Base	68.6	61.8
103		N-2	M-16	20-434	280	0	0	0	Base	68.0	62.5
103		N-2	M-16	20-434	280	0	0	0	Base	69.4	62.1
103		N-2	M-16	20-434	280	0	0	0	Base	71.3	64.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	76.2	70.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	69.2	62.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.2	69.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	70.3	66.0
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	68.3	62.0
103		N-2	M-16	20-434	280	0	0	0	Base	69.6	64.7
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	77.3	73.9
103		N-2	M-16	20-434	280	0	0	0	Base	74.6	67.9
103			M-16	20-434	280	0	0	0	Base	69.7	65.3
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	71.0	64.1
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	72.8	66.6
103	5/12/99		M-16	20-434	280	0	0	0	Base	71.0	64.2
103	5/12/99		M-16	20-434	280	0	0	0	Base	67.7	61.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	82.8	82.9
103	5/12/99		M-16	20-434	280	0	0	0	Base	78.8	78.7
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.8	64.9
103	5/12/99		M-16	20-434	280	0	0	0	Base	71.7	62.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	69.6	62.3
103	5/12/99		M-16	20-434	280	0	0	0	Base	83.9	84.0
103	5/12/99		M-16	20-434	280	0	0	0	Base	86.0	86.3
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.3	69.3
103	5/12/99		M-16	20-434	280	0	0	0	Base	70.4	64.4
103	5/12/99		M-16	20-434	280	0	0	0	Base	73.2	67.2
103	5/12/99		M-16	20-434	280	0	0	0	Base	74.6	74.0
103	5/12/99		M-16	20-434	280	0	0	0	Base	70.2	63.8
103	5/12/99		M-16	20-434	280	0	0	0	Base	71.3	66.1
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.4	68.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	75.5	69.8
			M-16	20-434	280	0	0	0	Base	70.9	64.4
103	5/12/99			20-434			0	0	Base	81.9	82.2
103	5/12/99		M-16		280	0		0		70.6	64.7
103	5/12/99	IN-2	M-16	20-434	280	0	0	ĮV	Base	1/0.6	104.7

Cluster	Date	Nesting Phase	Event Type	Event Dist.	Azimuth re.	RCW Response	Recovery time (min)	Remarks	Mic Pos.	SEL (dB)	at mic
		& Day	1,750	(m)	DOF	i iooponioo	()			Flat	A
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	68.3	61.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.3	68.7
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	69.9	63.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	67.5	60.1
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	68.5	61.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	69.7	61.0
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	84.2	83.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	77.5	72.6
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.8	70.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.8	66.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	85.1	85.5
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	79.4	76.2
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	76.1	70.6
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.9	70.5
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.0	69.6
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.9	67.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	76.0	68.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.6	67.7
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	67.6	62.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.4	71.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.8	74.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	75.1	68.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	74.4	69.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	78.8	76.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.9	68.2
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	72.0	65.5
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	74.5	69.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	71.5	66.1
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	76.0	71.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	74.4	73.8
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	77.0	74.5
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	74.1	69.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.0	66.0
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	71.2	70.3
103	5/12/99	<del> </del>	M-16	20-434	280	0	0	0	Base	71.4	65.6
103	5/12/99		M-16	20-434	280	0	0	0	Base	73.1	67.0
103	5/12/99		M-16	20-434	280	0	0	0	Base	76.7	69.9
103	5/12/99		M-16	20-434	280	0	0	0	Base	74.7	67.9
103	5/12/99		M-16	20-434	280	0	0	0	Base	76.5	74.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	73.3	65.7
103	5/12/99		M-16	20-434	280	0	0	0	Base	69.0	60.7
103	5/12/99		M-16	20-434	280	0	0	0	Base	67.3	57.6
103	5/12/99		M-16	20-434	280	0	0	0	Base	67.0	60.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	70.2	60.8
103	5/12/99		M-16	20-434	280	0	0	0	Base	78.4	72.7
103	5/12/99		M-16	20-434	280	0	0	0	Base	78.0	75.8
103	5/12/99		M-16	20-434	280	0	0	0	Base	74.8	72.2
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.6	67.0
103	5/12/99		M-16	20-434	280	0	0	0	Base	70.3	65.8
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.1	67.5
103	5/12/99		M-16	20-434	280	0	0	0	Base	70.1	65.8
103	5/12/99		M-16	20-434	280	0	0	0	Base	72.1	67.3
103	5/12/99		M-16	20-434	280	0	0	0	Base	77.2	74.7
100	10112133	J. 4-2	1141-10	120 707	1=00	<u> </u>	10		15456	1,,,-	1, 7,,

Cluster	Date	Nesting	Event	Event	Azimuth	RCW		Remarks		SEL (dB)	at mic
		Phase	Туре	Dist.	re.	Response	time (min)		Pos.		
		& Day		(m)	DOF						Α
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base		65.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	70.3	63.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	72.3	66.9
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	73.2	67.4
103	5/12/99	N-2	M-16	20-434	280	0	0	0	Base	76.4	71.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.4	61.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.7	71.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.6	63.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.5	74.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.5	63.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	78.3	75.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.2	67.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.0	66.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.1	62.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.8	63.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.9	64.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.9	66.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.4	63.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.6	73.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.7	73.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.5	71.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.7	71.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.4	63.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.0	67.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.4	73.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.8	72.9
103	5/13/99		M-16	20-434	280	0	0	0	Base	70.9	64.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.0	63.5
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.0	62.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.5	62.4
103	5/13/99		M-16	20-434	280	0	0	0	Base	71.5	64.5
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.3	67.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.8	66.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	75.6	66.3
103	5/13/99		M-16	20-434	280	0	0	0	Base	70.9	64.4
103	5/13/99		M-16	20-434	280	0	10	0	Base	72.3	63.2
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.7 70.5	66.9 63.9
103	5/13/99		M-16	20-434	280	0	0	0	Base		
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.4 71.7	62.9 62.6
103	5/13/99		M-16	20-434	280	0	0	0	Base		79.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	79.1 83.4	83.2
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.6	68.9
103	5/13/99		M-16	20-434	280	0	0	0	Base		85.4
103	5/13/99		M-16	20-434	280	0	0	0	Base	85.0	66.7
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.4 76.0	68.2
103	5/13/99		M-16	20-434	280	0	0	0	Base		68.7
103	5/13/99		M-16	20-434	280	0	0	0	Base	76.1	
103	5/13/99		M-16	20-434	280	0	0	0	Base	76.0	70.4
103	5/13/99		M-16	20-434	280	0	0	0	Base	74.6	69.8 75.5
103	5/13/99		M-16	20-434	280	0	0	0	Base	76.9	
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.2	70.5
103	5/13/99		M-16	20-434	280	0	0	0	Base	74.0	72.4
103	5/13/99	)  N-3	M-16	20-434	280	0	0	0	Base	80.5	81.3

103 5 103 5		Phase		Dist.	Azimuth re.	RCW Response	Recovery time (min)	Remarks	Mic Pos.	OLC (GD)	at mic
103 5 103 5		& Day	Туре	(m)	DOF	Пооролоо	unio (min)			Flat	Α
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.1	65.2
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	79.8	79.1
100	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.0	59.9
103  5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.2	63.5
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	80.8	80.3
		N-3	M-16	20-434	280	0	0	0	Base	78.2	78.4
			M-16	20-434	280	0	0	0	Base	69.9	66.6
			M-16	20-434	280	0	0	0	Base	70.9	63.9
			M-16	20-434	280	0	0	0	Base	73.3	61.3
		N-3	M-16	20-434	280	0	0	0	Base	75.1	64.8
		N-3	M-16	20-434	280	0	0	0	Base	72.0	64.1
			M-16	20-434	280	0	0	0	Base	73.6	64.9
		N-3	M-16	20-434	280	0	0	0	Base	69.2	69.0
		N-3	M-16	20-434	280	0	0	0	Base	73.2	63.2
		N-3	M-16	20-434	280	0	0	0	Base	78.1	74.1
		N-3	M-16	20-434	280	0	0	0	Base	72.7	64.7
	5/13/99 5/13/99	N-3 N-3		20-434	280	0	0	0	Base	71.2	63.6
			M-16	<u> </u>							
LL	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.0	61.3
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.0	66.0 66.9
		N-3	M-16	20-434	280	0	0	0	Base	73.9	
		N-3	M-16	20-434	280	0	0	0	Base	74.2	64.0
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	81.0	80.6
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.1	65.9
		N-3	M-16	20-434	280	0	0	0	Base	73.9	66.1
	·	N-3	M-16	20-434	280	0	0	0	Base	81.8	81.9
		N-3	M-16	20-434	280	0	0	0	Base	70.6	62.5
		N-3	M-16	20-434	280	0	0	0	Base	73.4	63.1
		N-3	M-16	20-434	280	0	0	0	Base	74.1	64.5
		N-3	M-16	20-434	280	0	0	0	Base	71.9	62.0
		N-3	M-16	20-434	280	0	0	0	Base	73.6	64.9
		N-3	M-16	20-434	280	0	0	0	Base	74.4	65.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	84.9	85.4
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.2	62.8
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.6	64.5
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	80.6	79.5
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.8	64.2
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.5	62.8
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	84.4	84.9
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.0	68.1
103 5	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.8	68.6
	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.7	65.2
	5/13/99		M-16	20-434	280	0	0	0	Base	85.7	86.3
	5/13/99		M-16	20-434	280	0	0	0	Base	72.9	68.9
	5/13/99		M-16	20-434	280	0	0	0	Base	73.7	66.3
	5/13/99		M-16	20-434	280	0	0	0	Base	82.1	82.1
	5/13/99		M-16	20-434	280	0	0	0	Base	73.0	71.7
	5/13/99		M-16	20-434	280	0	0	0	Base	71.4	69.8
	5/13/99		M-16	20-434	280	0	0	0	Base	81.4	82.1
	5/13/99		M-16	20-434	280	0	0	0	Base	82.5	83.3
	5/13/99		M-16	20-434	280	0	0	0	Base	83.0	83.8
	5/13/99		M-16	20-434	280	0	0	0	Base	82.6	83.5
	5/13/99		M-16	20-434	280	0	0	0	Base	75.0	71.6
	5/13/99		M-16	20-434	280	0	0	0	Base	74.1	66.8

Cluster	Date	Nesting	Event	Event	Azimuth	RCW	,	Remarks	Mic	SEL (dB)	at mic
		Phase & Day	Туре	Dist. (m)	re. DOF	Response	time (min)	l	Pos.	Flat	Α
100	E/4.0/00		N4 4 C	20-434	280	0	0	0	Base	73.7	66.6
103		N-3	M-16	20-434	280	0	0	0	Base	75.2	70.3
103		N-3	M-16 M-16	20-434	280	0	0	0	Base	76.7	72.7
103		N-3	M-16	20-434	280	0	0	0	Base	73.3	64.1
103		N-3	M-16	20-434	280	0	0	0	Base	75.8	66.8
103		N-3 N-3	M-16	20-434	280	0	0	0	Base	73.4	66.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	74.1	68.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.4	64.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.2	66.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.3	63.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.2	72.6
103		N-3	M-16	20-434	280	0	0	0	Base	73.3	64.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.3	63.6
103	5/13/99	N-3 N-3	M-16	20-434	280	0	0	0	Base	77.0	67.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	81.3	82.0
103	5/13/99 5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.8	70.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.1	67.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.3	66.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.9	74.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.4	64.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.6	64.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	80.5	80.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.5	71.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.0	61.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.3	61.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.1	65.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.6	70.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.5	70.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.1	65.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.2	63.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.7	69.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.0	72.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.7	70.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.6	62.2
103	5/13/99		M-16	20-434	280	0	0	0	Base	85.0	85.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	78.5	77.4
103	5/13/99		M-16	20-434	280	0	0	0	Base	71.3	65.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	82.2	82.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.5	67.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.6	64.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.7	74.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.8	62.8
103	5/13/99		M-16	20-434	280	0	0	0	Base	83.3	84.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.8	70.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.7	72.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.5	76.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.1	69.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.4	65.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.2	62.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.8	75.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.2	66.0
103	5/13/99		M-16	20-434	280	0	0	0	Base	75.4	75.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.3	68.5

Cluster	Date	Nesting Phase	Event Type	Event Dist.	Azimuth re.	RCW Response	Recovery time (min)	Remarks	Mic Pos.	SEL (dB)	at mic
		& Day	Type	(m)	DOF	response	Line (min)		1 03.	Flat	A
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	82.1	82.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	78.9	78.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.5	62.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.5	63.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	78.2	77.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.7	69.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.5	67.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.5	66.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.1	66.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.2	64.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	84.4	84.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	82.8	83.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.5	74.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.5	69.4
				20-434	280	0	0	0	Base	71.8	68.6
103	5/13/99	N-3	M-16 M-16	<del></del>		0	0	0	Base	71.5	67.0
103	5/13/99	N-3		20-434	280			+		77.8	75.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.8	68.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.8	76.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base		55.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	63.5	56.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	66.9	63.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.0	65.9
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.2	
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.2	63.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.9	76.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.1	62.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.6	73.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.0	65.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.2	63.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.0	63.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.4	66.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.1	67.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.7	67.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.8	69.7
103	5/13/99	<del></del>	M-16	20-434	280	0	0	0	Base	73.1	64.9
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.6	64.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	83.8	84.3
103	5/13/99		M-16	20-434	280	0	0	0	Base	75.0	74.2
103	5/13/99		M-16	20-434	280	0	0	0	Base	77.7	77.7
103	5/13/99		M-16	20-434	280	0	0	0	Base	82.0	81.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.9	64.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.1	63.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	82.9	83.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.2	68.2
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.3	67.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.8	70.3
103	5/13/99		M-16	20-434	280	0	0	0	Base	71.6	63.7
103	5/13/99	·	M-16	20-434	280	0	0	0	Base	72.4	68.0
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.5	70.3
103			M-16	20-434	280	0	0	0	Base	68.6	57.5
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.2	68.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	75.1	72.3
103	5/13/99		M-16	20-434	280	0	0	0	Base	74.0	69.9

Cluster	Date	Nesting	Event	Event	Azimuth	RCW		Remarks	Mic	SEL (dB)	at mic
		Phase & Day	Туре	Dist. (m)	re. DOF	Response	time (min)		Pos.	Flat	Α
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.6	73.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.1	64.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	78.6	78.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.1	61.7
103		N-3	M-16	20-434	280	0	0	0	Base	82.2	82.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	74.6	73.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	80.7	80.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	83.7	83.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.4	69.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.6	62.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.8	65.7
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.6	70.1
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	76.9	75.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	69.7	64.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.4	66.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.3	65.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	69.2	58.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	69.1	57.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.9	67.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.7	63.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.7	70.5
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	75.0	66.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	68.8	60.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	70.8	71.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.4	71.1
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.3	67.7 64.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.2	77.8
103	5/13/99		M-16	20-434	280	0	0	0	Base	78.0 70.8	67.8
103	5/13/99		M-16	20-434	280	0	0	0	Base	72.4	67.2
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.6	70.8
103	5/13/99		M-16	20-434	280	0	0	0	Base	87.2	87.9
103	5/13/99		M-16	20-434	280	0	0	0	Base	70.2	68.8
103	5/13/99		M-16	20-434	280	0	0	0	Base	70.4	63.5
103	5/13/99		M-16	20-434	280	0	0	0	Base Base	80.9	81.0
103	5/13/99		M-16	20-434		0	0	0	Base	83.9	84.4
103	5/13/99		M-16	20-434		0	0	0	Base	78.2	78.6
103	5/13/99		M-16	20-434	280	0	0	0	Base	73.6	69.9
103	5/13/99		M-16	20-434	280	0	0	0	Base	71.9	69.8
103	5/13/99		M-16 M-16	20-434	280	10	0	0	Base	72.6	69.8
103 103	5/13/99		M-16	20-434		0	0	0	Base	72.4	67.6
103	5/13/99		M-16	20-434		0	0	0	Base	81.5	81.8
103	5/13/99		M-16	20-434		0	0	0	Base	70.3	68.5
103	5/13/99		M-16	20-434		0	0	0	Base	69.6	59.8
103	5/13/99		M-16	20-434		0	0	0	Base	83.7	84.1
103	5/13/99		M-16	20-434		0	0	0	Base	77.0	74.4
103	5/13/99		M-16	20-434		0	0	0	Base	73.8	66.0
103	5/13/99		M-16	20-434		0	0	0	Base	70.2	65.4
103	5/13/99		M-16	20-434		0	0	0	Base	68.3	61.3
103	5/13/99		M-16	20-434		0	0	0	Base	71.9	65.9
103	5/13/99		M-16	20-434		0	0	0	Base	70.0	62.4
103	5/13/99		M-16	20-434		0	0	0	Base	73.4	69.4
103	5/13/99		M-16	20-434		0	0	0	Base	69.6	61.9

Cluster	Date	Nesting	Event	Event	Azimuth	RCW	_	Remarks	Mic	SEL (dB)	at mic
		Phase & Day	Туре	Dist. (m)	re. DOF	Response	time (min)		Pos.	Flat	Α
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.0	68.6
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	73.2	65.3
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	70.8	65.4
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	72.7	70.0
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	71.5	63.8
103	5/13/99	N-3	M-16	20-434	280	0	0	0	Base	77.3	77.4
103		N-3	M-16	20-434	280	0	0	0	Base	68.4	60.1
103		N-7	M-16	20-434	280	2	0	0	Base	81.4	80.7
103	5/17/99	N-7	M-16	20-434	280	2	0	0	Base	84.0	84.4
103		N-7	M-16	20-434	280	2	0	0	Base	79.1	75.2
103		N-3	M-16	20-434	280	0	0	0	Base	72.2	68.8
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.3	70.3
		N-3	M-16	20-434	280	0	0	0	Base	72.6	66.4
103	5/17/99										71.0
103	5/17/99	N-7	M-16	20-434	280	2	0	0	Base	76.3	
103	5/17/99	N-7	M-16	20-434	280	2	0	0	Base	79.0	76.4
103	5/17/99	N-7	M-16	20-434	280	2	0	0	Base	74.0	73.1
103	5/17/99	N-7	M-16	20-434	280	2	0	0	Base	78.3	73.4
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	73.5	69.7
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	83.4	82.8
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	77.2	73.2
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	74.7	70.8
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	75.7	72.4
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	74.5	71.1
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	71.7	67.7
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	84.8	85.3
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.6	72.9
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	73.1	69.7
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	87.9	88.1
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	75.2	69.5
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	87.4	87.8
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	84.0	83.8
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	73.5	68.9
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	72.6	68.4
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	78.2	74.1
103	5/17/99	N-7	M-16	20-434	280	0	0	0	Base	86.0	86.4
103	5/17/99		M-16	20-434	280	0	0	0	Base	87.9	88.1
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	79.2	75.9
103	5/17/99		M-16	20-434	280	0	0	0	Base	75.4	74.0
103	5/17/99		M-16	20-434	280	0	0	0	Base	74.3	70.6
103	5/17/99		M-16	20-434	280	0	0	0	Base	74.1	68.8
103	5/17/99		M-16	20-434	280	0	0	0	Base	83.2	83.2
103	5/17/99		M-16	20-434	280	0	0	0	Base	83.4	83.1
103	5/17/99	1	M-16	20-434	280	0	o	o	Base	76.3	73.3
103	5/17/99		M-16	20-434	280	0	lo	0	Base	73.8	68.4
103	5/17/99		M-16	20-434	280	0	0	0	Base	77.9	74.3
103	5/17/99		M-16	20-434	280	0	0	0	Base	75.6	71.2
103	5/17/99		M-16	20-434	280	0	0	0	Base	71.6	64.0
103	5/17/99		M-16	20-434	280	0	0	0	Base	73.8	70.6
103	5/17/99		M-16	20-434	280	0	0	0	Base	70.4	64.8
	5/17/99		M-16	20-434	280	0	0	0	Base	72.7	66.0
103				<del></del>		0	0	0		79.6	79.2
103	5/17/99		M-16	20-434	280				Base		
103	5/17/99		M-16	20-434	280	0	0	0	Base	75.8	70.4
103	5/17/99	114-3	M-16	20-434	280	10	0	0	Base	72.5	65.9

Cluster	Date	Nesting Phase & Day	Event Type	Event Dist. (m)	Azimuth re. DOF	RCW Response	Recovery time (min)	Remarks	Mic Pos.	SEL (dB) Flat	at mic
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	75.8	69.2
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	80.3	79.3
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	80.7	79.0
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	79.2	73.7
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.7	71.7
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.8	73.0
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	72.7	70.2
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.2	71.1
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	72.8	68.2
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	77.3	72.7
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	72.9	68.3
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	75.5	70.1
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	76.7	75.4
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	78.6	78.5
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	70.2	65.9
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	73.3	67.0
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	72.5	66.7
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	77.6	77.2
103	5/17/99	N-3	M-16	20-434	280	0	0	0	Base	70.5	66.0

Calc.	Overall SEL	71.5	72.0	75.2	73.9	70.1	66.3	7.4.7	67.8	72.1	68.1	68.7	76.0	9'.29	71.4	74.9	68.3	67.2	9.89	68.0	69.4	71.3	76.2	69.2	75.2	70.3	68.3	9.69	77.3	74.6	73.0	200	71.0	67.7	82.8	78.8	72.8	71.7	9.69	83.9	86.0
	20000	9	6	11	12		8		8	8																				1	25				53					32	အ
	16000	ន	55	21	24		11	18		17	16	13	8	16	20	15	78	92	R	22	27	52	28	31	23	52	23	23	53	07	23 %	3 8	3 ន	23	<del>\$</del>	34	31		23	49	25
	12500	56	27	24	25		8	13	13	8		80		Ξ	13			Ì					20	20	23				8				25		49	44				53	58
	10000	30	34	30	53	32	13	21	17	21	19	21	55	13	52	4	ន	ន		દ્ધ	50	31	31		31	28	56	56	ક્ક	8	55 K	3 8	ខ្ល	20	25	20	83	27	23	ક્ક	63
ŀ		38	40	37	37	42	50	56	21	25	23	52	17	24	<b>3</b> 8	19	35	32	33	33	52	35	33	35	38	39	35	33	4	25	8 2	2 %	3 8	33	28	52	g	31	31	29	
	6300	51	51	20	8	41	19	24	19	23	20	18		15	56		ន	ຂ	37	ଯ	20	32	44	38	42	46	29	88	45	<del>Q</del>	47 25	3 8	37	88	83	99	88	ន	31	89	72
	5000	41	42	41	8	46	36	36	36	37	35	35	82	င္က	35	32	37	g	36	37	37	41	20	43	50	53	42	42	51	48	49	3 2	‡ £	42	65	22	46	89	33	ន	55
	4000	44	41	43	47	49	41	88	36	36	34	34	31	32	37	93	54	54	£	4	45	46	53	45	52	53	46	46	25	2	25 8	2 0	ş 4	4	8	8	49	4	43	2	72
		49	48	49	25	47	41	40	45	37	36	98		98	9	ဆ	45	4	4	£	45	47	22	47	28	69	48	49	88	23	25 2	5 5	g 24	47	23	98	25	47	45	69	F
		49	48	51	54	21	æ	45	38	43	45	令	53	41	47	8	47	47	69	47	49	51	61	51	28	25	51	55	5	22	ß 2	5 2	¥ 53	51	75	71	52	25	51	75	74
	2000	48	49	23	51	20	33	49	44	49	47	45	58	45	51	က္က	S	<del>а</del>	21	20	48	51	62	22	9	22	53	22	49	83	32	3 5	ý 45	52	8	88	æ	ಜ	52	74	78
	1250 1600 2000	20	51	92	83	55		24			_	_		_	_	$\dashv$	_				-			-	$\vdash$	⊢	Н	$\vdash$	-	-	8 4	+	-	┿	┢	⊢	├	<del>! -</del>	Н	-	
				_	_	22	<u> </u>	Н	Н	H	_	ш	-			$\dashv$	-			_		-	Н	├	├	-	Н	$\vdash$	-	-	8 3	-		╫	⊢	├	├	╀	⊢	-	
	1				L	$oldsymbol{ol}}}}}}}}}}}}}}}}}$	<u> </u>	_				ш	$\Box$	$\Box$				_			Ш		Ц	L-	1	L.	Ш		_		22	-	-	4-	⇤	┺	╙	ន	_	-	Н
		$\vdash$	H	<u> </u>	-	ļ	-	Н		-	-	$\vdash$	-	$\vdash$		$\vdash$	$\vdash$	-		_	$\vdash$	-	Н	⊢	-	┞—	-				8 2	+	-		┿	-	₩	49	-	0 73	Н
	_			_	<b>!</b>	2 25	_	70 7		-	ш	$\vdash$	$\vdash$	Н	_	-	-			-		$\vdash$	Н	$\vdash$	-	₩-	Н	-	-	-	22 22	+	-	+-	⊢	⊢	-	8	-	$\vdash$	-
		_				42 5	┡-	-			$\perp$	$\perp$		$\vdash$		_	_				-	_	_	ļ	-	┿	-	$\vdash$	$\rightarrow$	_	री ह			+	╄	+-	+	╄	⊢	_	64 (
		-		⊢	⊢	53	_	_		_	_	$\vdash$		-		$\vdash$		_	_		-	$\vdash$	-	╙	-	_	-	_		-	6         5	-	-	-	-	-	-	+-	-	23	22
	250	05	25	54	54	26	<del>우</del>	49	42	47	47	44	43	49	48	40	23	72	\$	21	54	25	အ	95	8	ස	25				: R				_	8	19	ŝ	88	19	61
	160 200	49		ಜ	-	28		48	_	_			_	_	_	_	_	જ		-	_		64		_	22	-	_			88	_	_	_	_	8	-	88	_	85	23
		⊢	⊢	⊢	25	├	5	-	44	_	-	_	_	48	-	$\vdash$	-	33	-		⊢	$\vdash$	29	-	┼	-	29	-	-	:S		-	<del></del>	+	╌	+-	+	+-	┞—	65	83
es (Hz	80 100 125	59 55	61 56	64 60	63	58 61	44 46	51 51	49 46	-	53 47	$\vdash$	$\vdash$	51 53	-	Н	-	57 55	_	-	60 59	_	99 89	9	99	61 61	28 60	-	$\vdash$	99		-	2 E	+-	╌	+-	<b>12</b> 53	┿		9 29	$\vdash$
dneuc	8	62	23	9 /9	65	29	84	53	$\vdash$	$\vdash$	ш		-	-	25 4	-	Н	26		_	19	19	├	65	┿	8	88	<del>                                     </del>	$\vdash$	-	<del>-</del> +		3 8	+-	+	+-	-	+	₩		65
ter Fre	8	89	-	69	88	╄	51	22	⊢	-	-	-	┝	-	_	Н	$\vdash$	22	-	88	├—	├	89	┞		╄	⊢-	-	₩	8	-+-	-	3 2	┿	2	25	8	+-	₩.	2	8
ım Cer	ଝ	62	62	29	88	82	8	22	જ	22	જ	25	7	21	51	29	28	54	22	99	જ	22	84	22	5	Ŗ	જ	26	29	23	ន	ខ្ល	33 82	3 8	150	83	88	ß	+	-	8
pectr	\$	⊢	<del>-</del>	22	+	53	⊢	ន	⊢-	├	⊢	ន		-	-	$\vdash$	_	\$	_		-	-	-	┿	88	-	┼	-	8		-+	-	<u>بر</u>	+	83	+-	╂	+	+-	ස	-
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	33	ස	ļ	8	<u>ස</u>	8	╄-		⊢	42	-	-	8	47	8		-	20	_	22	₩-		58	╄	+	\$	╄	-	92	_	_		3 S	+-	8	+-	+-	╄	↓	٠.,	22
1/30	25	⊢	29	├-	╌	Ļ	43 47	╀	50 55	42 45	⊢	44 43	56 61	7 49	45 41	63 62	$\vdash$	43 53	_	14	53 42	38 45	6 <del>0</del>	4	51 52	⊢	47 45	-	49 48	_		+	47 52	+	51 48	+	┿	41 45	120	22	25
(dB)	8 8	50 48	55 54	⊢	49 52	+	47 4	46 4	54	48		4	49	45 47	各 4	48	$\vdash$	$\vdash$	$\vdash$	⊢	53	$\vdash$	55	18	┰	4	52	╄-	-	_		+	± 5	+	+	55	-	┿	47	84	41 5
<b>P</b> SEL	5	8	8	-	+	+	4	37	64	╄	£3	⊢	⊢	⊢	±,	48		41 '	Н	Ë	-	Ť	-		Ť	H	-	Ė	Ì			+	+	+	$\dagger$	+		+	T	F	H
Ban	2	8	S	_	╄	┿	┼	╌	င္သ	₩	37	-	-	8	4	$\vdash$	37	-	4		ಜ	46	T	4	t		25	4	84	41	4	1	ę		125		8	8		8	₩
Mic	Pos.	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base	Base
Event Mic Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	(m)	200	200	299	200	200	1200	1200	1200	1200	1200	1200	0	1200	1200		20-434	20-434	20-434	20-434			20-434	20-434	20-434	20-434	20-434		I. I	20-434	20-434	20-434	20 434	20-434			20-434			20-434	20-434
Event	Type	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	.50 ca	M-16	M-16	.50 cal		M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16		M-16		M-16			¥-16	Z Z	M-16	9 W	M-16	M-16	₩-16	M-16	M-16
Col. Date		5/17	2/12	2/12	5/17	5/17	5/2	5/2	5/5	5/5	5/5	5/2	5/2	5/2	5/5	2/2	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	5/12	_	5/12	5/12	3/15				-	-	5/12	5/12
Ŝ		က	က	က	က	က	ន	ĸ	g	23	£	33	જ	ಜ	જ	ន	ਛ	සි	និ	<u>ខ</u>	និ	ਛ	ਛ	ន	සි	සි	8	ਛ	ਛ	ਛੁ	ន	<u>ම</u>	និន្ត	3 \\ \varepsilon	8	<u>≅</u>	<u> </u>	<u> </u>	\$	ន	5

				٦	٦	T									_												_				T	T.	$\mathbb{T}$	_		6		ے	<sub>s</sub>		4			
Calc.	SEL	72.3	70.4	73.2	74.6	70.2	71.3	72.4	75.5	70.9	81.9	70.6	68.3	75.3	69.6	67.5	68.5	69.7	84.2	77.5	75.8	73.6	85.1	79.4	76.1	75.5	75.0	73.5	76.0	73.6	70/1	2 2	75.1	74.	78.8	73.	72.	74.	71.	76.	74.	77.0	4.	73.
20000	2000	23																	23				8			20																		
16000	300	56	22	88	88	22	8	56 26			17	27	ଛ	27	23	52	22		36	28	82	53	22	ଝ	හ	ឌ	ន	23	္က	8 8	<b>8</b> 8	3 2	3 83	56	59	99	22	27	53	52		30	82	88
10500					53		ន	ಜ	27		52							_	43	<b>2</b> 6	<sub>2</sub>		22	52		ឧ	8				5	3 8	3		33			20	82	50	31	ક્ષ		
-	_									-			_	_				_													+	+	-		_				_	_	7	2		
4000								32	_	_	_			Н								-					_	_	-	$\dashv$	+	+	8	├-	-	L	-	H	-	┞	$\vdash$	$\vdash$	$\dashv$	$\dashv$
0008		H	32	Н		Н			<u> </u>	▙	┞	-	Н	Щ			Н					Ш				Ш	_		4	4	4	-	3 8	┼—	╀	-	╀	╄~	╁	⊢	-	$\vdash$	Н	
0069		40		37	_	Н		44	┝	+	┝	$\vdash$	_	_			56		-	-		Н	Н					$\vdash$	$\dashv$	$\dashv$	+	+	<del> </del>	t	╁╌	╁	H	t	t	1	╁╌	Н	Н	
2002				L				L	_	L	L	L					L	<u></u>					L	Ш		Ш				_	4	4	3 8	↓_	╄	L	╄-	L	Ļ		▙	Н	$\vdash$	Н
900	4	Ц.	L_						ـــــ	↓_	↓_	٠.	<u> </u>		_	-	-	_	-	_		$\vdash$	-	-	$\vdash$	-		-	_	$\rightarrow$	-	-+	8 5	+-	┰	+	+	-	+	+-	+	+	-	_
0450					_	$\vdash$	L	ļ.	_	╀	↓	-	L	<u> </u>	-	├—	⊢-	_	ļ	<b>—</b>	├-		-		⊢	$\vdash$		-	_	-	-+	-	8 15	+	+	+	+	+-	+	+	┿	+	Н	$\boldsymbol{\vdash}$
7050	0007 0007 009L			L		$\Box$		1_	_	_	١	4—			<u></u>		⊢–	<u> </u>	Н—	╙	⊢-	┡	<u> </u>	-	⊢	$\vdash$	_	-	Н	$\vdash$	-	-+	3 88	-+	+-	+-	+	┿	+-	+	+-	1	-	Н
	<u> </u>	1			L			٠	_	-	┺-	-	—	_	_	-		-	⊢		├—	_	⊢-	╄	-		-	-	_	-	-	-	8 8	┿	+	+	+	+	+-	+-	+	1		
1	<u> </u>	_	_	ᆫ	L_	ㄴ	Ļ	1-	-	╄	4-	╃—	┡-	-	<b>—</b>	<b>!</b> —	⊢	_	⊢	⊢	⊢	⊢	┞	├	<b>├</b>	<b>├</b>	_	┞		$\vdash$	$\rightarrow$	-	à 6	+-	┰	+-	+	┿	+	+	+-	-	-	-
	262	L.,	ــــــــــــــــــــــــــــــــــــــ	_	Ļ	┺-	L-	╄	┺	╄	-	-	_	┞~	┞	├-	-	⊢	₩	┡	₩	-	├-	-	⊢	⊢	-		├—	⊢⊢	-	-	2 E	┿	+-	+	+-	┿	+	+	+	+	-	
	3	1		1	L		L.		_	ㅗ	_		_			١	<u> </u>	_	┺	_	ㄴ	ـــ	ـــ				1—	1-		-	$\rightarrow$	-	8 8	+	<del></del>	+-	+	+-	+-	+-	+-	+-	-	
	<b>≋</b>							1	<u></u>											L	<u> </u>		_	_				_	_			_	3 8	-			-	-	_	-	-	-	+	-
	200	· !			L										_		-	_	-	_	_	1	_		-	+-	-	-	-	-	$\rightarrow$		8 x	-	-	-	_	-	_	_	_	_		
I ⊩	<del>2</del> 35		_	1			1		_				_	1	_	-	-	-	-	-	-	_	-	-	-	-	_	-		-	$\rightarrow$	_	36 37		_	_	-	_	-	-	-	-	_	-
	315 #	1			1	I	_								_			1	_	_	_		_	-			_	_		_	$\overline{}$	_	8 2	_	_	_			_	_	_	_	_	_
1 F	 520			L			1		_	_		1		1		_	_		_		_		_	_	_		-	-	-	$\overline{}$	$\rightarrow$	_	8 8	-	-	_	-	-	_	-	_	_	+	+-
l t	음	83	+	┿	1-	1	+-	+-	25	+	_	+-	1	99	1	1_	19		1	1.	1.	١.,	1_	1	_	જ	-	_	ಜ				8 8											ន
	9	8	æ	ន	88	88	9	5	65	32	8	85	26	65	65	25	29	55	29	99	49	64	8	29	94	83	ន	62	8	64	99	છ	8 8	3 8	3 8	3 8	8 8	3 8	8 8	+	+-		┿	8
Œ	<del>1</del> 25	8	8	26	9	8	8	នេ	8	8	8	8	88	┿	┰	+-	┿	╌	+-	+	8	+-	+	+-	+	+	છ	┿	19	+-	Н		ଞ		+	+-	+	+	+-	+	+	+	+-	ន
encies	8 5	ន		ន	+-	5	╌	+-	┿	+-	┿	+	┿	┿	8	+	ස	+-	+	┰	+-	┿	+-	+-	+	+	+	┿	8	╄~		-	ន	+	+		+	-	-	+	┿		┿	99
Frequ		83	+-	+	┼	┿	┿	┿	+	╌	+		┿	┿	19	┿	59	+-	+	+	+	╄	+-	+	+	+	+	+-	┿	61	-	-	3 61 61	+	+-	+	+	+-		+		┿	+	64
Center	ප ස	┿	59 62	+	+-	+	┿	┿	+	+-	3 2	+-	56 58	↤	98	+	52 57	+-	62	+-	65	+-	┿	+-	+	+-	+-	+-	+-	┼	53 55		28 28	+	+	┿	+	+-	+	+	+		┿	$\vdash$
etre.	송 	+	57 5	+-	┰	╂	┿	┿	+-		3 12	+-	25	+-	+-	+-	+-	┰	65	╌	+	+-	┿	+	┿	+-	+-	+	┿	┿	-	-	92 2	+	+		+	+	+	-	+	25	+-	8
e Spe	33	8	+-	+-	┿	┿	╄	-	+-		3 2	+	25	+-	5	+-	51	+	8	-	+	+	+	┿	+-	+-	┿	+	+-	22	25		18 2	-	+	┿	+-	-	+	+		\$ Q	+	ß
Octav	8	63	┿	┿	+-	83	+-	+-		-	-	+-	┿	ES	┿	┿	$\dagger$	47	+-	+-	+	+	+-	+-	+	+-		8	+	25	4	32	ક્ષ્	2 2	ត	3   3	‡ 4	۽ و	ş   ¥	3 2	5 4	\$ 4	23	45
at 1/3	8	64	: 4	8		9	5	3	æ	3	5	3 8	i E	ន	22	4	1	5	1 22	1 2	1 2	8	5 2	- 9	48	25	25	\$ 8	4	T	8	48	4 :	₽ Z	5 Z	5 9	ş ç	ş ş	<b>2</b> 8	કુ ફ	ş (e	ş <del>8</del>	<u>ئ</u>	38
(dB)	9	64	2 6	4	47	45	α V	} <u>15</u>	2	3 5	ç ç	\$ 8	8	14	4	8	89	4	9	8	85	8	থ	8	: E	94	46	2	64	88	46	44	S :	÷ ;	g ç	ş y	g 7	ត	3 5	3 á	<u>କୁ</u> ଦୁ	4 &	65	29
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	55	I					$\prod$	$oldsymbol{\mathbb{I}}$	\$	-	ន្ន	3	47	1	$\prod$	67		5		$\int$	44											L	43	1	₽	1	$\perp$	$\downarrow$	$\downarrow$	$\downarrow$	1	4	1	
	10	.	2	_1 ~	٩	4	+-	و ا	و ا	┙,	n	3 5	+-	⊣ ց	1	+	4	2	4	+-	ન વ	و ا	واي	8	+-		╅	+-	+	+	49	g	$\vdash$	=	๛⊩	#	დ  –	‡ ;	pase	Base	Base	Dase Se 47	–ia:	8
Mic	Pos.	Bace	۵			- 6	_	i	å		٥				å			┸	L_	_1_			L	å			丄			1		Base		Ě	L	ă	_L	ğ		$\perp$	$\perp$	ä	3	le e
Event	Dist.	20.434	20.434	20.434	20.434	_		_	_	_	404 404 404 404	_	_		_	_			20.434					_					_		_	20-434	-	_			_	_	_	_	_	2 63		
Event	Type	M.16	N 4	¥ 4	M 46	2 2	2   9	5 X	2 4	2 5	₽   <del>\$</del>	5 5	¥ 2	2 2	2 4	2 4	1 4	2 2	2 2	¥ 4	2 4	2 4	2 2	N Y	2 4	M-16	N A	M-15	2 2	¥ 9	M-16	M-16	M-16	M-16	9 3	<u>ا</u> ۾	¥-19	2 S	و غ	9 S	9L-₩	2 2	¥ 2	2 <del>2</del> 2 <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del>
Date	-	6/19	-		-	+	4	-	-	-	-	21/6	_		-	-		-	-	_		—		-	-			-	-	+-		5/12	-		5/12	21/2	5/12	2/15	215	2/12	2/12	2/12	5/10	5/12
<u>S</u>	-	-   =	-		-	3 5	-	3 5				3 5	-	-	-+-	-	3 5	_	-	-				_	-	-		-	_		_	+	55	$\rightarrow$		-	-	-+	<u> </u>	-+	<del>-</del>	3 5	-	

Calc.	Overall SEL	71.2	71.4	12	76.7	74.7	76.5	73.3	0.69	67.3	0.79	70.2	78.4	78.0	74.8	72.6	70.3	72.1	70.1	72.1	77.2	72.0	70.3	72.3	73.2	76.4	71.4	76.7	9.07	77.5	72.5	78.3	75.0	72.1	71.8	71.9	72.9	73.4	75.6	73.7	74.5	75.7	70.4
	20000						20														50									53	R		+	+						23			-
	16000	30	g	22	ន	52	59	50	23	23	50	25	28	35	53	23	56	52	22	23	92	50	25	20	28	53	8	53	20	8	R)	35	3 8	27	83	52	28	27	53	26	53	ಜ	R R
	12500	23		8	33	33	31						50	41	33						32				50	93		52		34		14							56	34		31	
	10000	33	R	g	g S	56	40	30	23				31	47	38	28	27	28	56	50	42	25	29	22	30	37	52	88	82	40	8	48	3 8	8 %	ន	27	25	25	41	38	30	88	೫
	8000	41	8	34	ဗ္ဂ	37	47	33	8	83	8	35	ဇ္ဌ	21	4	38	35	32	36	34	47	34	35	34	34	45	35	£	83	8	5	51	5 8	8	33	38	88	33	49	49	38	4	ജ
	9300	44	8	89	<b>₽</b>	39	51	37					45	55	49	40	34	36	33	35	49	37	32	33	35	55		47		25	83	2	3 6	5		25	22	ន	22	48	45	25	ล
	2000	51	5	46	<b>Q</b>	47	54	44	ස	35	37	37	22	28	25	47	45	45	44	45	54	43	44	44	46	28	္က	25	စ္တ	26	<sub></sub>	\$ C	٤	5 4	£	£	45	43	25	25	49	8	41
	4000	54	4	ន	ន	21	28	49	£	40	42	42	54	61	33	25	49	49	47	51	26	48	47	49	92	88	4	<u>2</u> 2	4	19	<b>φ</b>	92	5 8	3 4	14	64	84	46	19	64	ਹ	88	47
	3150	23	5	ន	SS.	22	63	51	44	4	14	40	28	64	29	22	23	20	51	22	19	21	25	54	54	8	43	28	45	8	8	8 4	3 8	3 8	8	25	65	47	99	69	29	5	5
	2500	29	83	28	5	22	64	55	47	46	47	47	99	29	ន	22	25	99	54	29	83	22	24	22	22	83	22	8	22	8	22	8 8	3 2	3 23	25	55	25	ಜ	61	65	62	83	છ
	2000	62	25	82	8	88	62	55	49	45	89	48	19	29	64	29	28	25	22	28	64	26	54	28	22	28	25	61	54	8	53	9 9	3 8	3 2	8 8	28	88	ಬ	65	25	26	27	ස 
		62	22	25	5	88	93	28	ಜ	45	25	48	62	89	ន	57	25	28	26	22	29	26	53	28	29	19	25	64	55	83	33	8	3 8	3 8	8 8	જ	8	54	65	53	64	æ	જ
	1250	19	83	25	8	82	29	အ	52	47	25	51	64	99	64	57	99	09	28	58	89	22	53	28	58	62	22	64	92	8	83	8 8	3 5	3 2	8	72	83	ಜ	8	ಜ	29	25	ន
	1000	88	22	83	හ	29	29	28	ಜ	49	ಜ	53	29	65	83	26	53	09	09	22	29	99	53	22	28	63	51	62	55	8	25	29	5 5	3 8	S 2	ಜ	25	51	64	જ	61	28	25
	800	22	22	82	24	5	64	54	<b></b>	45	89	49	63	63	91	54	22	28	52	99	64	54	20	22	54	62	48	59	23	25	69	<b>2</b> 2	ង ន	3 8	65	ಜ	22	အ	8	47	83	22	47
	930	┅	-			_	_	-	┞			-	-	_			-	_	-	-	-	-	-		-			_	_	-	-+	-	-	<del></del>		+-	+	+	+-	+-	द्ध	_	
	8	-			1	_	-	╙	-	—	—	_	-	_	-	_	$\vdash$	-	-	-	$\vdash$	$\mathbf{I}$	ш	_	-	-			-	-	$\rightarrow$	_	-	-		+-	+	+	-	+	ន	-	-
	400		_	-			<u> </u>	-	-	٠.,		-	$\vdash$	_					_		-		-	_	-	_		$\mathbf{I}$		-		-			-	┿	-	+	+	-	ន		_
	315	-	$\rightarrow$	_	_		⊢	_	╌	-	⊢	-	$\vdash$	_	-	_		-		-			$\vdash$	-	Н	-	$\vdash$	_		-		-+	+	+	+-	+-	-	+	+-	┼	92	-	-
	250	_	_			_		⊢	₽	-	┡-	┞—	-		_		_	⊢	-	-	ш	$\vdash$	-	_	ш	-	_	_	-	$\vdash$	$\rightarrow$	-	-		+	+	+-	+-	+	+	89	-	⊢
	0 200		_	_	_												-	_	_	_		_			_	_	-	$\mathbf{L}$	_	_		26 2		-	-	+	-	+	+	+	64	64	_
	160	99 /		_	_				ــــــــــــــــــــــــــــــــــــــ	L	L	_	-				-				-	_	_	_	-	_	$\mathbf{I}$		_		-	67 65	-	-	-	۰	29	-	₩	<del> </del>	┺	99	_
ies (Hz	125	56 5		26 6	-		-	-		-	-		-	-		-	_	_	-	-	_	_	-	├	-			-	_			8 8		_	-	-	2	+	+	-	-	9 89	μ.
dneuc	8	58	-		-		ļ					_	$\blacksquare$	_	_		_				_	L	_	_	-	-	-	_				88 8	-				88	-	-	-	-	99	_
er Fre	83	99	_	-1	$\dashv$		64	├	٠	-		-	_	_		-	$\vdash$	⊢	-			$\vdash$		-	-	_	$\perp$	-	_	88			-	-		+-	-	+-	+-	-	ន	$\perp$	-
n Cent	ଝ	22		-	$\dashv$		₩	_	_	_	_	_	63	_	_	<u> </u>		-	-		-		-	⊢	-	-	_	_	_	-			-	3 8	3 8	83	8	150	8	88	æ	ಚಿ	85
ectrun	<b>3</b>	54	55	28	82	જ	88	22	52	69	25	53	59	29	22	22	な	22	\$	8	88	æ	54	54	26	54	55	8	55	28	22	8 8	3 8	8 2	3 82	: KS	: 8	15	53	S	22	99	3
ive Sp	33	33	55	26	22	23	ಜ	33	8	25	49	8	26	54	53	95	51	ಜ	င္သ	င္သ	28	26	51	47	22	ક્ક	35	22	જ	8	સ્ટ	8	នន	3 2	3 2	8	1 8	25	23	51	ಜ	22	95
3 Octa	52	용	48	જ	51	20	25	47	용		8	25	54	53	20	ક્ષ		ಜ	84	ક્ષ	54	25	51	5	14	22	25	24	45	92	47	æ :	ត	3 2	2 4	8	2 88	<b>€</b>	જ	æ	47	20	45
) at 1/	ଯ	45	44	46	52	49	25	49	6		45	47	22	53		84	47	53	48	46	38	88	æ	47	46	46		25	25	46	43	S :	€ E	8 4	£ 5	£	6	4	88	8	20	43	46
L (dB	16	84	44	38	64	46	20		47	25	47	41	52	20	38	45	8	49	54		46	జ	45	44	47	47	48	ଝ	ၕွ	45			4	ŭ	2 5	54	7.4	ଓ	8	47	51	43	4
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	ಽ							4				-	53						51									Ĺ				4		<b>3</b> =		46	<u>:[</u>	41	+	45	-		Ĺ
Ba	2	4		41	46	61	6	47	4		8	<u></u>	44	<b>—</b>		6	_	4	S		25		6,	4	48	6,		S	6	44	41	ন্ত্ৰ জ	\$ 8	3 8	_	-10	, [	41		4	46	<u> </u>	┡
Mic	Pos.	Base	Base	Base	Base	Base		Base	L.		_	Base		Base	Base		1		8	Base	8		Base	Base	ä	Base	1		ŀ				Pase						Base		Base		L.
Event	Dist.	20-434		_	_	-	+-	_	-		20-434										20-434								20-434		20-434		20-434			20.434			20-434		20-434		
Event	Type	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	₩-19	₩-16	M-16	M-16	₩-16	M-16	M-16	M-16	₩-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	9 S	2 2	F 4	M 16	2 4	¥	M-16	M-16	M-16	M-16	M-16
Date	Type		5/12				_						5/12								5/12	5/12	5/12	5/12	5/12	5/12	5/13	5/13	5/13		_	5/13			2 2	_	_			5/13	-		-
9		103	±	103	103	<u>ខ</u>	53	5																					ਛ	និ	និ	<u>8</u>	3 8	3 8	3 5	3 2	3 €	<u> </u>	i E	इ	ã	<u>ខ</u>	8

Calc.	Overall SEL	73.0	75.4	77.8	70.9	72.0	72.0	71.5	71.5	72.3	73.8	75.6	70.9	72.3	73.7	70.5	73.4	71.7	79.1	83.4	72.6	85.0	73.4	76.0	76.1	76.0	74.6	76.9	73.2	74.0	80.5	1.5.1	70.0	71.2	80.8	78.2	6.69	70.9	73.3	75.1	72.0	73.6	69.2	/3.2
	20000				1		8				92									59		92						20			R				37	8								
	16000	27	83	88	R	88	27	92	52	56	S6 26	52		જ	22		92	30	36	49	26	46	56	88	83	92	28	32	23	31	£ 8	8 2	8	28	51	42	92	83	53	53	25	23	56	87
	12500		30	ន						28									43	54		23					23	25	33	35	84	ç	3		55	25	82							
	10000	23	88	37	22	8	27	8	31	31	ន	28	36		33	28	23		48	22	53	26	30	33	ಜ	32	34	33	40	42	200	8 9	<b>9</b> 8	9 8	26	26	31	28	52	ಜ	31	30	8	702
	0008	32	45	44	34	34	83	83	38	39	98	33	40	32	88	34	36	33	20	09	38	29	38	88	40	40	42	45	45	47	21	8 2	5 6	2 2	57	26	38	35	32	98	36	37	32	34
	9300	20	20	49	8	ଝ	27		45	68	36	38	43	52	42	30	34		25	63	33	61	33	41	45	43	48	20	25	49	8	38	8		69	88	\$	8		အ	33	32		8
	2000	43	54	54	45	45	41	6	46	46	45	46	49	41	49	43	43	41	23	99	47	64	46	48	51	20	23	26	51	53	5 E	€	4 S	8 F	: 6	8 8	46	47	၉	44	45	45	各	3
	4000	48	28	26	8	47	46	4	25	49	49	49	52	46	49	46	46	47	99	99	51	29	49	21	53	54	33	29	22	54	29	£ 5	23 5	7 4	5 15	3 19	25	51	45	49	8	49	47	47
	3150	25	69	29	21	49	46	45	23	54	23	54	99	48	54	20	48	47	150	99	53	0/	25	54	22	22	28	63	22	99	5	25	8 5	ج ک	6	9	જ	51	43	25	49	25	8	8
	2500	28	63	62	55	54	52	25	54	26	26	25	22	52	26	54	53	52	69	89	54	74	22	56	69	59	29	99	29	64	22	25	3 5	÷ 5	3   8	3 5	28	5	49	55	જ	26	25	23
	1250 1600 2000	⊢			_	!	_		_	⊢	⊢	<u> </u>	<b>_</b> -	-		-	-	⊢	₩	⊢	⊢	Н	⊢	Н	-	-	-	H	$\vdash$	⊢⊣		-	+	₹ 8	┿	+-	╫	₩	+	┰	┼	Н	$\dashv$	→
	160	<b>├</b>	_	Н	_	-		-		-	_	⊢	⊢	┝	-	├	-	-	⊢	-	⊢	H	┝	$\vdash$	⊢	⊢	┝	┝	$\vdash$	Н	$\dashv$	$\dashv$	+	€ E	┿	┿	+	╫╌	╁	⊢	┢	H	62	83
L		╂	H	Н	_					├	_	-	<u>                                     </u>		<u> </u>	-	-	-	├-	-			-	H	⊢	ļ	_	-		<del>  -</del>	$\dashv$	-	-+	2 4	+	+	+	+-	+-	⊢	⊢	$\vdash$		22
	1000	_	L	Ш		$\Box$		Щ	L	۰.	L	_	ļ	ļ	<u> </u>	_		_	┞-	┡	<b>!</b>	<u> </u>	┞	-	Ь.	┡	⊢	-	_		-	-+	-	22 12	+	+-	┿	┿	╄-	+	╁	$\vdash$		
	930	┺	ļ	_	_	$\vdash$		Н		-	├	├	-	₩		<del> </del>	⊢	⊢	-	⊢	-	⊢-	-	ļ	ļ	⊢	⊢	├	├-		-	-+	-	47 5 6	+	+	+	+-	+	+	-	┼	-	_
	200	ـــــ	ـــــ	$\vdash$	-	$\Box$		_		ļ		-	ļ	⊢	┡	١_	┞	┡-	٠	ļ	-	ļ		-	⊢	┞	-	┼—		-		-	-	8 2	-	-	+-	┰	+-	+-	+	+	-	_
	90		_	-		-		_		ļ	-	_	┡-	-	_	⊢	-	₩	-	-	-	-		-	⊢	╄	-	<del> </del>	⊢	-	-			æ 6	-			+	-	+-	+	+	-	-
	315	28	54	83	55	55	51	54	51	52	જ	83	21	53	22	25	54	25	ಜ	88	22	88	23	25	22	88	26	ಜ	꽃	23	25	22	8	2 23	3 8	8 2	21	23	92	25	54	29	ည	22
	220	22	8	62	22	29	29	22	29	28	88	23	54	28	8	99	8	ဆ	23	19	22	62	23	19	19	59	8	8	88	28	55	8	19	88	S &	<u>د</u> و	3 53	8	9	62	8	61	52	9
	88	╄	19	⊢	88	H	-	H	ස	⊢	┼~	┼	╄	┼-	-	⊢	-	5	ន	8	+-	┼	┼	┰	8	+	-	+-	+	+-	-	_	$\rightarrow$	8 8		+	+	+-	+-	+	+	-	-	
	9 160	8		98	59	_	09		5	8	₩	8	8	88	8	ස	8	19	┿	59	9	8		8	19	2	95	╄	5	9	Н			-+	8 8	-+-		╫	┿	+-	+	2	51	Н
es (Hz	100 125	64	65 64	70 68	63	95 66	65 65	83 83	63 64	65 61	99	89	1-	65	99 65	63	7 65	64 64	┼	3	64	99	╌	₩	╌	99	99	+	╄	62					3 8	+	+	┿	+	68 67	+-	+	47 53	99
quenci	8	99	├-	70	9	⊢	9	64 6	83	61	99	╌	62	┼	85	61	65 67	83	+	64	+	99	╄~	99	┼	┿	9 29	+	-		Ь		$\dashv$	$\dashv$	70 20			┿	┿	+-	╫┈	+-	52	$\vdash$
Band SEI (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	8	8	⊢	┼	65	├	62	├	├	83	+-	;	62	╌	-	+-	59	8	+	8	╌	25	+-	-	-	╄┈	╁	+	+	┿	Н	-			-+-	\$ 12	+	2 22		8	+	+	╀	$\vdash$
a Sel	ន	83	83	8	8	29	29	8	88	छ	æ	ಜ	83	છ	19	83	8	8	S	8	25	5	8	83	ន	8	83	8	22	22	40	83	5	22	8 2	تًا مَ	3 2	35	3 6	8	88	5	5	5
pectru	32 40	28	26	29	ಜ	22	88	83	88	52	සු	8	28	25	88	26	83	33	47	88	જ	57	83	8	8	59	ß	88	53	28	48	28	99	33	-	S &		3 8	+-	62	123	22	S	$\vdash$
tave S	32	22	+	⊢	25	₩	53	⊢	+-	23	┰	82	┼-	+	+	+	යි	+	8	+-	+-	29	+	+	╀	╫	┰	+	+	+-	-	$\vdash$	$\rightarrow$	ន	$\rightarrow$		ş (ç	+	+	+	┿~	+-	╄	$\vdash$
1/300	25	ड	25	┼	25	4	65	-	8	+-	┰	+	+	-	╄-	+-	4	4		89	+	8	+	+	+-	+-	+-	23	+	+	_	54		4	-	<u></u>		1	+	+	┿	+	╄	↤
(E)	8	_	20	+-	3 25	45	49	48	25	+	+	+-	+	+-	48	╌	+	Ļ	88	_		L	& 6	+	+-	╌	+	47	+-	<del>-</del>	£	$\vdash$	-	8	$\rightarrow$	3 8 8	3 8	+	+	40	+	+-	44 45	$\vdash$
130	13 16	41	+-	49	8	41 54	8	æ	\$	65	£	25	4	5	4	4	4	₩	47	23	4	4	88	\$	49	8	150	€ 4	8	47	4	Н	43 47	ន	201	+	+	+	r   u	7	+	4	4	
Rand	5	49	+-	4	4	46 4	$\vdash$	47	8	+	╁	╁	+	4	┞	8	4	+	+	SS.	4	+	47	+	8	8	+	+	46	+	48	⊢	51 4	$\dashv$	+	4	<del>}</del>		‡ ( <del>2</del>	+	4	5 4	82	46
Min	+	Base 4	╁	┿	+	Base 4	Base	Base 4	+	Ioù	Base	Base	Base		-la	Base 4	+-	-l a:	Rase	Base	-	Ⅎℴ	Base /	–  ա	Base 4		-1 a:	Base	Base /	-I -	Base /	Base 4	Base	Base	00 -	_	base '	Dasc		I a		┰	┿	Н.
Event		72		۰.	ட	1_	20-434		ــــ	ட	20-434	20-434	20-434		1	20-434		<u>.</u>	20.434						L.	ᅶ		20-434			<u> </u>		20-434	20-434			20-434		ㅗ			_L_	<u> </u>	
Cuont		M-16	_	_		-	M-16	-	_	_			_		_				_		_	_	_									M-16	M-16		_	_	91-19				_			
0,00	3	5/13	-	+-	-	-	-	-	-	-	+-	٠.	-		-	-	_	-	-	-	-	-	_	_	-	-	_	-	-		-	5/13	5/13					2 5	2/2	2 6	2 6	5/13	5/13	5/13
3		-	-	12	+-	+-	+	+	-	-	+	+	-	<u>≘</u>	-	-	+	-		-					-	-	+-	-	<del>-</del>  -	-	8	-	5			-+	-+	3 5	-	+	-	$\boldsymbol{+}$	-	
16	δİ	Ι÷	:   =	:12	⊣≃	⊣⊔	ا∺	⊢ا≃	۲۱≃	: I=	: 12	:  ≃	:  ¥	:  ¥	· 1=	·   <del>~</del>	-   ∓	·  =	-  `=	- I≠	- 1=	. J¥	- I <del>-</del>	-   =	- I <del>&gt;</del>	-  ∓	-   ∓	- 17	-   =	- 1=	ı=	1=	ı÷	ı == 1	<del>-</del> 1	<del></del> 1	3	- J3	- 13	-   <del>*</del>	- j÷	- 1	· 1 <del></del>	1-

Т		П			7		Γ-					П		П				_	_					Г		Γ		<u> </u>		$\neg$	Т	1	Т	Т	Т	Т	Τ	Т	Т	Τ	Τ	Γ	Τ
Calc.	Overall SEL	78.1	72.7	71.2	70.0	0.97	73.9	74.2	81.0	73.1	73.9	81.8	9.02	73.4	74.1	71.9	73.6	74.4	84.9	70.2	71.6	90.6	73.8	72.5	84.4	73.0	74.8	74.7	85.7	72.9	73.7	82.1	73.0	*: 1	90 F.	830	82.6	75.0	74.1	73.7	75.2	7.97	73.3
	2000	33							50			32						20	38					50	36				33			89		66	3 8	3 6	38	20					
	16000	20	50	ଛ		58	52	22	37	30	27	49	23	28	56	50	52	27	51	50	દ્ધ	36		23	49	8	83	8	55	52		£	/2	8 2	5 8	5 15	25	S	88	56	25	52	88
	12500	57							47			99							22			45			54	53			09			8	8 8	5 2	3 2	8 8	82	8		20	8	ន	
	1000	54	25	23		20	36		20	20	30	58	20	22	56	25	50	26	61	27	53	20	30	50	59	က	31	27	62	31	22	88	£ 5	5 8	8 8	3 &	55	4	g	30	33	37	g
	000	23	34	33	ಙ	35	41	33	28	33	38	23	32	32	32	32	31	34	65	32	37	23	36	33	83	93	88	33	99	္က	33	ا 5	4 6	3 6	8 8	3 8	- E	£	89	37	4	4	g
L	9300	ន	30	ຂ	32	33	44		29	31	39	99		59	88	27	78	32	99		32	28	37	56	64	45	43	33		42	စ္တ	23 5	\$ £	3 8	2 0	2 2	99	€ 000	88	gg	45	84	8
h	2000	59	43	43	6	43	20	43	64	43	46	61	38	43	48	40	41	45	65	Н	_	Н		-	-	┝		$\vdash$	H	ᅥ	$\dashv$	十	გ 9	十	+	+	+	╁	+	+	┢	H	t
	<del></del>	28	47	46	4	48	23	47	83	48	50	29	42	47	49	44	46	48	29	48	49	89	48	47	5	51	25	49	72	23	51	8	ន្ទ	3 8	2 14	2 8	2	1/2	25	21	22	끃	ţ
	350	29	20	8	£	25	55	20	83	51	53	65	45	49	51	42	49	25	12	21	25	63	51	84	74	83	53	51	77	22	23	2	ខ្ល	8 8	5 14	2   %	2	1 88	55	52	28	83	1
	2200	-	Н	-	-	_	$\vdash$	$\vdash$	-	$\vdash$	-		-	Н			_	_	-	Н	⊢	Н	Н	├	╌	⊢		Н	Н	$\dashv$	$\dashv$	+	5 5	+	+	+-	┿	+-	+	┿	┼	╁╴	╁
	8	29	56	54	25	99	26	54	74	56	22	73	51	53	55	25	22	28	8/	54	26	71	54	ಜ	11	ဗ္ဗ	8	RS FS	78	28	8	2/2	3 8	8 8	7 2	1	:   4	: 5	88	88	19	ន	1
	<u> </u>	65	26	55	25	26	22	53	73	22	22	73	54	25	24	52	99	28	9/	54	22	72	54	ಜ	9/	22	19	26	77	8	25	۳ ا	\$ 8	3 8	5   5	<u>,                                    </u>	:   %	8	88	83	8	83	1
	1250	8	55	22	22	22	88	53	72	22	99	75	92	20	54	51	22	돲	75	25	54	71	54	5	74	8	8	55	75	62	22	22	3 8	3 7	-   =	2   5	2 72	25	188	SS.	29	8	
	<u>§</u>	23	53	53	51	54	22	53	2	57	26	75	99	51	53	51	54	54	75	52	52	69	53	25	73	8	88	22	72	8	မ္တ	=	3 8	3 5	2 8	3 2	8	2 2	153	128	19	2	1
}	<del></del>	28	49	20	47	25	25	51	29	ક્ક	54	72	25	48	20	20	25	51	71	46	51	89	49	က	82	23	99	ಜ	69	59	જ	29	<u>.</u>	3 6	3 6	3 12	: 2	3 23	22	23	88	150	1
	89	ಜ	48	49	8	20	21	64	23	25	22	29	49	48	99	47	20	ន	29	47	49	64	20	64	29	8	23	ಜ	69	22	ន	8	3 8	<u>ا</u>	8 8	ខ្ល	3 62	2 2	SS.	49	26	88	Ī
	Š	52	51	48	46	25	S	51	22	જ	51	62	49	51	25	51	51	51	83	49	20	29	20	49	62	25	33	જ	63	25	25	5	5	3 8	3 2	5 2	ខ	3 23	2	ଞ	જ	33	
L	<u>§</u>	—	_		$\rightarrow$	$\vdash$	╙	_	_	┡-				-		-	_	⊢	_	$\vdash$		$\vdash$	⊢	-	-	-	<del> </del>	╄		_		-	\$ 6	-	-	-	-	+	+	+	+	+	+
	315	-										-	_			_		_	_	_	_	_	_	-	-	-	-	-	-	_	$\rightarrow$	$\rightarrow$	\$ S	-	_		-	_	_	-	+	+	-
	220		-	_	-		-	-	-	├-	Η-	-	-	_	_	-	$\vdash$	-	-	_	-	-	-	-	-	_	_	-	-		_	-+	3 2	<del></del> -		_	+	-	_	+	+-	+-	+
	160	7 65	-	$\vdash$		_	-	-	65 63	⊢	├	-	60 54			61 61	3 62	64 62	⊢	-	-	$\vdash$	65 61	-	-	62 57	64 63	65 62	-		-	65 69	-	-	8 2	-	┥~	-	+	-	85 83	-	4
ı		69	-	62 29	-	9 89	⊢	65	├-	65	99		63	_	_	$\vdash$	-	99	89	-	_		$\vdash$	⊢	╌	╁	99	9 29	₩-	63 61		-	-	-	8 8	-	+		+-	+-	67 6	╄	+
	0 13 16 20 25 32 40 50 63 80 100 125	8	-	Н	_	9 69	99	┞—	88	-	99		63	9 /9	9 99	⊢	9 99	29	65	-		-	9 /29	85	╄-	├	<u>6</u>	98	-		-	-	-	+	3 8	+	-+-	+-	+	+-	99	┿	4
man l	<del>-</del>	69	$\vdash$	Н	$\dashv$	88	99	-	⊢	83	├		62	-	⊢	⊢	65	98	53		-	-	┝	2		├	+	19	62	-	-	-+	-	-	2 2	-	+-	+	┰	+-	╁	+-	4
	8	19	9	62	28	88	ន	98	98	æ	54	28	8	55	65	29	49	જ	જ	8	62	88	83	8	25	ន	26	8	19	63	8	8	8	23 (2	8 8	8 8	3 2	3 2	1 15	2	छ	8	1
3	જ	62	22	69	52	23	8	8	62	83	8	ည	33	85	29	8	8	59	5	28	88	ន	8	ස	23	ಜ	ន	8	S	28	61	ន	88	¥ :	ន្ទ	ន	3 12	3 8	3 22	9	9	ಜ	:]
	8	8	25	56	54	88	88	29	65	22	28	53	_	<u> </u>	-	જ	-	83	જ	-	88	29	29	28	22	ಜ	8	88	95	22	28	22	22	3	3 3	ñ 4	5 8	-	3 6	+	+-	┿	4
lave	33	╄	ļ	23	53	88	22	├	-	55	\$	-	├	ಜ	-	-	-	22	⊢	44	55	⊢	⊢	જ	╌	25	┼	┼	જ	_	_	-	-+	-	-	₽ 1	5 2		3 2		_	4-	4
3	8	₩	⊢	8	_	22	⊢	જ	₩	9	\$	-	4	<b>├</b> ──	\$	5	├	ಜ	├	L	├	ន	├	┰	+-	┿~	+-	5	<b>_</b>	51			-	-	-+	3	1		-	-	3	+	-
up) at	<u>ম</u>	┰	⊢	$\vdash$	47	8	-	⊢	-	╄	45	8	49	<del>2</del>	L	5	9	22	25	-	88	├-	8	+	╄	+-	╌	43	£	88	$\vdash$	-	-	4	+	8 9	+		-		+		4
֡֟֝֟֝ <del>֚</del>	£	4	4	25	4	_	4	35	င္သ	4	43	45	47	<del>6</del>	4	45	S	\$	49	44	88	4	£	55	46	8	4	ន	├	જ	43	\$	<b>₽</b>	$\dashv$	- ;	} {	+ 4	7 7	3 8	4	41 47	+	+
	<del>+</del>	$\vdash$	_	44	41	L	$\vdash$	4	47	9	$\vdash$	L	જ	41 41	47	22	-	$\vdash$	H	┞	4	4	┞	$\vdash$	4	8	4	$\vdash$	┝	4	H		æ	$\dashv$	+	+	╀	+	1	+	4	╀	7
S S		Base	Base	Base 4	Base 4	Base	Base	Base 4	Base 4	Base 4	Base	Base	-	╌	-	Base	Base	Base	Base	Base	Base 4	<del>!</del> —	Base	Base	Base 4	+	+-	Base	Base	Base /	Base	Base		Base	Base	Pase	Dase	Baco	Race /	_ a	Base	Base	2000
Event	Dist.	20-434	20-434	20-434	20-434	20-434	20-434	L	20-434	20-434	20-434	20-434	20-434	20-434	20-434		20-434	20-434		20-434	20-434	20-434			20-434				20-434				_	_	_			20.434		20 434	_		_
Event	Туре	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	M-16	91-10 ₩-10	9-12 ¥-12	2 4	- Y	M-10	M-16	¥-16	M-16	2
Col. Date Event		5/13	-	5/13	5/13	5/13	5/13	-	-	5/13	5/13	₩-	5/13	5/13	5/13	5/13	5/13	5/13	5/13	╄	5/13	-	5/13	+	-	+-	┿	-	-	5/13	5/13		_	-	-	_	2 5	-		-			4
-		55	-		103	₩	55	╌	+	+	┿	5	┿-	+	<u>≅</u>	±	5	53	5	╌	<u>≅</u>	+	-	+-	+	+	+	+	+-	+	53	-	-	-	-	2 8	-	3 5		-	-	-	-

10000   12500   16000   20000   OV	$\dashv \dashv$	23
25         25           26         25           26         27           27         27           28         27           29         26           29         27           29         27           20         23           20         23           20         23           20         26           20         27           20         29           20         26           20         26           20         26           20         26           20         26           20         27           20         27           20         26           30         37           20         27           20         27           30         37           20         27           20         27           20         27           20         27           20         27           22         20           23         27           24         27           25         <	25 25	$\vdash$
25         25           26         25           26         27           27         27           28         27           29         26           29         27           29         27           20         23           20         23           20         23           20         26           20         27           20         29           20         26           20         26           20         26           20         26           20         26           20         27           20         27           20         26           30         37           20         27           20         27           30         37           20         27           20         27           20         27           20         27           20         27           22         20           23         27           24         27           25         <	$\dashv \dashv$	ξ.
26 28 29 29 29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	37	1
10000 100000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 1	2 3	-
▎┞ <del>╸┆┆┊┆┆╎┞┆┆┆┆</del> ┼ <del>┆┆┆┆┆</del>	1 1	
8000 8000	34 44	27
	51	34
6300           6300           6300           6300           6300           6300           6300           6300           6300           6300           6300           6300           6300           6300           6400           650	Ÿ 4	88
5000           5000           5000           5000           64           44           43           45           46           47           48           49           40           64           64           64           64           64           64           64           64           64           64           64	58	55
4000 4000	59 54	84
	65 56	ß
250 250 250 250 250 250 250 250 250 250	88 88	33
! <del> </del>	88	299
1600 1600 1600 1600 1600 1600 1600 1600	88	129
128	67 83	25
100 100 100 100 100 100 100 100 100 100	8 8	52
88       98 <td>88</td> <td>╁</td>	88	╁
630 530 530 530 530 530 530 530 5	╌┼	+
500         500 <td><del> - -</del> </td> <td>+</td>	<del> - -</del>	+
315 40	<del>}                                    </del>	
25		+-
200 200 200 200 200 200 200 200 200 200	28	3 6
5         18 </td <td>+</td> <td>_</td>	+	_
	┿	
66         69         67           66         69         67           66         69         67           66         66         66           67         69         67           69         69         67           69         67         69           69         67         69           69         67         69           69         67         69           69         67         69           69         67         69           69         69         67           60         69         67           60         69         69           60         69         69           60         69         67           60         69         67           60         69         69           60         69         69           60         69         69           60         69         69           60         69         69           60         69         69           60         69         69           60         69	+	-
Ar Frequency         Ar Frequency           Ar Frequency         Ar Frequency		-
10 Center Fig. 10 Cen	<del>                                     </del>	-
Company         Company <t< td=""><td>++</td><td>5 5</td></t<>	++	5 5
83 85 85 85 85 85 85 85 85 85 85 85 85 85	<del>-1</del>	-
25 29 29 29 29 29 29 29 29 29 29 29 29 29	64 84	9 9
ag       20       48       48       48       49       40 <td>9 6</td> <td>ş ç</td>	9 6	ş ç
11. (dB)	25	2 2
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies (H2)           0         13         16         20         25         32         40         50         63         80         100         128           4         48         48         48         57         56         61         64         65         66         69         67           0         53         48         48         57         56         61         64         65         66         69         67           0         52         45         56         57         57         62         63         66         65         66 <t< td=""><td>11-</td><td>1</td></t<>	11-	1
	يوايو إ–	8
Nic   Post	1	١
Event (m) 50-434 (20-434) 20-4	$\overline{}$	
M-16 M-16 M-16 M-16 M-16 M-16 M-16 M-16		
	5/13	5/13
Date           5/13	وماريمار	<u>ක</u>

And September 19	T <sub>=</sub>				T	Τ	Τ	T	T	T																		I			$\prod$						T	T.					$ \begin{bmatrix}                                   $	
12   12   12   13   14   15   15   15   15   15   15   15	Overa	SEL	71.2	75.8	77.	72.3	80.1	78.9	70.5	70.5	78.2	21.7	71.5	74.5	72.1	70.2	84.4	82.8	74.5	75.5	71.8	71.5	77.8	72.8	76.8	63.5	6.99	74.0	74.2	71.2	74.9	70.1	75.6	73.0	72.2	75,	7.0	73.1	/5/	73.8	73.1	73.6	83.8	75.0
1,	2000	2000			5	3	33	3		20						20	34	59							23						23											ŀ	æ	
1 (a) (a) (a) (a) (a) (a) (a) (a) (a) (a)	16000	20001		<u>ج</u>	97	₹ 8	27	£	8 8	83	32	25	25	27	56	27	47	47	35	20	23	23	32	28	88	25	88	52	23	8	31	26	83	83	ន	3 8	3 3	3 23	77	83	83		46	82
1 (a) (a) (a) (a) (a) (a) (a) (a) (a) (a)	12500	3		88	Ş	g-	5	5 64	,		99	20					55	22	43		33		8		88						99	,	88	1						R			22	88
18	-		20	£ 5	20 2	# S	3 12	3 4	) (8)	20	44	35	32	56	28	27	22	57	47	32	38	31	33	30	93			32	8	22	9	23 2	S 13	3   S	27	5	3 8	23 25	3 3	98	52	83	19	46
18   18   18   18   18   18   18   18	-		28	æ	3 8	8 8	3 82	3 2	   & &	ا 8	48	41	38	36	34	30	61	61	52	39	44	9	45	37	46	32	27	37	32	38	49	R)	14 6	<u>چ</u> او	25 25	25 65	3 3	¥ 6	ş !	45	34	용	23	22
Fig. 200   250   315   400   500   630   600   1000   1250   1500   2500   315   400   5	1		53	ф ф	9 8	3 8	} 2	5 45	+-	T	54	48	41	88	36	33	61	64	54	<del>-</del>	44	5	22	33	£9			ន	ន	4	8	8	45	3 8	8	\$ 3	‡   {	র :	<del>1</del>	£	ន	္က	·	54
Fig. 1200   250   315   400   500   1000   1000   1200   1000   2500   3150   4000   1000   1000   1000   1000   2500   3150   4000   1000	$\vdash$	一	42	25	ۍ ا ا	၉ ဗ	2 2	3 6	1 24	<b>\$</b>	26	51	48	47	46	44	99	62	61	<b>유</b>	æ	<del>6</del>	5,	46	28	93	eg eg	44	£	5	82	=	25	£ :	4 6	3 6	٩	3 6	2	8	<del>-</del>	<b>왕</b>	8	57 L
140   200   250   315   400   500   650   650   100   1250   1250   15	$\vdash$		45	25	₹ Z	- E	3 8	3 8	8 8	55	59	28	20	20	20	48	65	68	88	22	8	ည	22	20	23	89	용	& &	6 <del>5</del>	& &	8 I	5	Z	3 9	& i	\$ 12	5 5	æ  :	24	83	&	47	<u>و</u>	88
60         58         56         44         50         60         100							+	+	+-	╁		-	-				_	_	-			$\dashv$	$\dashv$		$\dashv$		-	-	-	-+	-+	-+	-+	+	$\dashv$	-+-	-+	-+	+	$\dashv$	-+			
160         200         280         315         400         630         630         100         120         150         200         100         120         160         200         100         120         160         200         100         120         100         200         100 <th></th> <th></th> <th>25</th> <th>25</th> <th>8 3</th> <th>\$ 8</th> <th>3 8</th> <th>2 82</th> <th>8 8</th> <th>25</th> <th>8</th> <th>65</th> <th>22</th> <th>55</th> <th>54</th> <th>54</th> <th>77</th> <th>9/</th> <th>29</th> <th>83</th> <th>99</th> <th>28</th> <th>99</th> <th>22</th> <th>99</th> <th>4</th> <th>4</th> <th>ಜ</th> <th>જ</th> <th>ន</th> <th>-</th> <th>8</th> <th>8</th> <th>8</th> <th>ន</th> <th>3 2</th> <th>5 1</th> <th>8</th> <th>2</th> <th>8</th> <th>22</th> <th>ន</th> <th>22</th> <th>83</th>			25	25	8 3	\$ 8	3 8	2 82	8 8	25	8	65	22	55	54	54	77	9/	29	83	99	28	99	22	99	4	4	ಜ	જ	ន	-	8	8	8	ន	3 2	5 1	8	2	8	22	ន	22	83
160         200         250         315         400         650         650         160         120         120         120         120         120         120         120         120         120         160         120 <th></th> <th></th> <th>25</th> <th>29</th> <th>8 8</th> <th>8 8</th> <th>3 18</th> <th>2 5</th> <th>: 8</th> <th>ಜ</th> <th>2</th> <th>26</th> <th>29</th> <th>22</th> <th>22</th> <th>99</th> <th>78</th> <th>9/</th> <th>99</th> <th>8</th> <th>23</th> <th>29</th> <th>- 62</th> <th>26</th> <th>29</th> <th>4</th> <th>4</th> <th>ន</th> <th>22</th> <th>22</th> <th>8</th> <th>83</th> <th>8</th> <th>8</th> <th>ន</th> <th>\$ S</th> <th>8</th> <th>8 8</th> <th>ន</th> <th>88</th> <th>32</th> <th>22</th> <th>F</th> <th>8</th>			25	29	8 8	8 8	3 18	2 5	: 8	ಜ	2	26	29	22	22	99	78	9/	99	8	23	29	- 62	26	29	4	4	ន	22	22	8	83	8	8	ន	\$ S	8	8 8	ន	88	32	22	F	8
1460   200   250   315   400   500   630   800   1000			25	29	8	8 2	5 14	2 5	: 8	54	8	22	09	28	59	56	9/	74	65	99	5	99	- 62	23	89	5	45	ន	28	£	29	ន	9	န္တ	22	8 [	6	3 23	۾	8	32	ន	11	8
160   200   250   315   400   500   630   800	1250	200	25	29	3 2	۵ ۵	3 8	7, 02	22	55	69	28	29	28	28	26	74	72	ဗ	61	61	28	68	19	89	45	£	22	22	22	22	23	:S	2	22	3 8	g	S (2	8	8	32	54	~	93
160   200   250   315   400   500   630       60   58   56   54   51   54   50   630       61   62   61   63   65   64   67   64   62   61   64   62   61   62   64   62   61   62   64   62   61   62   64   62   61   62   64   64	90	3	53	29	3 2	و م	3 2	- g	25	55	29	28	59	26	57	56	74	69	61	61	99	26	89	09	99	47	48	\$	92	ន	8	25	8	Z,	ន	ន	ន	8	3	5	22	જ		64
160   200   250   315   400   500	-	_	Н		+	-	┰	┰	+-	-	╄	_	-				_	-	_		_	$\vdash$	-	$\vdash$	$\overline{}$	$\vdash$	$\rightarrow$	$\rightarrow$	-	$\rightarrow$	-	-		-+	-	-+	-	-+			-	-		
140   200   250   315   400   140   200   250   315   400   140   250   250   315   400   250   315   400   250   315   400   250	_	$\overline{}$	_	_	-		-	_	┷	+-	-	┺	-		_	_				_		-	_	ш	-	-	_	-	-	_	_	-+		-	$\rightarrow$		-		-	-	-		-	
160   200   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250   315   160   250	_		-	$\rightarrow$	-	-	-			4-	╄	₩		_				├	$\vdash$	-		_	$\vdash$	$\vdash$	_	-	-	$\rightarrow$	-	-	-	-	$\rightarrow$	-		-	-	-+	-+			$\rightarrow$		-
160 200 250			ш	_				-	-	-	₩	_	_		_	_	_			_	-		_	-	-	-	$\rightarrow$		-	-				-	$\rightarrow$			-	-	-	-	-	-	-
20			Н	$\rightarrow$	-	-	-	-	-	+	┿	⊢	-	-	-	-	⊢	$\vdash$	Н	Н	$\vdash$	Н	Н	Н		-	-			-	-	-+	-+	-	-+	-	-+	-	-	-	-		-	$\vdash$
	8	3	28	28	25 5	3 8	8 %	3 4	9	:S	23	22	28	62	69	25	အ	19	26	ೞ	25	28	63	61	61	51	26	29	83	83	೫	23	8	8	83	8	5	8	8	8	61	29	8	27
30 Crave Spectrum Centler Frequencies (Hz)           25         32         40         50         68         80         100         128           50         54         58         69         62         63         80         100         128           51         53         56         59         64         63         65         64         66         66           43         52         51         49         53         55         55         56         64         66<	_	_	_		-	-	-	-	-	+	╄	<del> </del> —	-	-	_				Н	Н			-	-	-	$\vdash$	$\vdash$	$\dashv$	-	-	-			-	-+	-	-+	-	-		-		$\vdash$	9
3 Octave Spectrum Center Frequencie           25         32         40         50         68         60         100           26         32         32         40         50         68         60         100           50         54         58         59         62         63         60         100           49         53         56         66         66         63         66         67         68         68         69         60         100         60	125		Н	$\dashv$	-	-		+	+	+-	+	-	⊢	_	Ξ	-	_	⊢	Н	Н	$\vdash$	$\vdash$	-	$\vdash$	Н-				Н	-	-	-1			-	-+	-+		-	-	-	-	$\vdash \vdash$	83
3 Octave Spectrum Center Frequency Spectrum			⊢	$\vdash$	-+				+	+-	+	⊢	⊢	Н	H	⊢	┝	⊢-	$\vdash$	Н	$\vdash$	$\vdash$	_	-	_	$\vdash$	-		-	$\dashv$	$\rightarrow$	-	-	-	-	-+	-	-+		-	Н	-	$\dashv$	62 62
3 Octave Spectrum Central Spectrum Centr	2 8		-		$\rightarrow$	-	-		┩	-	+	ļ	├	_	-	_	⊢	├	$\vdash$	Н	-		-	Н	$\vdash$	Ь	Н	₩		-	$\dashv$	-		-	-	+	-	-+		-	Н	_	-	61 6
3 Octave Spectrum 5 of the page 1 of the page 2 of the page 3 of the page 2 of the page 3 of the pag	2 2		-	-			+	+	+	+	╌	⊢	-	├-	-	├-	-	-	-	-	$\vdash$	-	-		-	Н	Н	Н	Н	-				-	-	-+	-+	-+	-		Н	$\vdash$	88	$\vdash$
3 Octave S <sub>3</sub> 20 Ctave S <sub>4</sub> 20 Ctave S <sub>5</sub> 20	8		28	26	25	5 5	8 2	8 8	3 8	223	8	æ	22	98	55	ಜ	29	22	53	59	99	5	8	55	22	49	84	25	28	99	38	જ	59	න	22	25	۾	5	22	83	85	28	29	51
20 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	32	ž	24	53	83	3 5	8 2	3 8	3 8	ន	55	છ	53	88	55	49	26	54	21	53	25	25	⊢	-	⊢	47	50		-	-	44	54	57	જ	-	-		-	-	-	-		$\vdash$	21
	3   S 2   –		-	⊢	-	-	-	+	+	+-	4-	-	⊢	-		⊢	⊢	├			╌	_	-	-	-		Н	Н	Н	-	Н		-1	-	$\rightarrow$	-		-+			-	45	용	-
1 1 2 2 4 3 4 5 4 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5	ا <u>ا</u>		-	╌	-+	-		+		+	+	4	+	⊢	⊢	⊢	⊢	⊢	-	$\vdash$	⊢	⊢	┡	-	├-	8	┝╌┤	<b>├</b> ─┤	$\vdash$	Н	Н	_	Н		-	$\dashv$	-			-	-		Н	7 47
SEL (dd SEL (d	3 1		₹.	4	4	ŭ	+	+		1 4	4	┝	4	4	क्ष	4	⊢	4	4	4	4	4	4	5	2		25	4	-	4	2		4	-	2	2	₹	22	4	_	Н	4	4	47
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			$\vdash$	$\vdash$	$\dashv$	-	2 2	+	+	+	83	╁	┝	┝	8	=	├	4	$\vdash$	-	23	94	4	=	-	H	Н	H	"	S S	25		4	-	14	မ္	4	င္ယ	47	44		44	46	49
	╁		Base	Base	Base	ωŀ	-		υ <b></b>	ᆔᅇ	-	Base	Base	Base	⊢	⊢	⊢	⊢	Base	Base	⊢−	⊢	⊢	⊢	Base	Base	Base	Base	Base		_	Base	_	Base	┝	-	-	-		$\vdash$	Base	$\vdash$	Base	-
. 1	Diet	E)	20-434	20-434	20-434			i_	20.434	20-434	20-434	20-434	20-434	20-434	20-434	L		┖-	20-434	20-434	<u> </u>			<u> </u>	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434
	T VEIL		+-			-	-	_		-	_						_	+	+					_	_	_														į			M-16	
			-	-		-	-	-		4-	+	+-	-	-	-	⊢	╄	-	-	-	-	-	_		₽		⊢	-	-		-		-		-			_		_	-			-
			+-	-			-	— <u></u>		<del></del>	-	-	+		<del>-</del>	-	┼	┿	+-	-	<del> </del>	+	-	+	╄		-		+	₩				_	-	-		_	_	_	<del>!</del>	-	-	55

_																F		<del>-1</del>	-				-	_					_		_	<b>-</b> T			_	_	T	1	Т	1	Т	т-	Τ		
Calc.	Overall	7.77	82.0	71.9	72.1	82.9	72.2	72.3	73.8	71.6	72.4	72.5	9.89	72.2	75.1	74.0	74.6	7.17	78.6	70.1	82.2	74.6	80.7	83.7	71.4	70.6	71.8	72.6	76.9	69.7	73.4	70.3	2.69	100	71.7	73.7	75.0	68.8	70.8	73.4	73.3	72.2	78.0	70.8	
	20000		59			44									ล			į	50		25		83	83					20					8	3									82	
	16000	S	43	52	56	47.	22	31	8	59	30	29	27	ଷ	88	S	27	83	£	27	44	88	88	44	ន	52	52	g	es Si	8	ន	ន	3 33	7 2	ខ្ល		30	20	32	27	ន	27	ೱ	ន	
	12500	39	52			55			ន			27			ន		8	,	₽		23		47	49	83			S3	42							20			32	20			38		
		64	55	56	27	61	53	22	34	20	31	39	23	္က	88	32	98	88	84	92	22	34	54	54	99	83	34	35	46	50	83	g g	8 8	8 2	5 8	33	23	23	45	88	33	T	45	32	
	 0008	26	22	32	33	63	88	37	41	೫	37	45	25	99	43	8	£3	35	54	8	eg Eg	42	22	88	42	ಜ	41	45	22	32	37	32	ន	3 9	3 €	ę.	3 8	32	S	4	88	32	25	38	
	9300	જ	8		83	64	54	æ	44	62	န္တ	S		42	8	8	S	g	83	ဗ္က	8	46	8	83	48	ឌ	4	47	28		98	ဆု	8	₹ !	3 6	4	-	Γ	22	8	4	98	88	42	
	200	8	62	43	42	64	49	46	25	41	46	52	34	49	SS S	47	23	46	62	4	8	51	83	29	25	41	49	51	28	39	45	43	32	8	<del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del> <del>2</del>	20	8 44	88	25	5	48	44	55	20	
	900	83	59	84	47	99	25	51	54	46	25	24	37	25	24	25	જ	8	99	45	8	25	29	69	22	46	21	54	61	43	49	8	육 :	€	가 &	2	2 64	4	23	8	3 5	47	8	51	
	3120	83	64	ಜ	64	88	88	53	22	45	25	88	37	22	22	SS S	33	<b>₽</b>	2	45	73	29	89	02	22	84	53	28	99	45	25	င္သ	33	\$	3 B		3 62	45	2 2	3 2	3 27	2	8	29	
	5200	29	2	22	83	8	8	26	26	51	22	8	53	25	23	22	ន	72	71	25	9/	64	29	72	8	21	55	09	99	51	54	જ	<b>₽</b>	\$	8 2	: [8	3 6	55	3 8	3 2	£ 5	12	8	88	
	2000	7	74	52	ಜ	75	8	22	19	ಜ	88	ස	46	22	ន	5	29	24	7	51	74	65	71	73	5	25	නු	99	83	52	29	S	4	£	25	: [2	3 %	2	: 8	3 8	3 12	54	5 ~	28	
ļ	1600	8	E,	æ	54	92	29	82	အ	54	8	29	44	29	64	82	67	33	8	51	7	99	72	75	61	25	22	61	64	22	22	28	3	₽ P	52	3	2 82	2	84	£ 5	3 2	3 5	3 8	ස	]
	1250	8	22	RS FS	않	22	83	23	အ	52	8	5	46	8	65	82	ន	23	29	51	8	99	72	77	28	21	29	19	88	57	25	25	47	£	88 Z	5 8	2 E	2	; E	3 8	3 8	3 4	3 8	8	
	1000	8	7	£	끃	23	26	82	9	53	ස	25	S	29	65	90	64	29	ß	52	22	63	73	76	58	53	22	æ	29	22	22	55	49	65	27	3 2	9 4	3 2	5 g	3 2	5 8	3 15	3 6	ස	
	800	53	72	25	ន	F	ಜ	22	22	25	26	8	42	28	62	28	23	조	8	51	23	29	╙	-	۰	20	-	<del> </del>	╄	-	54	$\vdash$	45	4	¥ 8	3 8	8 2	5   9	2 2	3 12	2 6	; [2	3 8	25	
	630	88	┰	4-	╀	8	<b>-</b>	╌	⊢	23	+-	+	-	<del></del>	-	_	-		$\overline{}$	Н		├	├	-	⊢	84	_	-	⊢	┯	╄	-	Н		ස   ද		-		7 2	+	+	5 9	+-	+-	┨
	200	83	+-	+-	₩	╄	-	52	-	+	+-	+		╀-			-	$\vdash$	$\vdash$	Н		┼	⊢	-	⊢	33	<u> </u>	-	⊢	+	╁	<del> </del>	┝╼┥	$\dashv$	22	+	2 2	+	+-	┰	+	+	+-	+	1
	315 400	+	88	+-	┰	+-	┰	55	╄	28	+-	+	+	⊢	├		Н	Н	⊢	53 51	_	┈	⊢	╄	├	54	-	╄—	╄┈	┼	├-	├	54 4	_	2 2	+		+	+	-	8 4	+	+	+	1
	250 31	+	61 5	┼	_		_	58	_			_	-	٠		_		$\blacksquare$	╙	-		-	┡	-	⊢	٠	-	-	╄-	-	╄	⊢	8	_	59 8	-	-		+		+	+	3 8	┿	┨
	200	85	-	-	88	╄	+	┿	_	┵	-	-	4	-	_			_	⊢	22	┝		٠	+	-	25	-	-	-	-	+-	-	19	23	8 8	3 8	3 2	5 2	5 2	5 S	8 8	3 8	8 8	3 123	1
	160	+	8 8	+	15	+-	82	-	+	8	+		+	-	8		-	-	_	-	_	<b>→</b>	-		-	23	-	-	-	-	+-	-	-	29	8 2	5 3	5 6	5 8	၉ ရ	3 8	3 2	5 8	3 &	25	1
£		8	8	50	ន	83	5	83	63	62	62	62	8	19	ន	အ	8	19	64	ន	19	ಜ	အ	64	8	62	8	9	49	-	_	-	_	_	ន	_	_		5 8		-	5 3	\$ E	-	4
Band SE1 (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)	8	79	98	83	84	╄	29	+-	╄	ន	-	-	8	┰	-	⊢	2	╄	25	-	-	-	-	-	┿-	8	-	-	+	+-	+	٠	┅	_	8	-	-	-	<u>ء</u> ا	-	8 8	-		8 8	_
Freduc	8	- 2	_	┷	4-	╄~	-		+	ន	-	4-	5	-	<del></del>	┡	⊢	-	-		_	_	_	26	_	_	┿	છ	+	8	-		-		£ 8	-		-	-	4 8	+	5 8		3 23	-
enter	ន	-	3 2	+	+-	+-	+	-	╄~	8	+	88	+-	8	╄	-	8		9 65					62		58			_	_	-	-	-	-	61 64		8		-	⊋ {9		2 8		9 95 8 95	-
frum	40	┿	5 E	+	25	+-	4	<del></del>	+	57 59	+	-	_	-	60	₩	53					-	-	_		54	-	_				-	51 5		${}^{-}$	-+	8 8	-	-	-+	-	-	2 2 2 2	_	4
Spec	32	-	9 9	+	<del>-</del>	+-	+	-	+-	: K	-	-		-	-	-	₩-	-	╌	8	-	_				5	_	_	_	_	-	+			83	-+	-	-		-	25	-	-	3 8	-
Octav	52	-	t 8	-	_	123	-	20	-	-	+	48	-	47	-	-	-	₩	-	88	╄-	+-	+	+	63	_	25	-	_	5 8		_		42	$\vdash$	-+	$\rightarrow$	8		1	\$ 5	₽	38 6	\$   E	;
at 1/3	ଛ		F 8	+	+	+-	+	<u>ස</u>	╂			₹ 4	-	-	-	-	-	-	-	8	-	-	-	47	4	8	4	6	8	8	2	23	8	46	9	2	21	4	1	25	4	3	\$ 8	ક્ર જ્	إ
(AB	9	ę	2 8	3 8	54	6	व	8	54	84	5 8	2 2	74		47	47			46	<b>&amp;</b>	14	84		ß	22	8	84	21		2	1 2	46	47	21		4	88	3	89	8	9	3	4 5	8	
Spue	55						Ι	47	4		41	_												41				$\perp$	L	$\perp$	45	-		L	4			4				_	4	$\downarrow$	4
L	Γ.	ę	£ 5	3 4	1		+	: 9	+		-	—  ი	واي	و ا	يو	1	J 05			23	-	+-	8	_ 0	12	_	ے ا	ر پو ا	8	_ 1 ~		_	25	g	48	_	as L	4		ο ŀ	₩	-+	-	\$ 2	-
$\vdash$	Pos.		Base	1.							1		1	L	Base	m		۳				_	_L_		ľ	- 1		Base	ď		à			4 Base	iI	ä		1	8	Į				4 Base	
+ Event			20.434	_						_			20.434									_		8 20-434	20.43	8 20 434	20.43							6 20-434			6 20-434			$\overline{}$	$\overline{}$	_	-	6 20-434	
Fyton	좚		2 2 2		_	M.16	-	_	_	_	_	_	2 4	_	_			-		-	-	_				M-16		_	_	_				M-16		M-16	_	_	_		-	_	_	W-16	_
5		9	5/13	5 6	3 5	2/13	2 6	2 13		2 2	5 6	2 2	2 2	7 2	5/13	5/13							2 2	2/3	2 5	5/43	2 6		_	_		_		_		_	5/13			_				5/13	_
3		1	3 5	3 5	3 5	3 8	3 8	3 5	3 2	3 5	3 5	3 5	3 5	3   5	Ē	Ē	Ē	ā	3	3   2	3	3   2	3   5	3 2	3 2	3 5	3 5	3   5	3   5	3   5	3   §	3   2	<u> </u> සි	503	5	53	<u>ස</u>	ន	ន	ន	සි	흅	<b>≅</b>	සි ්	3

	Salc.	Overall SEL	72.4	73.6	87.2	70.2	70.4	6.08	83.9	78.2	73.6	71.9	72.6	72.4	81.5	70.3	9.69	83.7	0.77	73.8	70.2	68.3	71.9	70.0	73.4	9.69	73.0	73.2	70.8	72.7	71.5	77.3	68.4	81.4	84.0	79.1	72.2	76.3	72.6	76.3	79.0	74.0	78.3	73.5	83.4
	4		H					_	_		-		-			)			0					-																			$\dashv$	-	
1	ŀ				84			83	31	-		8			28	50		25	50		-	_										92				_							$\dashv$	4	82
1			92	26	29	ຮ	50	34	43	34	ន	53	32	22	49	30	23	45	28	ន	92 26	ន	ន	58		50	52	28	50	27	23	3	ଷ	34	88	83	34	34	29	59	38	ස	ଛ :	ଛ	8
		12500		52	64	ಣ		45	52	43		31		50	22	34		51	22									20				40		34	43						45	37	22		48
No. 10.   No.		0000	50	34	65	32	20	20	57	47	53	33	34	28	09	49	25	26	35		8	23	52	23	29	22	36	28	56	56	20	47	92	5	20	37	35	33	36	32	41	40	8	22	ន
No. 1985   No. 1985	İ	000	32	42	88	99	30	20	8	51	37	44	40	36	64	51	32	28	43	31	37	23	33	- 82	37	೫	41	34	34	37	33	54	ജ	25	28	4	9	42	40	43	47	46	₹	8	22
14   15   15   15   15   15   15   15		930	30	45	7	<del>6</del>		25	64	22	40	48	43	45	99	20		2	47			ຂ	8	22	38		45	37	38	40		8		ક્ષ	83	46	4	45		41	23	ည	\$	ස	8
1		2000	44	51	20	49	42	65	68	55	48	ಜ	49	46	67	48	37	61	53	42	47	జ	44	38	47	40	52	44	43	47	42	9	89	5	65	54	49	51	46	51	28	57	83	49	88
1	ľ	900	46	25	72	22	45	09	89	2	51	52	52	51	2	23	41	2	26	47	ន	£	64	44	25	44	54	48	48	52	46	29	£3	8	99	8	\$	54	20	25	8	83	8	22	71
		3150	25	29	11	ន	47	69	69	ន	54	22	26	29	73	99	40	72	61	<b>Q</b>	ន	4	꼬	4	72	45	22	49	49	22	20	65	£	88	2	5	ß	22	4	28	83	88	5	83	2
			25	8	8	28	21	73	74	88	29	28	22	29	74	52	46	74	63	54	8	25	92	ည	28	25	29	54	54	61	53	69	25	8	23	64	29	09	26	61	99	8	8	23	5
Marco   Marc		2000	29	ස	81	8	54	2/3	9/	17	9	8	29	29	73	59	47	76	64	99	28	25	28	25	09	53	22	55	22	62	53	70	2	=	77	29	9	61	22	61	89	29	8	5	5
1.   1.   1.   1.   1.   1.   1.   1.		<u>8</u>	09	64	9	62	22	72	11	73	ೞ	61	62	28	72	61	49	76	99	28	22	ន	22	5	19	53	58	55	26	62	54	69	<del>0</del>	23	77	89	8	9	99	62	69	64	8	8	1,1
This continue was a			29	83	77	9	22	22	11	88	62	62	63	28	69	62	20	75	29	22	22	25	32	51	-61	51	09	99	25	19	54	89	ည	23	76	99	90	09	28	19	<b>29</b>	61	ន	<u></u>	74
This   This		900	28	09	74	8	54	0/	75	29	9	09	62	99	69	59	51	73	99	22	28	22	જ	52	61	53	60	56	58	60	54	67	51	72	75	8	58	61	28	19	<b>29</b>	61	83	8	5
913         Mile         700         Mile         70	- 4		54	92	33	83	51	69	20	ន	88	88	29	53	89	56	48	7	ည	99	ಜ	S	22	25	28	21	28	54	99	99	25	62	8	88	r	ន	22	28	26	22	64	22	9	83	5
No.   No.	- 1		25	\$	8	54	49	99	89	88	22	24	အ	21	99	25	51	8	8	83	<u>දූ</u>	<b>₽</b>	င္သ	<del>6</del>	22	49	22	25	25	23	20	28	47	2	99	8	55	99	54	25	9	ន	8	22	ž
Yield         Wield         Yield         Nick         Nick         Yield         /td> <td></td> <td>ន</td> <td>24</td> <td>88</td> <td>8</td> <td>20</td> <td>မေ</td> <td>54</td> <td>28</td> <td>54</td> <td>24</td> <td>\$</td> <td>51</td> <td>99</td> <td>22</td> <td>55</td> <td>ន</td> <td>61</td> <td>29</td> <td>22</td> <td>33</td> <td>જ</td> <td>25</td> <td>22</td> <td>21</td> <td>99</td> <td>54</td> <td>53</td> <td>53</td> <td>25</td> <td>88</td> <td>\$</td> <td>ន</td> <td>ន</td> <td>8</td> <td>23</td> <td>29</td> <td>22</td> <td>28</td> <td>62</td> <td>8</td> <td>8</td> <td>ક્ક</td> <td>20</td>	- 1		ន	24	88	8	20	မေ	54	28	54	24	\$	51	99	22	55	ន	61	29	22	33	જ	25	22	21	99	54	53	53	25	88	\$	ន	ន	8	23	29	22	28	62	8	8	ક્ક	20
TYPO         (MI)         CAPACITY         CAP	L		Н	-	-		-	_	-				-	-			-	-									_		_	H	$\vdash$	Н	_	-			_	Н	_	-	-		-	$\dashv$	L
Type (m)         (m)         Post (m)         (m)         Post (m)         (m)	- 1		╌				-		-	⊢	1	⊢	$\vdash$	$\vdash$	Н		$\vdash$	-	ш	-	$\dashv$	$\dashv$	$\dashv$	-	$\vdash$	-	$\vdash$	$\vdash$	$\vdash$	$\perp$	Н	Н	$\dashv$		_	_				$\vdash$	-	-	-+		H
Type (III)         Name (III)         Type (IIII)         Name (IIII)         Name (IIII)         Name (IIIII)         Name (IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	L.		-	-	-		_	_		┝	$\vdash$	⊢	$\vdash$	-	$\vdash$	$\vdash$	$\vdash$	-	$\vdash$		_	_	-		ш	$\overline{}$	$\vdash$	Н	ш	-	Н	Н	-	_	_	-	-	_	-	$\vdash$	-		-	-	H
Type         (m)         Page         47         51         52         53         40         50         60 <t< td=""><td></td><td></td><td>-</td><td>_</td><td>-</td><td><math>\dashv</math></td><td></td><td></td><td>-</td><td>-</td><td>-</td><td>├</td><td>-</td><td>_</td><td>_</td><td></td><td>-</td><td>-</td><td>_</td><td>_</td><td><math>\rightarrow</math></td><td>-</td><td>-</td><td></td><td></td><td></td><td>-</td><td>-</td><td></td><td>-</td><td>_</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td>_</td><td></td><td>_</td><td>_</td><td>-</td><td>-</td><td>-+</td><td>H</td></t<>			-	_	-	$\dashv$			-	-	-	├	-	_	_		-	-	_	_	$\rightarrow$	-	-				-	-		-	_				_			_		_	_	-	-	-+	H
51/13         M-16         20-434         Base         44         77         51         55         57         56         59         63         60         60         70	ı		₩		-	-	-	_	_	├	-	-	-	⊢	Н	_			-	-					$\vdash$		-	-			$\vdash$	Н	-				_	_	_	_	-	$\vdash$	-	-	L
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>ZU) CA</td> <td><u>8</u></td> <td>-</td> <td>_</td> <td></td> <td></td> <td>_</td> <td>_</td> <td>-</td> <td>├</td> <td></td> <td></td> <td>-</td> <td></td> <td>_</td> <td></td> <td>_</td> <td></td> <td>-</td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td>Н</td> <td><math>\vdash</math></td> <td>_</td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>_</td> <td>-</td> <td>_</td> <td><math>\vdash</math></td> <td></td> <td>-</td> <td></td> <td></td> <td>H</td>	ZU) CA	<u>8</u>	-	_			_	_	-	├			-		_		_		-			-					_	Н	$\vdash$	_	$\vdash$	$\vdash$	-	-		-	_	-	_	$\vdash$		-			H
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>SII AN</td> <td></td> <td>-</td> <td>_</td> <td><math>\dashv</math></td> <td>-</td> <td><math>\vdash</math></td> <td></td> <td>⊢-</td> <td>├</td> <td>-</td> <td><b>├</b></td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td>-</td> <td></td> <td>_</td> <td>-</td> <td></td> <td><b></b>-</td> <td></td> <td>_</td> <td>-</td> <td><b>!</b></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>_</td> <td>_</td> <td><u> </u></td> <td></td> <td><math>\vdash</math></td> <td></td> <td>-</td> <td>L</td>	SII AN		-	_	$\dashv$	-	$\vdash$		⊢-	├	-	<b>├</b>	-	_		_	-	_		_	-		_	-		<b></b> -		_	-	<b>!</b>				_				_	_	<u> </u>		$\vdash$		-	L
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td><u> </u></td> <td></td> <td>Н</td> <td>-</td> <td>-</td> <td></td> <td><math>\vdash</math></td> <td>_</td> <td>-</td> <td></td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td></td> <td>-</td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td>_</td> <td>_</td> <td>-</td> <td>_</td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td>_</td> <td>-</td> <td>ш</td> <td></td> <td></td> <td>-</td> <td>H</td>	<u> </u>		Н	-	-		$\vdash$	_	-		-		-	-	-		-		-	_					-	-	-	_	_	-	_	_						_	_	-	ш			-	H
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>3</td> <td></td> <td>ш</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td><math>\vdash</math></td> <td>-</td> <td><math>\vdash</math></td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>_</td> <td></td> <td></td> <td>_</td> <td>-</td> <td><math>\rightarrow</math></td> <td>_</td> <td>_</td> <td>-</td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td>_</td> <td><math>\mathbf{H}</math></td> <td><math>\vdash</math></td> <td>_</td> <td><math>\vdash</math></td> <td>ш</td> <td></td> <td></td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td>_</td> <td></td> <td>ш</td> <td>Н</td> <td>-</td> <td>-</td> <td>L</td>	3		ш						$\vdash$	-	$\vdash$	-	-	-	-	_			_	-	$\rightarrow$	_	_	-	$\vdash$	$\vdash$	_	$\mathbf{H}$	$\vdash$	_	$\vdash$	ш			-	_		_	_		ш	Н	-	-	L
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>3</td> <td></td> <td>-</td> <td><math>\dashv</math></td> <td></td> <td>-</td> <td>-</td> <td>_</td> <td>-</td> <td>├</td> <td>_</td> <td>-</td> <td><del> </del></td> <td>_</td> <td><math>\vdash</math></td> <td>_</td> <td>_</td> <td></td> <td>_</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td><math>\vdash</math></td> <td>_</td> <td>_</td> <td></td> <td></td> <td>-</td> <td><math>\vdash</math></td> <td>_</td> <td><math>\rightarrow</math></td> <td>-</td> <td>-</td> <td>_</td> <td>├</td> <td>⊢</td> <td><math>\vdash</math></td> <td>ш</td> <td>-</td> <td></td> <td></td> <td>Ļ</td>	3		-	$\dashv$		-	-	_	-	├	_	-	<del> </del>	_	$\vdash$	_	_		_	-					-	$\vdash$	_	_			-	$\vdash$	_	$\rightarrow$	-	-	_	├	⊢	$\vdash$	ш	-			Ļ
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>200</td> <td></td> <td>-</td> <td>_</td> <td></td> <td>-</td> <td></td> <td>_</td> <td>-</td> <td>_</td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td><math>\vdash</math></td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>_</td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td>-</td> <td>-</td> <td>-</td> <td>Н</td> <td>_</td> <td></td> <td>-</td> <td>-</td> <td>_</td> <td>_</td> <td>-</td> <td>-</td> <td><math>\vdash</math></td> <td>Н</td> <td>-</td> <td></td> <td>H</td>	200		-	_		-		_	-	_	-	-	-		$\vdash$		-	-	-	-	-	-	-	_	$\vdash$	$\vdash$	$\vdash$	$\vdash$	-	-	-	Н	_		-	-	_	_	-	-	$\vdash$	Н	-		H
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>8</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>-</td> <td>-</td> <td><math>\overline{}</math></td> <td></td> <td></td> <td><math>\mathbf{I}</math></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td></td> <td>_</td> <td><math>\vdash</math></td> <td><math>\vdash</math></td> <td>-</td> <td><math>\mathbf{H}</math></td> <td></td> <td></td> <td></td> <td><math>\vdash</math></td> <td>_</td> <td>-</td> <td>_</td> <td>-</td> <td>Н</td> <td></td> <td>_</td> <td>_</td> <td>L</td>	8					_				_		-	-	$\overline{}$			$\mathbf{I}$					_	-	_		_		_	$\vdash$	$\vdash$	-	$\mathbf{H}$				$\vdash$	_	-	_	-	Н		_	_	L
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>21</td> <td></td> <td>-</td> <td></td> <td></td> <td>_</td> <td>_</td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td></td> <td>-</td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td><math>\vdash</math></td> <td>-</td> <td>_</td> <td>-</td> <td>_</td> <td>_</td> <td>-</td> <td><math>\blacksquare</math></td> <td><math>\overline{}</math></td> <td><math>\vdash</math></td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td>_</td> <td>-</td> <td>51</td> <td>Ь.</td> <td></td> <td>25</td> <td>52</td> <td></td> <td></td> <td>55</td> <td>-</td> <td>-</td> <td>Ī</td>	21		-			_	_	-	-	-			-	_					$\vdash$	-	_	-	_	_	-	$\blacksquare$	$\overline{}$	$\vdash$	-	-	-	-	_	-	51	Ь.		25	52			55	-	-	Ī
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>(an) -</td> <td></td> <td>-</td> <td>_</td> <td>_</td> <td>_</td> <td>-</td> <td>-</td> <td>_</td> <td><b>├</b>─</td> <td>47</td> <td>٠</td> <td>_</td> <td>_</td> <td>48</td> <td>46</td> <td>38</td> <td>49</td> <td></td> <td></td> <td>_</td> <td></td> <td>_</td> <td>-</td> <td><math>\vdash</math></td> <td></td> <td><u> </u></td> <td>_</td> <td>_</td> <td>-</td> <td>_</td> <td>_</td> <td>-</td> <td></td> <td>_</td> <td>_</td> <td></td> <td><math>\vdash</math></td> <td>┡</td> <td>┞</td> <td>55</td> <td>09</td> <td>ଞ</td> <td>83</td> <td></td>	(an) -		-	_	_	_	-	-	_	<b>├</b> ─	47	٠	_	_	48	46	38	49			_		_	-	$\vdash$		<u> </u>	_	_	-	_	_	-		_	_		$\vdash$	┡	┞	55	09	ଞ	83	
Date         Type         Dist.         Pos.         1           5/13         M.16         20.434         Base         4           5/13         M.16         20.434         Base         4 <td>200</td> <td></td> <td>П</td> <td></td> <td></td> <td></td> <td><math>\equiv</math></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td><math>\rightarrow</math></td> <td></td> <td>H</td> <td></td> <td>H</td> <td>H</td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td><del></del></td> <td></td> <td></td> <td>Г</td> <td>_</td> <td><math>\vdash</math></td> <td></td> <td>Н</td> <td></td> <td></td> <td>Ī</td>	200		П				$\equiv$				_						-					_	$\rightarrow$		H		H	H			-				<del></del>			Г	_	$\vdash$		Н			Ī
July Composition         July Composition<	ğ			$\dashv$			46				44		T	47	48	51	17	41		44	4			47	$\vdash$	4	47	=			25	ę	41	54	-		Т		25	T		П	$\sqcap$	$\dashv$	ſ
5/13 M.16 20-434 5/13 M	3	Pos.	Base	Base	Base	ക		Base	Base	Base	Base	Base	Base	_	-	-		-	Base	_	Base	Q)		_	Base	⊢	-	⊢	Base	a o		_	$\perp$	_	Base	Base	Base	Base		Base	Base	Base	Base	Base	
5/13 M-16 5/13 M		E)	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434			20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434				20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	
5/13 5/13 5/13 5/13 5/13 5/13 5/13 5/13		ž.	_		_		I		-	_										Ī	91-1	- 16	1-16				1-16	4-16	-16	4-16	4.16									-					
	<u>ا ت</u>	<del>-</del>	-	-	-		ш	$\vdash$	┡-	┞	₩		-	_	_		_		_	_					_	_		-	—	-	-	_			├		-	⊢	⊢	-	├	$\vdash$	$\boldsymbol{\vdash}$	_	Ļ.
51	<u>8</u>		+	_	$\vdash$	-	$\vdash$	$\vdash$	-	-	<del> </del>	+-	-	_	_	_	_		_			_	_	_	-	_		-	_		-	_	-	-	_		-	—	-	-	-		-	_	۰

	Т	Т	Т	٦	_			П			Ī					٦	_		٦			Т	Т	Т	T	Т		7	Τ	T	Т	T	Т	T	Τ	Τ	T							<u> </u>
Overall	SEL	71.7	74.7	75.7	74.5	71.7	84.8	9.92	73.1	87.9	75.2	87.4	84.0	73.5	72.6	78.2	86.0	87.9	79.2	75.4	74.3	74.1	83.2	83.4	76.3	/3.8	B: /	9:0	71.6	73.8	70.4	70.7	75.8	20,2	75.8	80.3	80.7	79.2	7.97	76.8	72.7	76.2	72.8	77.3
2000							27	30		53		27					83	32					27									ç	3											
16000	į	8	32	8	83	33	48	30	37	22	32	49	98	32	S	34	14	22	32	8	8	8	36	9	12	3	8	23	37	8 8	200	3 8	3 8	3 8	34	35	34	32	35	27	32	35	37	33
12500							25			28		57	42			\$	48	62	ಜ	32			42	47								70	\$			32	34			37				
1000	$\dashv$	+		34	32	32	62	37	34	150		91	51		33	88	25	64	40	45	27	32	23	25	88		34	8	57	\$   S	8 8	/7 \$	3 6	,, 00	3	45	64	35	32	35	34	35	93	34
9000	-  -  :	45	41	£3	42	38	63	43	37	99	41	99	29	40	33	4	62	92	45	44	88	98	22	28	£ 3	88	<del>+</del>	£	8 8	37	8 6	ر اد	8 8	3 %	30	20	54	39	9	5	43	41	32	6
9300	-	27	3	69	20	37	98	46	35	82	4	72	61	37	4	£	9	29	20	54	8	8	8	8	9	88	9	42	8	<del>2</del>	કુ	<del>5</del> 5	8 8	¥ 2	5 g	3 2	28	44	£	융	3	44	37	41
2000		5	21	54	51	47	92	55	45	72	S	72	69	47	47	25	89	23	26	99	49	47	20	29	23	8	22	8	4	8	4	\$ 8	3 8	3	‡   ¢	2 G	159	51	51	50	51	69	47	20
		22	54	26	54	52	8	29	21	75	22	75	70	21	25	22	89	72	28	29	23	25	8	۶	22	22	22	25	69	23	<b>₽</b>	3 3	2 2	, e	⊋ £	4 <u>5</u>	8	25	25	ध	54	54	25	75
2500 3150 4000						L.,	L_	_	ـــ	<del></del>	↓_	ــــ	L	ш	$\perp$	L				_		-	-	-	-+			-	64		-	-	-+	-+-	+	-	+-	+	+	+	+-	-	-	╁
2500		_				_	Ь.	1	┞	_	<u> </u>	4-	<u> </u>	_		-	_	_		$\vdash$	$\vdash$				-+	-	-+		83	-		-+	-+-	+		-	+	+-	+	+-	+	┼	┼	┿
2000		_		_	Ь.	ــــ	<b>!</b>	↓	↓_	┺	╄		_	┞			<u> </u>	L	<u> </u>		Н	$\rightarrow$	-1			-	-		53 54	$\dashv$	-+	-+	-	+		-+-		+-	+	┿	┰	┰	+	+
1250 1600				_	L_	<u> </u>	ــــ	┺-	┺	┺	1.	<del></del>	╙		_		<u> </u>	_		-	$\vdash$	-4			-+	-	-		53		-+	-+		-+	-		-	+-	+-	╁	+	1	+	+
1000					<u> </u>	<u></u>	<u> </u>	_	┖	_	↓_	_	L	_	-	L	┡	╙	_					$\vdash$	-				ક્ક	-	-		-	-		-	+	+	+	+	+	+	-	+
88						ı		1					I			L													ည	_	_	_	_	-		_	_	-	-	-	_	+	+	-
630					1	1			f						ــــ		_			_		_					_	$\overline{}$	75		$\rightarrow$	$\rightarrow$	_	-	$\overline{}$		_	_	_	-	-	+	-	-1
400 500	_					<u> </u>			_						_		٠	_	-	-	_				$\vdash$	_	_	_	50 54	$\overline{}$	_	-	$\rightarrow$	_	-	_	_	-	_	-	_	_	_	_
315 4		61	22	65	8	88	83	65	82	8	19	25	ន	83	22	55	83	83	2	88	9	25	19	64	91	62	19	09	99	99	8	8	8	8	28	3 8	3 2	3 8	8	8	25	23	හු	:
250		_	Ь.		╌	-	-		+	-	-	+	-		-	-													63 62															
160 200		_	65 63	64 63	63	_	+-	+	+	+-		2 99	99	63 63	-	65	+-	╄	+-	62	-	-	99	99	Н		99 89	99 /9	$\vdash$				-	_	-	-	0 0	-	+-	+	_	_	_	-
1	_	89	┼-	99	8	┼	+	+	┿	╌	+-	+	29	83	-	8	┿	12	₩	-	8	_	29	89	H	$\vdash$	89	29	⊦	65	_		-+	+	-+	+	2 8	+	┿	┿	+-	+	+	;
0 1 13 1 16   20   25   32   40   50   63   80   100   125			26	88	ន	+-	+-	+	4-	-	+	+-	╌	ಔ	₩	88	+-	╁	-	+-		æ	29	83	$\vdash$	98	99	25	1-	63	-			-		-	8 8	+	+	+		╌	+	-
63		99 99	64 62	65	63	+	+-	┈	┰	+			┿		61 62	-	╌	┰	+	+-	83 85	64 65	99	-	64 64	59 64	83 88	⊢	-	59 62					-		2 G	+		+	3 6	┿		-
50		29	⊢	88	65	+-	┰	+	+-		┿	┰	8	+	88	+	╌	╫	┿	┿	┿	8	150	+	8	55	⊢	8	-	├—	H	_	-	$\dashv$		-	25 25		5 8	┿		+	+	-
8		19	28	22	83	25	6	8 8	13	5 E	, E	3 50	8	22	22	ଷ	50	88	20	88	જ	ස	57	8	83	25	8	ജ	54	જ	22	22	91	8	28	25	g (2		_		_	4	-	_
8		22	83	28	56	57	57	28	6	3 8	3 8	38	88	┿	क्ष	+-	+-	+-	+-	+	28	ß	+	25	₩-	2	+-	+-	88	25	25	22	$\vdash$	_	쫎	-+	2	-		+	3 12	3 2	5 6	3
2			L	L	ļ.	$\perp$	1	$\perp$	ļ	ļ	1	154	+-	+-	+	+	8	+	45	╂		L	ន	⊢	\$	_	42	5	+	L	_		$\vdash$	\$	-	8		8 4	+	+	+	1	1	-
٦		5	┰	83	┿	$\downarrow$	2	┿	┿	165	+	25	<del>-</del>	8	+-	+-	65	+-	┿	8	╌	-	S	┼	+-	23	23	╫	┿	+	8	L	5 48		-	8	-	-+	2 q	+	8 8	+	8 2	-
13 16		33	88	╀	82	152	3 2	3 12	5   2	7	4	-	: E	+	83	153	82	2	133	83	+	8	╀	23	22	20	72	83	88	25	8		45	4	29	20	ន	0	8 4	f   4	5 4	7 4	2 4	-
10		$\vdash$	122	+	╀	+	+	2	5   6	-	-	+	8	<del>- </del>	+	<u>E</u>	1 15	25		+	53	╁	+	+	92	72	25	╁	51	51	╁	-		H	8	5	$\dashv$	$\dagger$	-	5 2	<del>,</del>	1	8 8	- 04
900		Base	Base   5	نە ا-	Bace	Bace	0000	Bace F	_	<b>—</b> 1 0	Dase	<b>⊸</b> α	Race /	+-	-l <u>e</u>	Base	+-	+-	+	ન છુ	Base	J 00	Base	Base	Base	_	+	⊣ ღ	Base	+	Base	Base	Base	Base	ш	Base	Base	Rase	⋴⊢		Pase		╅	-
		20-434	┸	L.,	434	20.434	101.00			20-434			_	_		┸	. 1 .				丄		20-434	20-434				_			20-434	20-434	20-434	20-434	$\vdash$		20-434	20-434		_	- 1	454-02	- 1	
-	2 2 2	M-16 20	_	_	-		_	M-10	_		01-W	_	_	_	-				_	_	_	_	_	_	_	_	_	-	_	_	_	_	M-16 20	M-16 20		_	_	_	_	_		01-IN		
300	=	+-	5/17 M	+-		+	+	71/C	+	-	71/C	+	┰		╅	+	╅	+-	╅	┰	┿	╄	┿	┿	+	+	+-	+	+-	┿	+	+	-	5/17 N	5/17 N	$\vdash$		-+		-+	2/1/2	-	71/9	_
3 3		-	-		-	200	-	-+-	3 3	-	-+	<del>-</del>	3 5		_	202	_	-				-	5 5		+	+-	+		_	-	103	+	+-	-	-	_	-		-+	_	200	_	3 S	-

		$\top$	Т				·			
Calc.	Overall	72.9	75.5	7.97	9.87	70.2	73.3	72.5	9.77	70.5
	20000	27			22					
	16000	32	32	33	46	35	08		35	
	12500			42	51	41			43	
	10000	34		52	49	27	30	27	47	27
ı	0008	g	93	54	53	35	39	35	22	22
	930	98	42	22	23	22	28	35	99	32
	2000	46	49	22	55	45	49	44	59	44
	<del>§</del>	5	52	09	61	49	52	48	28	20
	3150	53	54	છ	63	47	51	20	64	47
	2500	22	29	65	59	54	22	99	89	54
	2000	26	69	29	69	25	22	25	02	25
	1600	29	8	2	23	29	25	28	22	28
_	1250	8	15	92	7.5	25	22	22	29	88
	1000	8	19	ಚ	69	89	29	25	92	28
	8	22	83	83	99	22	54	52	62	51
	630	53	57	88	62	23	53	54	09	51
	200	88	65	88	9	ಜ	ဆ	22	29	8
	400	25	83	88	8	ß	හු	SS.	75	ಜ
	315	82	+-	5	ස	28	8	හු	හි	28
	0 250	2	┿	9	150	8	ន	8	-61	28
	0 200	8	╁	8	8	8	8	8	9	28
٦	5 160	6	+-	20	8	89	83	ន	8	9
es (Hz)	125	1	╫	3 64	65	8	8	53	3 64	9
uenci	0 100	0	╌	63	8	88	63	<del>1</del> 9	8	8
r Freq	83	9	+-	2 64	19	58 59	⊢	62	63	9
Cente	9 05	47	╫	59 62	55	54	22 61	55	55	54 60
ctrum	40	54	+	58 5	48	53 5	54 5	58 5	56	55
e Spe	32	55	+-	52	45	98	95	65	23	22
Octav	22	+	20	Ť	Ė	Ė	Ė	İ	45	H
Band SEL (dB) at 1/3 Octave Spectrum Center Frequencies	8	6	╁╌	45	45	£	82	H	45	25
L (dB)	91	22	8	8	ಜ	83	ES ES	SS.	55	RS FS
II SE	55	†	1		Γ	T	T	Γ	T	Γ
Ba	2	2	2		8	8	ट	8	1	Γ
Mic	Pos.	Вась	Base	Base	Base	Base	Base	Base	Base	Base
Event	Dist.	20.434	20-434	20-434	20-434	20-434	20-434	20-434	20-434	20-434
Event	Type	M. 16	9- <u>1</u> -9	M-16	¥-16	₩-16	₹-16	M-16	M-16	M-16
Date		5/17	5/17	5/17	2/17	2/17	2/17	5/17	5/17	5/17
8		٤	<u> </u>	5	5	ā	ਛ	5	53	50

Table D 7. Summary data for passive helicopter flights on Fort Stewart, GA.

Col.	Date	Nesting	Event	Event	RCW	Rec. time	Mic	SEL (dB)	
		Phase	Туре	Dist.	Resp.	(min)	Pos.		
		& Day		(m)				Flat	Α
6	4/21/99	1-2	Helicopter	150	0		Base	100.2	87.6
6	4/26/99	I-6	Helicopter	300	0		Base	92.9	75.0
6	4/29/99	1-9	Helicopter	100	0		Base	104.4	88.0
10	5/27/99	N-2	Helicopter	300	0		Base	90.3	82.5
23	4/28/99	I-3	Helicopter	250	0		Base	97.7	78.7
25	5/5/99	1-9	Helicopter	400	0		Base	84.8	71.6
44	4/21/99	I-2	Helicopter	200	0		Base	98.5	86.1
44	4/21/99	I-2	Helicopter	250	0		Base	95.3	85.4
56	4/15/99	Inactive	Helicopter	300	0		Base	93.6	84.3
56	4/15/99	Inactive	Helicopter	300	0		Cavity	102.5	91.2
83	5/19/99	1-2	Helicopter	250	0		Base	99.2	84.9
143	4/21/99	1-6	Helicopter	300	0 .		Base	93.3	84.1
151	5/4/99	I-6	Helicopter	300	0		Base	91.0	82.7
218	4/20/99	I-1	Helicopter	400	0		Base	85.1	74.5
218	4/20/99	I-1	Helicopter	300	0		Base	93.8	82.7

Table D 8. Representative unweighted noise spectra for passive helicopter flights on Fort Stewart, GA.

	Sa Si	Overall	SEL	100.2	92.9	104.4	90.3	57.7	84.8	98.5	95.3	93.6	102.5	99.2	93.3	91.0	85.1	93.8
ľ		20000		29	32		8	25		8	83	22	8	53	ຮ	æ	85	92
		16000		22	46	21	5	55	83	37	37	33	37	99	34	28	£	36
		12500		55				49		34	32	82	36	31	27			34
		10000		55	45	64	46	22	62	40	6	දි	43	40	38	53	တ္တ	43
		8000		28	49	28	23	ည	35	43	45	45	44	43	45	19	98	48
		9300		59	L			25	99	49	46	44	46	46	41		24	53
		2000		53	88	63	09	25	သ	29	25	20	20	54	48	89	41	22
		0 4000		89	09	65	62	51	25	61	28	22	21	29	53	8	45	61
		0 3150		71	37	47	3	20	37	99	63	09	99	63	69	38	48	64
		0 2500		74	9	2	99	92	48	66	/9	64	29	99	64	02	22	. 67
		00 2000		5 74	4 62	7	99 9	1 57	3 49	8	69	99   6	3 56	89   I	99 (	02   5	5 29	69
		50 1600		6 75	54	6 71	99 8	3 61	2 23	73	4 71	1 69	e9 E	3   71	2 70	4 65	4 62	3 71
		1000 1250		92 82	99	92 82	76 73	E9 / 2	0 57	76 74	2 74	75   71	4 63	4 73	4 72	5 74	7 64	74 73
		800 10		7 67	9 69	78 7	7 97	29 02	09 89	7 08	77 62	79 7	68 64	78 74	77 74	71 75	68 67	75 7
		630		08	: 29	. 18	22	. 22	99	85	08	81	69	. 12	08	92	89	75
		009 0		181	29 !	82	75	171	89	80	78	79	71	62	6/ 1	9/	. 67	11
		315 400		81   82	95 89	80 81	72 69	02 69	89   69	74 75	11   11	70 75	80 75	80   82	73 78	E9 97	64 67	74 76
l		550		82 8	14	83 8	.   1/2	)   1/2	62 (	92	. 12	71	8 68	12 8	. 02	. 14	) /9	74
17.7	S (HZ)	200		84	17	98	71	8/ (	9 9	98	62	76	101	74	74	99	69	72
ŀ	nencie	125 160	_	81 84	92   62	91 87	76 81	84 80	99   99	82 85	81 84	80 83	96   38	78 78	92	92 08	64 72	9/ 9/
	rrreq	1001		92	81	94	74	98	) //	84	98	83	3 62	83	62	71 8	9 29	. 82
į	ctrum Center Frequencies (HZ)	88		83	85	86	83	88	9/	83	85	78	72	85	9/	83	9/	98
	ectrum	50 63		90	92 8	26 96	11 11	06 G	72 77	68 68	34 82	34 80	90 26	88 86	34 81	99	75 74	12 84
4	ve sp	8		8	82 8	36	72 7	8 / 8	1 11	3 06	82   8	84 8	81 8	8 68	83	908	64 7	0/
3	3 Octa	32		84	73	90	80	87	20	80	75	73	11	62	74	08	11	87
1	B) at 1	20 25		95 91	71 82	87 93	72 83	83 89	92	92 88	90 78	87 76	96 76	88 96	85 85	69 62	29 80	68 87
17	SEL (d	16		84	02	75 8	71	64	0/	87 (	71 8	83	85	84 6	85 8	85	99	22 (
	Band SEL (dB) at 1/3 Octave Sp	10 13		/9	1 78	88		84	29	64	62	60	. 60	62	29		99	09
-	<u>ال</u>	Pos. 10		Base 68	Base 68	Base 87	Base 66	Base 81	Base 56	Base 65	Base 65	Base 55	Cavity 57	Base 59	Base 53	Base 78	Base 54	Base 59
H	ع ن ن	time P	min)	ä	e c	B	B	B	B	ä	ä	B	Cs	B	ä	ĕ	B	ä
t	<u>-</u>	Resp.	<u>=</u>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Event	Dist.	Œ	120	300	92	300	250	400	500	250	300	300	250	300	900	400	300
	Event	Type		Helo	Hele	Helo	Helo	Helo	Helo	Helo	Helo	Helo	Helo	Helo	Hefo	Helo	Helo	Helo
	Nesting	Phase	& Day	1.5	9-1	6-1	N-2	6-1	61	7:1	1:5	Inactive	Inactive	2:1	9-1	9.	≖	Ξ
	e Case			4/21	4/26	4/29	5/27	4/28	2/2	4/21	4/21	4/15	4/15	5/19	4/21	5/4	4/20	4/20
[	<u></u>			9	9	ဖ	5	ន	દ્ધ	4	44	99	92	æ	143	151	218	218

Table D 9. Summary data for passive large-caliber live fire noise on Fort Stewart, GA.

Cluster	Date	Nesting	Event	Event	Azim.	RCW	Rec. time	Remarks	Mic	SEL (dB) at	mic
		Phase	Туре	Dist.	re.	Response	(min)		Pos.		
		& Day	1	(m)	DOF					Flat	A
10	5/27	N-2	Artillery	0	0	0	0		Base	79.6	50.1
25	5/5	1-9	Artillery	0	0	0	0		Base	90.6	62.2
25	5/5	1-9	Artillery	0	0	0	0		Base	90.3	62.3
25	5/5	1-9	Artillery	0	0	0	0		Base	91.1	62.0
25	5/5	1-9	Artillery	0	0	0	0		Base	91.3	65.1
25	5/5	I-9	· · · · · · · · · · · · · · · · · · ·	0	0	0	0		Base	90.5	61.6
83	5/2	i-2		0	0	0	0		Base	68.8	53.3
83	5/2	1-2	25 mm	0	0	0	0		Base	68.0	56.5
83	5/2	1-2	25 mm	0	0	0	0		Base	69.8	58.1
83	5/2	1-2	25 mm	0	0	0	0		Base	70.3	57.9
83	5/2	1-2	25 mm	0	0	0	0		Base	72.8	62.1
83	5/19	1-2	25 mm	0	0	0	0		Base	60.1	45.1
83	5/19	1-2	25 mm	0	0	0	0		Base	59.5	45.2
143	4/21	I-6	Artillery	0	0	0	0		Base	79.5	49.0
159	5/6	1-5	Tank blast	0	0	0	0		Base	86.3	70.8
159	5/6	1-5	Tank blast	0	0	0	0		Base	86.4	71.3
172	4/27	N-0	Artillery	0	0	0	0		Base	101.8	85.6
172	4/27	N-0	Artillery	0	0	0	0		Base	103.0	83.5

Table D 10. Representative unweighted noise spectra for passive large-caliber live fire events on Fort Stewart, GA.

|              | 7   | 9   | 9   | က  | <del> </del>  | က  | 2   
   
  | œ  
   
   | 0   
  | œ  
  | 8  
  | <u></u>   | <del> -</del>  | 2  | 2  
   | က  | ₹  | 8  | 0  |
|--------------|---|---|---|--|---|--
--
--
--
--
--
--|---
--
---	---	--	--
--			
Overall	75	79.	90.
   
  | .89  
   
   | 88  
  | 69   
  | 70.  
  | 72.   | 90.  | 59.  | 79.  
   | 86.  | .98  | 101.   | 103.0  |
| 2000         |   | 0   | 8   | Ξ  |   |  |   
   
  |  
   
   |   
  |  
  |  
  |   |  |  |  
   | 40   | 37   | 70   | 0,   |
| 16000        |   | 21  | 21  | 17   | 11  | 49   | 17  
   
  | 12   
   
   | 0   
  | 18   
  | 12   
  | 16  | 13   | 17   | 13   
   | £  | 45   | 89   | 89   |
| 12500        |   | 0   | 8   |  | 13  | 21   |   
   
  |  
   
   |   
  |  
  |  
  |   |  |  |  
   | 5  | 44   | 99   | 99   |
| 10000        |   | 20  | 22  | 22   | 73  | 21   | 19  
   
  | 7  
   
   | 12  
  | 13   
  | 10   
  | 16  | 15   | 13   | 15   
   | 47   | 47   | 9  | 65   |
| 8000         |   | 24  | 31  | 22   | 24  | 56   | 27  
   
  | 15   
   
   | 14  
  | 21   
  | 17   
  | 82  | 20   | 20   | 18   
   | 48   | 48   | 64   | 63   |
| 9300         |   | 0   | 31  | ଛ  | 14  | 56   | 33  
   
  |  
   
   |   
  |  
  |  
  | 15  |  |  |  
   | 20   | 20   | 63   | 62   |
| 2000         |   | 93  | 33  | ೫  | 32  | 38   | 35  
   
  | 24   
   
   | 52  
  | 27   
  | 56   
  | 28  | 21   | 56   | 28   
   | 21   | 51   | 63   | 61   |
|              |   | 32  | 36  | 31   | 41  | 38   | 36  
   
  | 28   
   
   | 53  
  | 30   
  | 56   
  | 30  | 28   | 33   | 53   
   | 52   | 53   | 63   | 61   |
| 3150         |   | 0   | 28  | 53   | 36  | 31   | 33  
   
  | 21   
   
   | 28  
  | 25   
  | 21   
  | 25  | 56   | 36   |  
   | 54   | 54   | 9  | 61   |
| 2500         |   | 34  | 35  | 34   | 33  | 36   | 34  
   
  | 30   
   
   | 30  
  | 33   
  | 31   
  | 34  | 36   | 32   | 32   
   | 55   | 22   | 89   | 62   |
| 2000         |   | 33  | 35  | 34   | 33  | 36   | 35  
   
  | 31   
   
   | 33  
  | 35   
  | 34   
  | 37  | 30   | 30   | 32   
   | 26   | 25   | 20   | 63   |
|              |   | 0   | 35  | 98   | 36  | 40   | 34  
   
  | 35   
   
   | 39  
  | 40   
  | 40   
  | 45  | 50   | 56   | 20   
   | 25   | 28   | 74   | 99   |
|              |   | 36  | 68  | 37   | 38  | 44   | 88  
   
  | 40   
   
   | 44  
  | 46   
  | 44   
  | 48  | 34   | 33   | 35   
   | 69   | 65   | 73   | 89   |
|              |   |   | 41  | L  | 41  | _  |   
   
  | Ĺ  
   
   |   
  |  
  |  
  | 51  |  |  | | | | |
   |  | 19   |  | 71   |
|              |   |   |   | L  |   |  |   
   
  |  
   
   | Ĺ   
  |  
  |  
  |   |  |  | | | | |
   |  |  |  | 57 75  |
|              |   |   |   | L  | Ĺ   |  |   
   
  |  
   
   |   
  | L  
  |  
  |   |  |  | | | | |
   |  |  |  | 7 75   |
|              |   |   |   |  |   |  |   
   
  |  
   
   |   
  |  
  |  
  |   |  |  |  
   |  |  |  | 77 97  |
|              |   | 40  | 27 5  | 58 5   | 57 5  | 9   29   | 55 5  
   
  | 47 4   
   
   | 52 5  
  | 53 5   
  | 54 5   
  | 28  | 37 2   | 36   | 43 4   
   | 99   | 9 /9   | 2 22   | 78 7   |
| 250          |   | 42  | 61  | ß  | 19  | 64   | 29  
   
  | 48   
   
   | 25  
  | 24   
  | 23   
  | 29  | 93   | 33   | 45   
   | 88   | 29   | 28   | 78   |
| <b>3</b> 9   |   | 44  | ဠ9  | 63   | 9   | 99   | 19  
   
  | 45   
   
   | 48  
  | 48   
  | 15   
  | \$  | £ <b>†</b>   | 43   | 47   
   | 88   | 69   | 08   | 08   |
|              |   | 53  | 29  | 61   | 65  | 89   | 09  
   
  | 48   
   
   | 20  
  | 25   
  | 25   
  | 59  | 49   | 47   | 48   
   | 89   | 20   | 84   | 84   |
|              |   |   | Ш   |  |   |  | 1   
   
  |  
   
   |   
  |  
  | <u> </u>   
  |   |  | L  | | | | |
   | L  |  |  | 35   |
|              |   |   |   | L.   |   |  |   
   
  | L  
   
   |   
  |  
  |  
  |   |  |  | _  
   |  |  |  | 98 88  |
|              |   | 61 6  | 75 7  | 79   | 78 7  | 81 7   | 76 7  
   
  | 62 5   
   
   | 49 5  
  | SS 55  
  | 58   
  | 9 89  | 44   | 44   | 99   
   | 76 7   | 7 97   | 6 96   | 88   |
| 20           |   | 61  | 79  | 8  | 74  | 111  | 9/  
   
  | 62   
   
   | 99  
  | 09   
  | 65   
  | 83  | 46   | 47   | 09   
   | 74   | 73   | 8  | 97   |
| <del>3</del> |   | 70  | 23  | 23   | 83  | 2  | 78  
   
  | 22   
   
   | 88  
  | 19   
  | 83   
  | အ   | \$   | 33   | 28   
   | 78   | 78   | 93   | ន  |
|              |   |   |   | 1  | _   | ┖  |   
   
  |  
   
   | Ш   
  |  
  |  
  | <u> </u>  |  | ш  |  
   | l  | 1  |  | 95   |
| 8            |   | 70  | 180   | 8  | 8   | 18   | 81  
   
  | 99   
   
   | 88  
  | 65   
  | 22   
  | 8   | 51   | 3  | 74 7   
   | 72 7   | 74 7   | 8  | 68   |
| 16           |   | 72  | æ   | 8  | 8   | 81   | 83  
   
  | 88   
   
   | 88  
  | 09   
  | 88   
  | 19  | ß  | 48   | 74   
   | 76   | 78   | 88   | 87   |
| 13           |   | 3 72  | 2 83  | 3 78   | 8 84  | 1-86   | 2 84  
   
  | 95   
   
   | 35  
  | 9 57   
  | 7 55   
  | 92  | £  | 7 46   | 8 71   
   | 9/ 9   | 9/ 0   | 5 87   | 7 88   |
|              | 4   | 22 0  | 0   | 0  | 0   | 8  | 8   
   
  | 0  
   
   | 0   
  | 0  
  | 0  
  | 0   | 0  | 3  | 9  
   | 9  | 0  | 0  | 0 87   |
|              | 4   |   | _   |  | _   | <u> </u>   | _   
   
  | F  
   
   | F   
  | ۴  
  | ۴  
  | F   | F  | ٦  |  
   | _  | _  |  |  |
| Type         |   | Art   | ¥   | Art  | ¥   | Art  | Art   
   
  | 25 mr  
   
   | 25 m  
  | 25 mr  
  | 25 mr  
  | 25 mr   | 25 mr  | 25 m   | Art  
   | Ta<br>Şë   | 뚩  | Art  | Art  |
| Phase        | a Day   | 7 N-2   | <u>6.</u>   | 6-1  | <u>6-</u>   | 6-1  | 6-1   
   
  | 2-1-2  
   
   | 2-1   
  | 7-1  
  | 1.2  
  | 1.2   | 2  | 2-1-5  | 9 <u>-</u>   
   | 5-5  | <u>5</u>   | 0.N  | 4/27 N-0   |
| _            |   |   | 5/2   | 8  | 5/2   | 2/2  | 52  
   
  | 2/2  
   
   | 5/2   
  | 5/2  
  | 2/5  
  | 5/2   | 5/19   | 5/19   | 4/21   
   | 2,6  | 2/6  | L  | 1  |
|              |   | 10  | ઇ   | ડર   | 52  | દ્ધ  | છ   
   
  | æ  
   
   | æ   
  | æ  
  | æ  
  | æ   | æ  | æ  | 143  
   | 159  | 159  | 172  | 172  |
|              | Type Resp. 10 13 16 20 25 32 40 50 63 80 100 125 160 200 250 315 400 500 630 800 1000 1250 1600 2000 2500 3150 5000 6300 8000 10000 12500 16000 20000 | Туре   Resp. 10 13 16 20 25 32 40 50 63 80 100 125 160 200 250 315 400 500 630 800 1000 1250 1600 2000 2500 3150 5000 6300 8000 10000 12500 16000 20000 | Phase Type Resp. 10 13 16 20 25 32 40 50 63 80 100 125 160 200 250 315 40 50 63 80 100 125 160 200 250 315 40 35 40 35 40 35 41 38 30 38 30 38 34 0 33 34 0 24 20 0 21 0 21 0 | Phase         Type         Resp.         10         13         16         20         25         32         40         50         63         80         100         125         10         13         16         20         25         22         40         20         63         63         70         60         63         70         60         63         70         60         63         70         60         70         70         60         60         70 | Phase         Type         Resp.         10         13         16         20         25         25         40         50         63         80         100         125         10         13         16         20         25         25         40         20         250         800         1000         1250         1000         1250         1000         1000         1250         10         10         10         20         25         25         40         20         25         40         20         25         40         20         < | Phase         Type         Resp.         Resp.         Type         Resp.                 Type         Resp.         Resp.         Type         Resp.         "><th>Phase         Type         Resp.         Resp.         Type         Resp.         <t< th=""><th>Phase         Type         Resp.         <th< th=""><th>Phase         Type         Resp.         Resp.         Type         Resp.         Phase         Type         Hesp         Type         Type         Type         Type         Type         Type         Hesp         Type         <t< th=""><th>Phase         Type         Resp.         10         13         16         20         25         40         50         63         10         15         40         50         630         100         1250         150</th><th>Phase         Type         Resp.         10         13         16         20         25         42         40         15         16         20         15         16         20         15         16         20         15         16         20         15         16         20         15         16</th><th>Phase         Type         Resp.         10         13         16         25</th><th>  Physical Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Ty</th><th>  Physic  
Physic   P</th><th>  Physic   P</th><th>  Phose   Phos</th><th>  Phose   Phos</th></t<></th></th<></th></t<></th></t<> | Phase         Type         Resp.         Resp.         Type         Resp.         "><th>Phase         Type         Resp.         <th< th=""><th>Phase         Type         Resp.         Resp.         Type         Resp.         Phase         Type         Hesp         Type         Type         Type         Type         Type         Type         Hesp         Type         <t< th=""><th>Phase         Type         Resp.         10         13         16         20         25         40         50         63         10         15         40         50         630         100         1250         150</th><th>Phase         Type         Resp.         10         13         16         20         25         42         40         15         16         20         15         16         20         15         16         20         15         16         20         15         16         20         15         16</th><th>Phase         Type         Resp.         10         13         16         25        
25         25</th><th>  Physical Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Ty</th><th>  Physic   P</th><th>  Physic   P</th><th>  Phose   Phos</th><th>  Phose  
Phose   Phos</th></t<></th></th<></th></t<> | Phase         Type         Resp.         ""><th>Phase         Type         Resp.         Resp.         Type         Resp.         Phase         Type         Hesp         Type         Type         Type         Type         Type         Type         Hesp         Type         <t< th=""><th>Phase         Type         Resp.         10         13         16         20         25         40         50         63         10         15         40         50         630         100         1250         150</th><th>Phase         Type         Resp.         10         13         16         20         25         42         40         15         16         20         15         16         20         15         16         20         15         16         20         15         16         20         15         16</th><th>Phase         Type         Resp.         10         13         16         25</th><th>  Physical Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Ty</th><th>  Physic   P</th><th>  Physic  
Physic   P</th><th>  Phose   Phos</th><th>  Phose   Phos</th></t<></th></th<> | Phase         Type         Resp.         Resp.         Type         Resp.                 Type         Hesp         Type         Type         Type         Type         Type         Type         Hesp         Type         "><th>Phase         Type         Resp.         10         13         16         20         25         40         50         63         10         15         40         50         630         100         1250         150</th><th>Phase         Type         Resp.         10         13         16         20         25         42         40         15         16         20         15         16         20         15         16         20         15         16         20         15         16         20         15         16</th><th>Phase         Type         Resp.         10         13         16         25</th><th>  Physical Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type
  Type   Ty</th><th>  Physic   P</th><th>  Physic   P</th><th>  Phose   Phos</th><th>  Phose   Phos</th></t<> | Phase         Type         Resp.         10         13         16         20         25         40         50         63         10         15         40         50         630         100         1250         150        
150         150         150         150         150         150         150         150         150         150         150 | Phase         Type         Resp.         10         13         16         20         25         42         40         15         16         20         15         16         20         15         16         20         15         16         20         15         16         20         15         16 | Phase         Type         Resp.         10         13         16         25 | Physical Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Resp.   Type   Ty | Physic   P | Physic   P | Phose  
Phose   Phos | Phose   Phos |

Table D 11. Summary data for ambient sound levels on Fort Stewart, GA.

Cluster	Date	Nesting	Event	Mic	AVG. LEG	Q (dB)
		Phase	Туре	Pos.		
		& Day			Flat	Α
179	07-Jun-99	Post-fled.	Ambient	Cavity	53.6	43.0
179	07-Jun-99	Post-fled.	Ambient	Base	48.8	44.2
71	07-Jun-99	Post-fled.	Ambient	Cavity	62.4	41.2
71	07-Jun-99	Post-fled.	Ambient	Base	49.2	41.0
35	07-Jun-99	N-12	Ambient		49.2	43.8
107	17-Jun-99	Post-fled.	Ambient	Base	50.1	43.0
107	17-Jun-99	Post-fled.	Ambient	Cavity	62.7	46.9
216	18-Jun-99	Post-fled.	Ambient	Base	53.7	43.6
216	18-Jun-99	Post-fled.	Ambient	Cavity	66.5	45.8
129	24-May-99	N-7	Ambient	Base	64.8	56.9
159	06-May-99	I-5	Ambient	Base	52.5	41.5
159	21-May-99	N-9	Ambient	Base	50.2	41.9
162	03-Jun-99	Post-fled.	Ambient	Base	52.7	41.6
162	03-Jun-99	Post-fled.	Ambient	Cavity	61.3	50.8
30	03-Jun-99	Post-fled.	Ambient	Base	48.0	39.9
30	03-Jun-99	Post-fled.	Ambient	Cavity	47.9	40.0
127	03-Jun-99	Post-fled.	Ambient	Base	61.6	51.6
127	03-Jun-99	Post-fled.	Ambient	Cavity	56.9	45.8
134	15-Jun-99	I-7	Ambient	Base	49.5	40.7
23	03-May-99	I-8	Ambient	Base	60.4	53.7
103	17-May-99	0	Ambient	Base	66.2	58.3
41	02-Jun-99	I-8	Ambient	Base	50.2	42.3
3	22-Jun-99	N-17	Ambient	Base	67.4	59.5
103	12-May-99	N-2	Ambient	Base	59.3	51.4
103	12-May-99	N-2	Ambient	Base	59.4	51.8
70	20-May-99	1	Ambient	Base	57.7	50.0
218	23-Apr-99	1-4	Ambient	Base	64.8	56.5
189	23-Apr-99	I-1	Ambient	Base	53.0	42.3
118	18-Jun-99	N-14	Ambient	Base	53.7	46.0
174	01-Jun-99	N-22	Ambient	Base	49.4	41.5
41	01-Jun-99	I-7	Ambient	Base	49.5	42.5
17	01-Jun-99	I-1	Ambient	Base	49.5	41.6
120	17-May-99	I-5	Ambient	Base	48.2	41.5
36	17-May-99	I-4	Ambient	Base	48.8	41.1
194	17-May-99	N-21	Ambient	Base	47.8	41.2
271	03-Jun-99	Post-fled.	Ambient	Base	50.4	42.3

Cluster	Date	Nesting	Event	Mic	AVG. LE	Q (dB)
		Phase	Туре	Pos.	ļ	
		& Day			Flat	Α
227	03-Jun-99	Post-fled.	Ambient	Base	49.9	42.0
227	03-Jun-99	Post-fled.	Ambient	Cavity	48.9	41.0
87	03-Jun-99	Post-fled.	Ambient	Base	51.0	41.3
87	03-Jun-99	Post-fled.	Ambient	Cavity	48.8	41.0
172	04-Jun-99	Post-fled.	Ambient	Base	49.7	41.3
172	04-Jun-99	Post-fled.	Ambient	Cavity	48.7	40.9
47	04-Jun-99	Post-fled.	Ambient	Base	48.8	41.2
47	04-Jun-99	Post-fled.	Ambient	Cavity	48.8	41.0
183	07-Jun-99	Post-fled.	Ambient	Base	48.7	42.6
183	07-Jun-99	Post-fled.	Ambient	Cavity	48.6	40.7
75	07-Jun-99	Post-fled.	Ambient	Base	49.9	43.0
75	07-Jun-99	Post-fled.	Ambient	Cavity	49.0	41.1
10	27-May-99	N-2	Ambient	Base	53.4	42.7
137	28-May-99	1-8	Ambient	Base	49.3	40.5
294	28-May-99	N-6	Ambient	Base	49.2	41.6
176	28-May-99	N-9	Ambient	Base	48.8	42.7
35	19-May-99	1-4	Ambient	Base	50.2	41.6
165	26-May-99	I-1	Ambient	Base	51.2	41.2
165	26-May-99	I-1	Ambient	Cavity	48.5	40.8
44	27-Apr-99	I-8	Ambient	Base	49.7	41.4
189	27-Apr-99	I-5	Ambient	Base	50.2	41.2
35	16-May-99	I-1	Ambient	Base	47.2	42.9
36	16-May-99	1-8	Ambient	Base	46.5	40.1
129	16-May-99	l-10	Ambient	Base	47.4	39.8
137	18-May-99	Pre-nest.	Ambient	Base	49.4	40.5
7	18-May-99	Between	Ambient	Base	50.4	39.5
163	18-May-99	1-6	Ambient	Base	47.3	39.7
41	28-May-99	1-5	Ambient	Base	47.9	41.2
80	28-May-99	N-0	Ambient	Base	49.7	42.9
2	28-May-99	I-7	Ambient	Base	46.7	38.9
10	28-May-99	N-3	Ambient	Base	49.0	41.2
67	28-Apr-99	I-4	Ambient	Base	52.3	44.0
13	14-May-99	N-4	Ambient	Base	51.8	40.0
31	14-May-99	N-6	Ambient	Base	48.4	39.1
32	16-May-99	N-0	Ambient	Base	49.5	40.8
5	16-May-99	1-4	Ambient	Base	50.1	40.4
141	16-May-99	N-5	Ambient	Base	49.5	40.0

Cluster	Date	Nesting	Event	Mic	AVG. LEG	Q (dB)
		Phase	Туре	Pos.		
		& Day			Flat	Α
177	16-May-99	N-2	Ambient	Base	48.7	39.4
120	16-May-99	1-4	Ambient	Base	46.6	38.9
80	16-May-99	Egg laying	Ambient	Base	47.4	41.1
1	10-May-99	1-7	Ambient	Base	47.8	39.1
122	13-May-99	N-1	Ambient	Base	47.9	39.4
132	13-May-99	I-7	Ambient	Base	48.5	40.8
73	13-May-99	N-8	Ambient	Base	49.6	39.6
37	13-May-99	I-5	Ambient	Base	50.0	40.2
189	03-May-99	N-0	Ambient	Base	51.0	40.8
82	29-Apr-99	I-8	Ambient	Base	49.7	41.5
159	29-Apr-99	Egg laying	Ambient	Base	48.7	41.6
71	02-May-99	1-3	Ambient	Base	15.3	11.9
68	02-May-99	Egg laying	Ambient	Base	15.3	11.9
38	02-May-99	I-9	Ambient	Base	48.5	39.3
34	02-May-99	Egg laying	Ambient	Base	51.8	40.9
174	03-May-99	I-5	Ambient	Base	47.0	41.0
174	28-Apr-99	I-5	Ambient	Base	47.9	39.8
89	28-Apr-99	1-4	Ambient	Base	51.5	42.1
203	16-Jun-99	Non-nest.	Ambient	Base	50.7	38.0
118	16-Jun-99	N-12	Ambient	Base	47.2	37.1
159	17-Jun-99	Post	Ambient	Base	47.1	38.1
159	17-Jun-99	Post	Ambient	Cavity	58.5	46.2
44	21-Apr-99	I-2	Ambient	Base	50.2	38.1
41	04-Jun-99	I-10	Ambient	Base	49.0	38.1
135	09-Jun-99	Incubation	Ambient	Base	53.5	38.6
130	09-Jun-99	Incubation	Ambient	Base	50.8	37.7
112	09-Jun-99	N-3	Ambient	Base	49.6	38.4
1	09-Jun-99	I-8	Ambient	Base	47.3	38.0
129	15-Jun-99	Post	Ambient	Base	46.2	39.4
129	15-Jun-99	Post	Ambient	Cavity	48.3	39.2
8	04-May-99	N-4	Ambient	Base	48.6	38.1
194	13-Apr-99	Pre-nest.	Ambient	Cavity	52.5	42.6
194	13-Apr-99	Pre-nest.	Ambient	Base	51.7	40.5
56	15-Apr-99	Inactive	Ambient	Base	55.1	42.2
56	15-Apr-99	Inactive	Ambient	Cavity	60.6	48.4
51	29-Apr-99	N-2	Ambient	Base	50.6	41.5
61	28-May-99	N-3	Ambient	Base	48.3	41.5

Cluster	Date	Nesting	Event	Mic	AVG. LE	Q (dB)
		Phase	Туре	Pos.		
		& Day			Flat	Α
88	28-May-99	Incubation	Ambient	Base	47.4	41.4
82	28-May-99	N-0	Ambient	Base	48.7	42.3
48	01-Jun-99	Post-fled.	Ambient	Base	48.6	40.6
48	01-Jun-99	Post-fled.	Ambient	Cavity	54.8	42.6
57	02-Jun-99	Post-fled.	Ambient	Base	46.8	40.3
57	02-Jun-99	Post-fled.	Ambient	Cavity	45.9	38.2
205	02-Jun-99	Post-fled.	Ambient	Base	47.3	40.0
205	02-Jun-99	Post-fled.	Ambient	Cavity	47.2	40.4
132	11-May-99	I-5	Ambient	Base	52.3	43.4
17	11-May-99	Incubation	Ambient	Base	47.7	41.6
122	11-May-99	I-10	Ambient	Base	45.9	38.1
189	29-Apr-99	1-7	Ambient	Base	50.2	39.7
17	11-May-99	Incubation	Ambient	Base	47.7	41.6
122	11-May-99	I-10	Ambient	Base	45.9	38.1
36	15-Jun-99	Post-fled.	Ambient	Base	46.3	42.6
36	15-Jun-99	Post-fled.	Ambient	Cavity	47.8	40.7
296	20-Jun-99	N-9	Ambient	Base	47.0	39.8
83	23-Jun-99	Post-fled.	Ambient	Base	49.5	41.9
83	23-Jun-99	Post-fled.	Ambient	Cavity	55.3	43.9
143	21-Apr-99	I-6	Ambient	Base	46.5	38.8
83	02-May-99	I-2	Ambient	Base	50.9	42.2
25	26-May-99	I-9	Ambient	Base	55.6	46.9
103	13-May-99	N-3	Ambient	Base	57.4	49.4
83	19-May-99	I-2	Ambient	Base	48.0	39.8
151	14-Jun-99	Post-fled.	Ambient	Base	51.3	43.7
151	14-Jun-99	Post-fled.	Ambient	Cavity	54.3	43.7
206	14-Jun-99	Post-fled.	Ambient	Base	57.4	51.2
88	18-Jun-99	Post-fled.	Ambient	Base	47.5	40.6
216	22-Jun-99	1-8	Ambient	Base	47.1	39.3
118	22-Jun-99	N-18	Ambient	Base	47.0	41.0
10	14-Jun-99	N-20	Ambient	Base	49.4	37.0

Table D 12. Representative unweighted noise spectra for ambient sound levels on Fort Stewart, GA.

1	48.8 48.8 48.8	54.8 50.6 55.1
Fig. 18	2	2
Fig. 18	15	15 16 14
Part   Leg (145)   141   135   136	- 19	
Mart   Mart	= <del>4</del> £ 2	E = E =
Market   Column   C	2 2 2 2	19 19 19
Mart   Mart	50	18
	2 8 8 8	2 2 2 3
Mart   Mart	29 88 68	28 3 2 3
Hand LEO (AEI) at 113 Octave Spectrum Content Frequencies (H4)  10 13 16 20 25 27 24 50 51 51 51 51 51 51 51 51 51 51 51 51 51		Ω Q
Hand LEQ (418) at 113 Octaves Specifrum Centre Frequencies (445)  10 13 16 20 2 2 2 2 2 0 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1		++++
Band LEO (AB) at 130 Octative Specificantim Contract Frequencies (Hz)           10         13         16         20         25         34         35         16         500         500         1000         1730           16         13         16         20         35         17         18         100         120         35         16         30         30         10         100         120         30         10         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120         10         120	<del></del>	<del>           </del>
Band LEO (cl8) at 1/3 Octative Specifical minimal control frequencies (t4)           10         13         16         20         25         22         40         50         100         120         150         100         600         100           10         13         16         20         25         24         40         50         100 <th><del></del></th> <th>2 2 21 22 24 28 24 24 24</th>	<del></del>	2 2 21 22 24 28 24 24 24
Martin   M	<del></del>	<del>                                     </del>
Fig. 12   Fig. 20   St. 2   Au   Au   St. 2   Au   St. 2   Au   St. 2   Au   St. 2   Au   St. 2   Au   Au   Au   Au   Au   Au   Au	<del></del>	<del>                                     </del>
Maria   LeO (48) at 143 Octava Spectrum Crime   Frequencies (Hz)   Hz   Hz   LeO (48) at 143 Octava Spectrum Crime   Frequencies (Hz)   Hz   Hz   Hz   Hz   Hz   Hz   Hz		
Sand   EQ   Color	8 8 8	3 8 8 8
Sand   EQ   Color	8 8 8 8	22 22 28
Sand   EGO   (Hg) at 1/3 Octave Spectrum Centrer Frequencies (Hz)   14   16   20   25   32   40   50   65   65   100   125   160   200   20   22   31   36   36   30   30   37   36   30   30   37   36   30   30   37   36   32   37   34   25   35   31   18   32   37   36   30   38   36   27   38   34   24   37   36   37   38   37   38   37   38   37   38   38	<del></del>	8 8 8 8
Band LEO (dB) at 1/3 Octave Spectrum Center Frequencies (Hz)           10         13         16         20         25         32         40         50         63         100         125         16         20           36         34         37         36         30         37         31         38         35         22         37         31         38         36         36         37         31         38         34         25         35         31         38         37         34         25         35         31         38         36         36         36         37         31         38         34         26         35         31         38         34         26         35         31         38         36         36         36         36         36         37         31         38         36         37         31         38         36         37         31         38         36         37         31         38         36         37         34         38         38         36         37         38         38         38         38         38         38         38         38         38         38	<del></del>	3 8 8 8
Band LEQ (dB) at 1/3 Octave Spectrum Center Frequenches           10         13         16         20         25         32         40         50         63         90         100         125           36         34         37         36         39         37         31         36         36         37         34         25         37         34         25         37         34         25         37         34         25         37         34         25         37         34         25         37         34         25         37         34         37         36         36         37         34         42         25         37         34         42         35         37         34         40         38         37         34         40         38         37         37         38         37         34         40         38         37         34         37         38         37         38         37         38         37         38         37         38         38         39         39         38         39         39         38         39         39         38         39         39         39         <		
Band LEO (dB) at 1/3 Octave Spectrum Center Frequence           10         13         16         20         25         32         40         50         63         10           36         34         37         36         30         39         37         31         38         35         22           27         31         38         37         36         30         37         31         38         35         24         25           27         21         35         38         37         36         36         37         31         38         34         24           27         21         35         36         36         37         31         38         34         24           29         31         38         37         36         36         37         34 <th>1 1 1 1 1</th> <th>. 1</th>	1 1 1 1 1	. 1
	2 23 28	
	40 40 39 39 40 40 36 39 39 39 39 39 39 39 39 39 39 39 39 39	<del> </del>
	± 88 9 88	2 E 8 8 4
	39 37 38 42 39 37 38 42 39 37	
	36 27 25 3 3 4 4 3 3 3 4	
	37 33 44	<del></del>
	22 33 37 38 38 38	27 27 38 27 39 39 45 43 45
Mic Base Base Base Base Base Base Base Base	ස ස ස ස	8 8 8 8
	Base Base Cavity	Cavity Base Base
Event Type Type Ambient	Ambient Ambient Ambient Ambient	Ambient Ambient Ambient Ambient Ambient
g g g	I-2 A I-8 A Post-fled. A	
<del>┡┈┈┈┧┈┧┈┧┈┧┈┧┈╅┈┧┈╅┈┧┈╃┈┼┈╏┈┨╸╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈</del>	<del>                                     </del>	<del></del>
<del>▐<del>▗</del>▔▕▗▐▗▐▗▊▐▗▊▊▊▊▊▊</del>	╅┼┼┼	+++

8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Calc.	Overall LEQ	9.09	46.8	45.9	48.3	52.3	57.7	62.4	49.2	49.6	49.9	49.0	47.4	49.7	49.7	48.7	50.9	48.0	49.5	55.3	51.0	48.8	47.4	47.5	51.5	59.3	59.4	57.4	66.2	20.1	62.7	49.6	4/.2	7.00	46.6	48.2	45.9	45.9	47.9	61.6	56.9	47.4	64.8
Part   Part		20000	4	16				6				9	П				5	0			-		2		ន	6	11	8	10			1	e	-	,	T	-				5			
Part   Part			15	23	5	16	13	92	4	4	9	<u>6</u>	15	14	50	17	17	12	ŧ	15	13	16	16	18	22	51	88	28	ક્ટ	8	=	9	£ :	با 2	<u> </u>	5 12	4	7	7	13	99	15	9	E .
Marie   Mari	Ī	12500		56			11					1		•	18										4	ಜ								Ì							23			
Day	Î	10000	14	52	=	17	14	24	5	6	14	∞	13	12	23	17	18	6	ಐ	14	12	13	13	21	9	54	24	22	22	ಐ	23	5	= ;	4 6	2 4	5 5	9	4	4	=	30	=	ವ	83
Mailing   Mail			50	35	2	35	21	30	6	82	19	22	8	21	56	23	34	16	2	22	19	20	8	33	%	30	સ	31	දි	ဗ္က	ន	ສ	5 8	3 8	3 8	3 8	ន	24	₽,	19	41	19	<u></u>	8
Part		6300		25		34	20					18		27	28		36			2				20	ន	33							19	2	75	3 4		3	က		36		#	
Part		2000	25	22	32	30	38	37	52	27	32	හ	27	22	33	53	27	22	52	33	25	56	24	56	22	98	40	36	35	<del>ද</del>	22	8	25	4 6	3 8	3 %	3	24	24	24	37	56	8	45
Partial Part			53	58	27	સ	33	38	27	22	27	32	28	27	38	53	32	52	53	35	33	58	22	တ္တ	શ	3	45	<del>1</del>	æ	8	8	8	12	7 8	8 8	3 2	8	92	92	56	40	82	<u>ج</u>	45
				18		24	3					ಣ		52	27	2	24	12		23	18			56	55	56				24			Ω,	1	T	T	17			-5	40		ន	
			30	22	22	88	32	38	53	83	27	8	82	83	58	53	32	22	58	31	30	58	88	53	22	တ္တ	40	88	37	8	83	3	£3 1	3 8	3 20	3 2	: 8	53	83	56	40	31	ଷ	4
Option State         President Armbinner         President Armbinner         President Armbinner         Read of State S			31	22	72	27	31	88	53	93	22	30	53	೪	58	30	53	58	22	59	53	53	83	28	82	58	40	33	37	84	೫	33	g 1	3 8	ડે દ	27	88	33	22	88	88	31	22	4
Option State         President Armbinner         President Armbinner         President Armbinner         Read of State S		1600	24	19	18	ಜ	31	29	56	21	8	23	19	22	19	19	16	23	56	23	21	23	20	10	8	21	29	31	32	88	ಣ	82	6	2 8	8 8	3 2	2 23	16	16	19	31	54	2	8
Date   Phase			34	30	ಣ	8	35	41	32	32	31	34	32	31	30	32	30	33	31	32	34	32	32	58	8	83	41	43	9	\$	중	37	23 2	20 2	3 8	3 8	88	೫	क्ष	સ	38	8	ಣ	44
Maring   Preside   Maring			35	30	ణ	೫	33	41	83	32	31	35	జ	32	31	35	99	33	31	31	34	33	ಜ	83	33	શ	45	43	4	8	88	용	g	<b>3</b> 5	3 8	3 8	8 8	೫	R	8	40	35	8	8
Date   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mode   Mesting   Event   Mesting   Event   Mesting   Event   Mesting   Event   Mesting	ŀ		53	52	ន	ಣ	27	32	27	92	22	62	88	22	27	56	23	32	દ્ધ	21	33	56	54	20	೫	54	33	34	દ્ધ	\$	ଛ	జ	ສ !	- 8	8 2	3 8	1 =	ĸ	£	ន	40	35	æ	4
Unit 500         Phase (1759)         Type (1759)         Phase (1759)         Type (1759)         State (1759)		630	36	35	೫	31	31	43	8	34	ဆ	98	34	8	32	34	32	37	32	31	34	34	33	30	8	31	43	45	43	SS.	32	33	8	3 5	⊋ ¿	5 6	8	3	3	33	45	32	8	49
Days         Type         Fresh         Band Led Class of State		28	37	35	31	32	35	44	ક્ષ	32	ဗ္ဗ	37	32		33	36	33	96	34	35	33	36	32	31	ક્ષ	31	44	46	43	22	ළ	88	<del>ह</del>	ੜ :	₹   £	3 8	8	ಜ	ಜ	೫	43	36	ន	2
Days         Finale         > <td>\$</td> <td>32</td> <td>13</td> <td>2</td> <td><b>œ</b></td> <td>24</td> <td>88</td> <td>22</td> <td>24</td> <td>ន</td> <td>8</td> <td>8</td> <td>52</td> <td>15</td> <td>55</td> <td>16</td> <td>56</td> <td>ន</td> <td>14</td> <td>23</td> <td>22</td> <td>54</td> <td>=</td> <td>গ্ৰ</td> <td>15</td> <td>54</td> <td>35</td> <td>22</td> <td>ဗ္ဗ</td> <td>ಙ</td> <td>8</td> <td>ର '</td> <td>2 8</td> <td>3 =</td> <td>2 2</td> <td>1 2</td> <td>62</td> <td>62</td> <td>ឌ</td> <td>42</td> <td>92</td> <td>=</td> <td>37</td>		\$	32	13	2	<b>œ</b>	24	88	22	24	ន	8	8	52	15	55	16	56	ន	14	23	22	54	=	গ্ৰ	15	54	35	22	ဗ္ဗ	ಙ	8	ର '	2 8	3 =	2 2	1 2	62	62	ឌ	42	92	=	37
Days		315	41	35	æ	ಜ	33	44	33	જ	34	98	35	34	33	36	33	35	ဗ္ဗ	35	34	32	33	35	8	3	45	46	43	21	33	జ	5	5 E	કે દિ	3 8	ষ্ট	3	3	ठ	4	ജ	ਲ	2
Date		220	46	33	83	37	33	42	98		34	37	ဗ္က	34	34	37	34	35	35	33	96	36	37	32	35	31	45	47	44	25	8	송	8	5	કે દ	3 8	8 8	જ	8	ठ	47	各	8	8
Date         Nestling         Event Fues         Mic           Phase         Type         Pos. 16           Day         Ambient         Cavity 56           04/15/99         Inactive         Ambient         Cavity 56           06/02/99         Post-fled.         Ambient         Base 33           06/02/99         Post-fled.         Ambient         Base 34           06/02/99         Post-fled.         Ambient         Base 37           06/0	_ [		25	20	\$	34	22	33	54	52	ಜ	21	9	22	55	52	23	50	ଛ	21	40	ଛ	ន	15	9	22	58	34	88	8	8	<b>₽</b>	ຂ	2	<b>5</b> €	2 4	2 8	2	62	ន	4	4	∞	ඉ
Date         Nesting         Event         Mic           Phase         Type         Pos. 10           D4/15/99         Inactive         Ambient         Gavity         56           04/15/99         Inactive         Ambient         Base         35           06/02/99         Post-fled.         Ambient         Base         36           06/02/99         Post-fled.         Ambient         Base         36           06/07/99         Post-fled.         Ambient         Base         37           06/07/	88 (HZ		Н	-	$\neg$	-	_	$\vdash$	$\vdash$	_	-		Н	$\neg$		$\vdash$		-	-	-	-	Н	-	$\vdash$	-	$\vdash$	Ι	$\vdash$	-	-	-		+	_	╅	_	+	+-	+-	┢	-	_	_	
Date         Nestling         Event         Mic           Day         Type         Pos. 10           Day         Type         Pos. 10           Day         Day         1           D6/02/99         Post-fled. Ambient Gavily 55           D6/02/99         Post-fled. Ambient Base 33           D6/02/99         Post-fled. Ambient Base 34           D6/07/99         Post-fled. Ambient Base 34           D6/17/99         Post-fled. Ambient Base 34 </td <td>dneuc</td> <td></td> <td></td> <td><math>\vdash</math></td> <td>_</td> <td>_</td> <td></td> <td>_</td> <td>L.</td> <td>Ь.</td> <td><b>!</b>—</td> <td>_</td> <td>ш</td> <td></td> <td>_</td> <td>_</td> <td></td> <td></td> <td>Ь.</td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td><math>\vdash</math></td> <td></td> <td></td> <td></td> <td>-</td> <td>_</td> <td>-</td> <td></td> <td>_</td> <td>4</td> <td>╀</td> <td>ـــــ</td> <td>┡</td> <td>_</td> <td>Ь.</td> <td>_</td> <td></td>	dneuc			$\vdash$	_	_		_	L.	Ь.	<b>!</b> —	_	ш		_	_			Ь.			_					_	$\vdash$				-	_	-		_	4	╀	ـــــ	┡	_	Ь.	_	
Date         Nesting         Event         Mic           Phase         Type         Pos. 10           D4/15/99         Inactive         Ambient         Gavity         56           04/15/99         Inactive         Ambient         Base         35           06/02/99         Post-fled.         Ambient         Base         36           06/02/99         Post-fled.         Ambient         Base         36           06/07/99         Post-fled.         Ambient         Base         37           06/07/	티모		_						_	<del>!                                      </del>	_	-	$\vdash$				_	-	Ь	$\mathbf{L}$		_				_		_	_	_		-			_	_	_	-	-				_	_
Date         Nestling         Event Fues         Mic           Phase         Type         Pos. 16           Day         Ambient         Cavity 56           04/15/99         Inactive         Ambient         Cavity 56           06/02/99         Post-fled.         Ambient         Base 33           06/02/99         Post-fled.         Ambient         Base 34           06/02/99         Post-fled.         Ambient         Base 37           06/0	5 E		_				-	-	_	-		-	-	-	$\overline{}$	-	_	_	_	-	_	_	_	_		-		_	-	$\rightarrow$	$\rightarrow$	_	_	-	_			_	_					_
Date         Nestling         Event         Mic           Day         Type         Pos. 10           Day         Type         Pos. 10           Day         Day         1           D6/02/99         Post-fled. Ambient Gavily 55           D6/02/99         Post-fled. Ambient Base 33           D6/02/99         Post-fled. Ambient Base 34           D6/07/99         Post-fled. Ambient Base 34           D6/17/99         Post-fled. Ambient Base 34 </td <td>Bectra</td> <td></td> <td>_</td> <td>_</td> <td></td> <td><math>\overline{}</math></td> <td>_</td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td>_</td> <td><math>\overline{}</math></td> <td>-</td> <td></td> <td>-</td> <td></td> <td></td> <td>_</td> <td>_</td> <td>_</td> <td>-</td> <td>_</td> <td>_</td> <td><math>\overline{}</math></td> <td></td> <td><math>\overline{}</math></td> <td><math>\overline{}</math></td> <td><math>\rightarrow</math></td> <td><math>\rightarrow</math></td> <td></td> <td>-</td> <td>2 2</td> <td><b>‡</b></td> <td>+</td> <td>-</td> <td>-</td> <td></td> <td>_</td> <td>_</td> <td></td>	Bectra		_	_		$\overline{}$	_				-	-	-		_	$\overline{}$	-		-			_	_	_	-	_	_	$\overline{}$		$\overline{}$	$\overline{}$	$\rightarrow$	$\rightarrow$		-	2 2	<b>‡</b>	+	-	-		_	_	
Date         Nestling         Event Fues         Mic           Phase         Type         Pos. 16           Day         Ambient         Cavity 56           04/15/99         Inactive         Ambient         Cavity 56           06/02/99         Post-fled.         Ambient         Base 33           06/02/99         Post-fled.         Ambient         Base 34           06/02/99         Post-fled.         Ambient         Base 37           06/0	taveS		_	_	_					·		_	-				_	_			_		_		_		_	_	_	_	_	_	_	_	_			-	<del></del>	┺	_	_		
Date         Nestling         Event         Mic           Day         Type         Pos. 10           Day         Type         Pos. 10           Day         Day         1           D6/02/99         Post-fled. Ambient Gavily 55           D6/02/99         Post-fled. Ambient Base 33           D6/02/99         Post-fled. Ambient Base 34           D6/07/99         Post-fled. Ambient Base 34           D6/17/99         Post-fled. Ambient Base 34 </td <td>3 0 0 0 0</td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td>_</td> <td>-</td> <td>⊢</td> <td>-</td> <td>-</td> <td>8</td> <td>-</td> <td></td> <td>_</td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td><math>\overline{}</math></td> <td>-</td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td><math>\mathbf{-}</math></td> <td><math>\vdash</math></td> <td><math>\mathbf{-}</math></td> <td><math>\overline{}</math></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td>_</td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>_</td> <td><math>\overline{}</math></td> <td>-</td>	3 0 0 0 0			_			_	-	⊢	-	-	8	-		_	-	_		_	$\overline{}$	-		-				$\mathbf{-}$	$\vdash$	$\mathbf{-}$	$\overline{}$						_	_	-	-		-	_	$\overline{}$	-
Date         Nestling         Event         Mic           04/1599         Inactive         Ambient         Cavity         56           06/0299         Post-fled.         Ambient         Base         37           06/0299         Post-fled.         Ambient         Base         38           06/0299         Post-fled.         Ambient         Base         39           06/0299         Post-fled.         Ambient         Base         36           06/0799         Post-fled.         Ambient         Base         37           06/0799         Post-fled.         Ambient         Base         37 <td>(G)</td> <td></td> <td></td> <td>_</td> <td>_</td> <td></td> <td></td> <td>-</td> <td></td> <td>—</td> <td>_</td> <td>37</td> <td>-</td> <td>_</td> <td>_</td> <td>_</td> <td></td> <td>_</td> <td></td> <td><math>\mathbf{-}</math></td> <td>-</td> <td>-</td> <td><math>\mathbf{I}</math></td> <td>_</td> <td><math>\overline{}</math></td> <td>-</td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td>_</td> <td>_</td> <td>_</td> <td></td> <td>_</td> <td>-</td> <td>_</td> <td>_</td> <td></td> <td></td> <td>2</td>	(G)			_	_			-		—	_	37	-	_	_	_		_		$\mathbf{-}$	-	-	$\mathbf{I}$	_	$\overline{}$	-	-	-		-	-			_	_	_		_	-	_	_			2
Date         Nestling         Event         Mic           Day         Type         Pos. 10           Day         Type         Pos. 10           Day         Day         1           D6/02/99         Post-fled. Ambient Gavily 55           D6/02/99         Post-fled. Ambient Base 33           D6/02/99         Post-fled. Ambient Base 34           D6/07/99         Post-fled. Ambient Base 34           D6/17/99         Post-fled. Ambient Base 34 </td <td>ğ</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td><u> </u></td> <td></td> <td></td> <td>98</td> <td>_</td> <td></td> <td></td> <td></td> <td>_</td> <td>_</td> <td>-</td> <td>Н</td> <td>-</td> <td>_</td> <td></td> <td>_</td> <td>_</td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td>-+</td> <td>_</td> <td>_</td> <td>_</td> <td>+-</td> <td></td> <td></td> <td>_</td> <td></td> <td>33</td> <td>ន</td>	ğ					_				1		<u> </u>			98	_				_	_	-	Н	-	_		_	_		-	-			-+	_	_	_	+-			_		33	ន
Date         Nesting         Event Price         Mic           Phase         Type         Pos.           Day         Ambient         Cavity           06/0299         Post-fled.         Ambient         Base           06/0299         Post-fled.         Ambient         Base           06/0299         Post-fled.         Ambient         Base           06/0799         Post-fled.         Ambient	Bal					_			_		_	<del> </del>	-	_	+			_	_	_			_	_		_		_	_	_	_				_		_			_		_		_
Date         Nestling         Event           Phase         Type           Day         Type           06/02/99         Post-fled. Ambient           06/07/99         Post-fled. Ambient           06/17/99 <td< td=""><td>_</td><td></td><td><del>}</del></td><td>-</td><td>_</td><td></td><td>_</td><td><del>-</del></td><td>-</td><td>-</td><td><del>! -</del></td><td>-</td><td><math>\vdash</math></td><td></td><td>_</td><td>_</td><td>_</td><td></td><td>-</td><td>-</td><td>⊢</td><td>-</td><td>_</td><td><math>\vdash</math></td><td>-</td><td></td><td>_</td><td>-</td><td>_</td><td>Н</td><td>-</td><td>_</td><td>-</td><td>_</td><td>_</td><td></td><td>+-</td><td>+</td><td>+</td><td></td><td>-</td><td>-</td><td>-</td><td></td></td<>	_		<del>}</del>	-	_		_	<del>-</del>	-	-	<del>! -</del>	-	$\vdash$		_	_	_		-	-	⊢	-	_	$\vdash$	-		_	-	_	Н	-	_	-	_	_		+-	+	+		-	-	-	
Date         Nesting           Phase         Phase           04/15/99         Inactive           06/02/99         Post-fled.           06/12/99         Post-fled.           06/12/99         Post-fled.           06/12/99         Post-fled.           06/12/99         N-12           06/12/99         N-14           06/12/99		Pos	Say	Bas	Cavi	Bas	Bas	Bas	Cavi	Bas	Bas	Bas	Cavi	Bas	Bas	Bas	Bas	Т	H		Savi	Bas	Cavi	Bas	Bas	Bas	Bas	Bas	Bas	Bas	Bas	Sa.	Bas	Ba Ba	88	8 8	Bas	Bas	Bas	Bas	Bas	$\vdash$	Н	Bas
04/15/99 06/02/99	Event	Туре	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient				Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient		_	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient			Ambient	Ambient
04/15/99 06/02/99	Nesting	Phase Day	Inactive	Post-fled.	Post-fled.	N-3	4	-	Post-fled.	Post-fled.	N-8	Post-fled.	Post-fled.	Egg laying	0-N	8구	0-N	?	27	Post-fled.	Post-fled.	Post-fled.	Post-fled.	Incubation	Post-fled.	1.4	N-2	N-2	ε. Σ	0	Post-fled.	Post-fled.	e z	N-12	N-14	2 2	5 5	무	1.10	Z-K	Post-fled.	Post-fled.	F10	¥-7
·····································	Date	<del></del>	<del> </del>	<del> </del>	_	5/28/99	4/28/99	├		╌	5/13/99	1	_	-	5/28/99	4/29/99	5/28/99	5/02/99	5/19/99		Η-	<del>                                     </del>	Н	-	_	4/28/99	5/12/99	5/12/99	5/13/99	5/17/99	Н	-	66/60/9	6/16/99	6/18/39	86/77/0	5/17/99	5/11/99	5/11/99	5/13/99	┼─		5/16/99	5/24/99
	 ਤ		<del> </del>	-	Н	H	<del> </del>	$\vdash$	┢	╁╴	┢╌	┝	├		-	H	$\vdash$	-	┢	H	-	┢	⊢	├	_	$\vdash$	┢	┝┈	├			$\vdash$	┪	+	+	+	╁	╁	╁	╁╌	╁	╁	┝	-

[;	le c	_	e			٦	٥	٦	<b>.</b>	<u></u>	2	2	3		_	2	~		2		<u>ښ</u>	60	~	ري		,	5)	9	. α	, ,	9	48.8	7	ဖွ	١	اب	?	0.	52.5	51.7	47.8	20.7	6.	7.5
L.,	<u> </u>	46.2	48.3	20.	52.3	48.	25 6	g	69	49	49	46.	51	54.3	₩.	52.	20.	47.	83	52.	<u>6</u>	47.	51	48.5	45.	48.7	47.9	47.0	\$ Q	48.7	23	48	8	48	23	<u>망</u>	ଥ	51	25	25	47	3	4	4
	20000 	6	2				١	2				က					3								2			$\downarrow$	1	$\downarrow$	2				2	_			3	-		4	^	_
	16000	12	16	9	£	2	2	22	9	16	4	9	ଯ	9	4	4	16	16	4	14	15	<del>1</del>	-	22	8	9	اع	<del>ن</del> م	5 £	2 2	9	16	9	15	17	7	12	15	46	9	5	9	۳	5
	12500	23			5								92					14						ļ	₹	ľ	~				7		2						15				ន	
	0001	27	11	12	<del>π</del>	4	7	7	2	9	12	Ξ	ಚ	7	Ξ	14	12	16	=	7	12	12	4	4	×	£	4	2 2	±   8	3 2	16	17	15	13	14	91	13	12	15	16	13	15	13	4
	0008	೫	82	53	8	2	2	8	2	8	50	19	32	ន	ន	52	22	22	21	18	48	20	짇	22	22	62	R	ខ្ល	7 8	3 9	6	23	12	82	21	21	18	18	18	19	56	ಜ	ន	51
	9300	34	9	10	ಣ		;	ន	8	91	10		19		14	83		15							ຂ		8	92	20	ğ	12	22	15							4	34	유	24	88
	2500 3150 4000 5000	1				_	_		_		_	_	$\vdash$	_	-		_	_			$\vdash$	$\vdash$	_		-	-		2 23	-		_	+	-	Н		_					_			
	4000	88	92	56	27	8	8	ಙ	8	53	31	58	ಜ	9	35	ස	31	22	22	೫	53	27	8	83	8	-+		ج ا	8 8	3 6	_	+	-	႙	গ্ৰ	88	56		88	82				<u>ਲ</u>
	3150	F	_		8			_	^			15			30			L.	13	L	24		8	_	7		9	-	4	2   ∓	+	38	⊢	Ц	∞		_	16	8		-	8	Н	=
	2500	_	L	ᆫ	82		_				_	_	1	_	_		<b>—</b>	⊢	<u> </u>	<u> </u>	<u> </u>	Н	-			-	-4	ਲ	+	-	┰	+	├-	-	_	├	-	┰	┼		$\vdash$	-	Н	Н
	2000	╁	┢╌	⊢	Н	┪	_						_	_			_	⊢	-	_	-	-		-		$\rightarrow$	-	83	-			+		-	_	_	┼	1	1		_			
	0 1600	╀╌	5	_	22	4		-		-	┼	├	╌		-	-	⊢	├	⊢	1	$\vdash$	┢	-	Н	_	-		æ !	╅	-	+	╅┈╴	+-	31 20	-	-	┪	-	1		1		30 1	1 22
	1000 1250	82	┺	┞		_		_			ļ	<b>!</b>	<b>├</b>	_	├	⊢	⊢	├-	-	├	⊢	├-		Н	_	H		62 63	-+	-	+	╫	╀╌	1	$\vdash$	<del> </del>	┝╌	┿	╁	-	╁╌	⊢	⊢	Н
	800	╂	₩	⊢	36 36	-			-	├		├	1	_	-		⊢	┢	┼	╌	┰	-	├-	├─┤	-	$\vdash$	$\dashv$	-+	-+	-+-	3 8	+-	+-	+	⊢	+-	-	+	+	$\vdash$	+	<del>                                     </del>	25	Н
	98 86	1	1							1			!	1		1			L	I				1				53					┸	_	Ц.	_	┺	<u> </u>	ــــــــــــــــــــــــــــــــــــــ	_	-	-	┖-	L
	8	十	3	-	_		-		_			-	+-	-	+	-	-	-	+		+	+	-	_		-		30	$\overline{}$	_	_	_	_	$\overline{}$	$\overline{}$	_	$\overline{}$			_	${}^{-}$	$\overline{}$	П	33
	400	4	2	1	8	56	19	15	18	8	2	9	ន	ន	23	ន	53	22	27	24	31	23	ន	20	41	18	7	17	72	₹ 8	3 8	~	8	2	22	ន	8	2	ន	62	55	12	ଛ	~
	315	1	33	1	L					┞	<del> </del> _	ـــ	37	ļ	ļ	ļ	-	╄	╄	↓_	╄	╄	_	ļ	⊢	1		೫	-	-+	+	+-	+-	+	├	┿	┼	1	┿	+	+	+	+	+-1
	250	3	ဗ္ဗ	8	34	88	J	<u> </u>		Ļ.,	╄	-	-	٠	╄-	╄	╄	-	╄	4	+-	╄	<b>├</b> ─	↓	⊢	-		ਲ	-	-	-		+	-	+	+-	+	+	+-	+	_	_	+	_
(2)	8		4	1	ន			ŀ	ı					i		t	1			1	1	1		L	1			11				_		-	-	_	-	+	-	-	-	_	-	
icies (Hz)	25 160	38	$\overline{}$	_	35			37 33		39	т	37	$\top$		89	Т	8	Τ.		1	Τ.	T.,	L	L			98 8	36		$\Box$	8 6	٦			8	. _	. ا	1	ءا،		88	37	88	~
Band I EQ (dB) at 1/3 Octave Spectrum Center Frequenc	100 125	_	-	4-	╄	8		gg	<u> </u>	1_	22	_		╄	↓_	┺	╄-	╄	8	┺	8	_	╙	╄-	ļ	₩-	82	╙	_	_	ج ا	┷	4	┿	╄	4_		┿	+-	╄-	2	-	22	22
enter	8	83	-	-	-	37	8	£	æ	88		-	+	4	-	-		-	_	_		+	+-	98	88	37	33	-			33 %	_	-	-	-	<del></del> -	-	-	-	+	-	-	_	37 35
otrum (	50	-	3 2	_	35 37	37 38	27 41	44	38 4	34 41	-	┪	+-	+	+-	+-	+	+			+-	-	-	+	39	21 40	38	1 1	-		ह   <del>ड</del>	-	-	-	+-	+	-			+		+		20
ve Spe	8	34	8	4	æ	37	జ	45	္တ	စ္တ	3	8	용	6	37	63	g	چ چ	99	£	4	뚕	_		88	_	88		88		33	_	_		-	_	-	-		_	-			8
/3 Octa	25 32	_	3 8		-	13 37	33	43 46	85 83	+-		-	+-	35 41	-	-	35	-	+	+	32 38	-	-	-	+	+-	39	31 38	_	-+	S S	_	3 8	-	+	-		-	_	8 8	_		_	31 36
B) at 1	2 2	-	3 8	-	-	33	₩	42	-	+-	<del>-</del>	-	-	+-	-	-	8	-	—	┿	-	+	-	-	98	-	35	-	-	-	-	7 2		-	+	<del>-i</del>	-	-		8	-			8
P) C4	16 20		3 15	_		ક્ષ	-	gg	-	+-			-	+	-	+	-			+-	-	+		-	စ္တ	စ္တ	ಜ	36	49	္တ	္က (	<b>₽</b> 8	3 8	3 8	Ę	3 8	1 8	3 8	¥ g	3 8	2 6	, g	3 6	32
pue	5	8	3 8	1 6	5	22	52	40	22	25	1 4			45		8	g	÷	25	3	; <sub>2</sub>	1 12	37		22			ន	59		33	<b>₽</b> ¤	2	$\perp$	44	_		g g		3 15	_	8	_	
-	5	3		-	4	ಜ	34	98	38	+		+-	-	-	-	_	_		-	+	_	-	+-	+-	+	+	+-	-	-	$\overline{}$	-	3 8	-	_	+	-		3 %		3 8	-	+	┿	8 8
Mis	Pos	8	Caulty	Base (	Base	Base	Base	Base	Base	Base	88	Race	Base	Cavity	Base	Bago	Bace	Bace	A Pier	Dage (	Aive C	Rase	Base	Savit	Base	Cavity	Base	Base	Base	Base	Base	Savid	Baco	Cavity	Baco	Page 1	Dasa	0030	Dase	Race	Bace	Race	Base	Cavity
Event	Type	Ambion	Ambiont	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Amhient	Ambient	Ambiant	Ambient	mhient	Ambient	Ambiant	Ambiont	Ambiont	Ambient	Ambiont	Imbient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambion	Ambient	Ambiont	Ambiant	Ambiont	Ambiont	Ambigat	Ambiont	Ambiont	Ambient	Ambient	Ambient
Moeting	Phase	Г	ISO CO	18		T	12	.5		Т		Т	7			2 4 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	Τ	Т	Т	٦				1	1	1.	_				_	Post-fled.	_	Post-fled	$\overline{}$	- 4	Т	T		Dro port	┰	7		_
otec		+	66/21/90	╅	+	05/13/99	06/12/99	╈	+	╁	05/16/00	02/10/20	+	+	+	+	00/00/30	00/21/00	2/00	00/1/99	┰		66/91/60	05/26/99	┿	┰	╈	05/03/99	06/01/99	05/28/99	$\rightarrow$	06/07/99	-	G 60/7/90	+	04/23/99	66//2	04/29/99	-+-	04/49/00	╅			+
-		+	+	┿	╁	+	╁	╁	╫	+	+	十	+	+	+	+	╁	200	+	+	+	102	+	╫	╁	+	╫	╁	╁╾	176 05/2	$\vdash$	179 06/	+	183 06/	+	+	╅	┰	┽	╅	+	+	+	205 06/
3	<u> </u>	٩	2 8	٤	3 5	15	3	. 6	3 2	5 5	2   5	- [-	3 5	¥	-   =	1		: ا		8	=   5		1	1		1	ľ	- [	۲	_		- [									_[	- ا	710	<u>" "</u>

			_									
Cafc.	Overall	LEQ	57.4	53.7	66.5	47.1	64.8	49.9	48.9	50.4	49.2	47.0
	20000		5				18	3		8	8	+
	16000		56	17	16	15	32	17	17	19	17	13
	12500		34							13	7.7	
	10000		48	15	14	16	32	15	13	17	50	13
	0008		46	22	50	56	38	17	50	54	98	22
	0089		23			30				18	23	19
	2000		32	22	56	53	33	97	92	58	22	22
	4000		99	67	58	58	43	53	87	31	53	35
	3150					4				30		18
	2500		36	31	31	56	45	67	87	31	67	12
	2000		37	31	31	56	43	53	53	31	29	27
	1600		30	23	22	18	40	17	50	56	21	21
	1250		39	35	37	53	47	33	32	32	31	90
	1990		33	36	38	53	48	34	33	33	32	30
	800		28	32	32	24	36	28	28	22	23	22
	630		40	37	36	31	20	36	34	34	33	32
	200		45	88	37	35	51	37	38	35	34	33
	400		82	92	52	11	38	52	55	23	50	16
	315		45	98	37	33	51	88	35		34	33
	220		4	37	33	33	53	37		37	35	34
(z	200		30	23	\$	82	40	24	23	ଝ	23	19
cies (Hz)	5 160		7 43	98 (	53	7 32	25 2	38	98	98	34	7 32
Band LEQ (dB) at 1/3 Octave Spectrum Center Frequen	100 125		37   47	29 40	45	24 37	44 5	25 40	25 40	28	39	18 37
nter Fr	80		47	38	14	8	25 /	37 2	35	es	37	33
흥	89		84	11	\$	37	99	9	9	45	9	37
pectru	20		35	33	44	19	31	22	22	31	33	15
ave S <sub>l</sub>	8		45	8	47	98	25	89	32	8	<del>우</del>	ဆ
3 Oct	32		3 46	8	69	8	54	8	8	6	33	98
) at 1/	20 25		42 36	44	56 51	38	23	88	37 23	98 98	38	38 26
8P) O	16 2		45 4	45 4	61	39	54 5	99 98	38	98 88	88	88
37 PL			-	45	8	28		8	27	8	92	25
Ba	10 13		43	47	8	34	23	39	88	37	ક્ક	8
Mic	Pos.		Base	Base	Cavity	Base	Base	Base	Cavity	Base	Base	Base
Event	Type		Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient	Ambient
Nesting	Phase	Day	Post-fled.	Post-fled.	Post-fled.	<u>æ</u>	4	Post-fled.	Post-fled.	Post-fled.	9-N	6-N
Date			06/14/99	06/18/99	06/18/99	06/22/99	04/23/99	06/03/99	66/00/90	66/03/90	05/28/99	06/50/99
ਣੌ			902	216	216	216	218	227	227	271	294	96Z

## **CERL DISTRIBUTION**

Chief of Engineers

ATTN: CEHEC-IM-LH (2) ATTN: CEHEC-IM-LP (2)

ATTN: CEMP ATTN: CEMP-CE ATTN: CEMP-EA (2) ATTN: CEMP-ZM ATTN: CERD-ZA

Engineer Research and Development Center

(Libraries)

ATTN: ERDC, Vicksburg, MS

ATTN: Cold Regions Research, Hanover, NH ATTN: Topographic Engineering Center,

Alexandria, VA

SERDP (3)

ACS(IM) 22060 ATTN: DAIM-FDP

CEISC 22310-3862 ATTN: CEISC-E ATTN: CEISC-FT ATTN: CEISC-ZC

HQ USAREUR & 7th Army

ATTN: AEAEN-EH ATTN: Unit 29351

US Military Academy ATTN: MAEN-A

ATTN: Civil Div Director ATTN: Dept of Geo & Env Engr ATTN: Facilities Engineer Commander FORSCOM ATTN: FCEN-RDF 30330-6000

US Army ARDEC 07806 ATTN: SMCAR-ISE

Linda Hall Library 10017 ATTN: Acquisitions

US Army Environmental Center ATTN: SFIM-AEC-NR 21010 ATTN: SFIM-AEC-CR 64152 ATTN: SFIM-AEC-SR 30335-6801 ATTN: AFIM-AEC-WR 80022-2108

National Guard Bureau 20310

ATTN: NGB-ARI

Naval Facilities Engr Command ATTN: Facilities Engr Command Code 20YAZ (2)

US Army CHPPM ATTN: MCHB-DC-EEN

US Gov't Printing Office 20401 ATTN: Rec Sec; Dep Sec (2)

Nat'l Institute of Standards & Tech

ATTN: Library 20899

Defense Supply Center Columbus

ATTN: DSCC-WI 43216

Defense Tech Info Center 22304 ATTN: DTIC-O (2)

> 41 5/00

## REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of Information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

wanagement and budget, Paperwork	reduction Project (0704-0100), Washing			
1. AGENCY USE ONLY (Leave Blank)	2. REPORT DATE May 2000	3. REPORT TYPE AND DATES C Final	COVERED	
4. TITLE AND SUBTITLE			5. FUNDING NUMB	ERS
	Impacts on the Red-cockaded We	oodpecker: 1999 Results		
Assessment of Hummig Head	impuoto on the rece to the to the	<b>P</b> • • • • • • • • • • • • • • • • • • •	CS 1083	
			C5 1005	
6. AUTHOR(S)				
David K. Delaney, Larry L. Pa	ter, and Timothy J. Hayden			
- · · · · · ·				
7. PERFORMING ORGANIZATION NAME	(S) AND ADDRESS(ES)		8. PEFORMING OR	
U.S. Army Construction Engir	neering Research Laboratory (CE	RL)	REPORT NUMBE	R
P.O. Box 9005			TR 00-13	
Champaign, IL 61826-9005			-22.00	
• • •				
			40. 00010000110011	HONITODING
9. SPONSORING / MONITORING AGENC			10. SPONSORING / I AGENCY REPOR	
	arch and Devleopment Program		AGENOT HER ON	
ATTN: Holst/ Program Manag 901 N Stuart St., Suite 303	₹e1			
Arlington, VA 22203-1853				
9. SUPPLEMENTARY NOTES				
Copies are available from th	ne National Technical Information	Service, 5385 Port Royal	Road, Springfield	i, VA 22161
40- PIOTRIPUTION / AVAILABILITY OTAT	HENT		12b, DISTRIBUTION (	CODE
12a. DISTRIBUTION / AVAILABILITY STATE		,	120.013 INIBUTION	
Approved for public release	; distribution is unlimited.			•
			<u> </u>	
13. ABSTRACT (Maximum 200 words)				
It is estimated that nearly a	quarter of the remaining Red-coc	kaded Woodpecker (RCW)	) population resid	es on military
installations in the southeast	tern United States. Such a close a	ssociation has raised quest	tions about the int	teraction between
training and the conservation	n of Red-cockaded Woodpeckers	on military land. Increase	ed importance has	been placed on
determining how noise affect	cts these species. This report pres	sents second year results of	f a multiyear study	y to determine the
effects of certain kinds of tra	aining noise on the endangered R	ed-cockaded Woodpecker.		
Droliminame data avagast the	at: measured levels of experiment	al noise from 50-caliber b	lank fire and artill	lery simulators did
not offeet PCW nesting and	cess or productivity; Red-cockade	ed Woodnecker flush freque	iency incressed so	stimulus distance
doggood magadian of stir	nulus type; woodpeckers returned	to their nects relatively or	ickly after heing	flushed and noise
decreased, regardless of stir	nulus type; woodpeckers returned odpecker nest cavities were subst	antially louder than lavels	recorded at the ha	ise of the nest tree
levels in Red-cockaded Wo	oupecker nest cavities were subst	annany louder man levels.	recorded at the ba	ioo of the frost froe.
14. SUBJECT TERMS		<u> </u>		15. NUMBER OF PAGES
threatened and endangered spe	ecies nois	se		144
Red-cockaded woodpecker		itary training		16. PRICE CODE
range management		RDP		
17. SECURITY CLASSIFICATION	18. SECURITY CLASSIFICATION	19. SECURITY CLASSIFICATION	)N	20. LIMITATION OF
OF REPORT	OF THIS PAGE	OF ABSTRACT		ABSTRACT
Unclassified	Unclassified	Unclassified		SAR